#### D-5-4 & D-5-5 INVESTIGATION REPORT

#### 7723 HIGHWAY 89

#### TOWNSHIP OF ADJALA-TOSORONTIO COUNTY OF SIMCOE

PREPARED FOR:

#### PILLA INVESTMENTS INCORPORATED

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#### 1.0 Introduction

C.F. Crozier & Associates Inc. (Crozier) was retained by Pilla Investments Inc. to prepare a Hydrogeologic Report to support the Draft Plan of Subdivision for the proposed development located at 7723 Highway 890 in the Township of Adjala-Tosorontio, County of Simcoe. The subject lands are approximately 29.1 ha in size and are located on the south side of Highway 89, west of Concession Road 7. A site location plan is presented on Figure 1. This report has been prepared in conjunction with a Functional Servicing & Preliminary Stormwater Management Report also prepared by Crozier and submitted under a separate cover.

The subject lands (the Site) are located within the Township of Adjala-Tosorontio, County of Simcoe. The Site is currently occupied by an existing rural residential dwelling and agricultural buildings, which are proposed to be removed. The elements envisioned for this development include:

- 22 commercial/industrial lots
- 22 at grade asphalt parking lots
- One site access point on Highway 89, located at 7723 Highway 89
- One site access point on Concession Road 7, approximately 240 meters south of Highway 89

Our review and work plan for this Hydrogeological Report was developed based on the Concept Plan prepared by MHBC, dated March 2022.

We have also reviewed the pertinent background information associated with the Site, including:

- Topographic Survey (J.D. Barnes Ltd March 11, 2021)
- Concept Plan (MHBC Planning, March 2022)

#### 1.1 Land Use

The Site is approximately 29.1 ha and landscaping on the property consists of agricultural land, trees, and grass. The Site is bounded by:

- Highway 89 and existing commercial properties to the North
- Concession Road 7 to the East
- Residential and agricultural lands to the West
- Agricultural lands to the South

The Site is currently zoned as Employment (E1) per the Township of Adjala-Tosorontio Zoning By-law No. 13-14, Schedule 'A', as amended.

The Site is characterized by active agricultural fields, an existing farm dwelling and agricultural structures. The existing farm dwelling, and associated agricultural structures are located along the north property line and are accessible via a gravel driveway access to Highway 89. Refer to Figure 1 for the Site location plan.

#### 2.0 Physical Setting

#### 2.1 Physiography

The Site is located within the physiographic region known as the Peterborough Drumlin Field, near the West Lowland area of the Simcoe Lowlands as shown on Figure 2. The area is characterized as an area of rolling drumlinized till plain. The Simcoe Lowlands physiographic region surround the north and east of the Site, while the Horseshoe Moraines physiographic region surround the area west of the Site.

#### 2.2 Topography and Drainage

No municipal storm sewer servicing or private storm infrastructure exists. The Site is a part of the Nottawasaga Valley Conservation Authority (NVCA) Source Protection Area and the Boyne River subwatershed. South of the Site features a tributary of the Boyne River that flows east to west named Spring Creek. Per the topographic survey, the Site generally drains surface flow from north to south across the property and a 26 m elevation difference is noted across the Site.

#### 3.0 Geology

The bedrock geology and surficial geology of the Site and surrounding area is displayed on Figures 3 and 4.

#### 3.1 Regional

According to Ontario Geological Survey (OGS) mapping, the surficial geology of the Site predominantly consists of glaciolacustrine clay to silty textured till that extends to the western part of the Site with sand to gravel foreshore-basinal deposits running through the eastern portion of the Site. The foreshore-basinal deposits are predominant in the region and extend from the Township of Essa to Barrie. The bedrock in the area is predominantly comprised of shale, limestone, and dolostone of the Georgian Bay Formation.

#### 3.2 Local

Surficial geology mapping for the area indicates that the soils for most of the Site are clay to silt-textured till and coarse-textured glaciolacustrine deposits. These soils are characterized as poorly drained and have high runoff potential.

Crozier and Walker Drilling completed a soils investigation on June 7 and June 8, 2021, during the installation of monitoring wells (Figure 5). The following soil profile was noted on the Site:

- 0.0 mbgs to 0.61 mbgs of brown, dry, loose sandy silt with organics and trace clay
- 0.61 mbgs to 1.22 mbgs brown, moist, dense silty clay with trace sand
- 1.22 mbgs to 4.27 mbgs brown to grey, wet silty clay to clay silt till with trace sand and trace clay
- 4.27 mbgs to 6.10 mbgs brown, wet sand with trace cobbles

The field observations of the soil profile above are consistent with OGS mapping. Further discussion of the 2021 Monitoring Well program is detailed in Section 5.0. As part of the D-5-5 and D-5-4 requirements, five (5) test water supply wells were completed by Franklin Drilling Services Inc. from June 2021 to August 2021.

The water well records indicate the following general soil profile was encountered:

- 0.0 mbgs to 0.3 mbgs topsoil
- 0.3 mbgs to 8.0 mbgs brown clay with stones
- 8.0 mbgs to 13.0 mbgs brown sand and silt
- 13.0 mbgs to 26.0 mbgs grey clay with stones
- 26.0 mbgs to 47.0 mbgs brown sand with gravel
- 47.0 mbgs to 57.0 mbgs brown clay
- 57.0 mbgs to 79.0 mbgs grey clay
- 79.0 mbgs to 92.0 mbgs brown sand

Further details of the 2021 Test Well Program are detailed in Section 5.0.

#### 4.0 Hydrogeology

#### 4.1 Hydrostratigraphy

The hydrostratigraphic framework of the Alliston area has been outlined in the NVCA Groundwater Monitoring Network Review and Assessment. Table 1 below summarizes the hydrostratigraphy of the study area and the subject property.

| Layer        | Name                   | Function | Material                          | Thickness<br>(m) | Water<br>Supply |
|--------------|------------------------|----------|-----------------------------------|------------------|-----------------|
| Youngest – 1 | Upper Confining Layer  | Aquitard | Till                              |                  |                 |
| 2            | Aquifer 1 (A1)         | Aquifer  | Sand and gravel                   | 10 – 50          | Domestic        |
| 3            | Confining Layer 1 (C1) | Aquitard | Clay and silt                     |                  |                 |
| 4            | Aquifer 2 (A2)         | Aquifer  | Interbedded sand<br>and silt/clay | 25 – 100         | Domestic        |
| 5            | Confining Layer 2 (C2) | Aquitard | Silty sand to sandy silt till     |                  |                 |
| 6            | Aquifer 3 (A3)         | Aquifer  | Sand and gravel                   | 35 – 70          | Alliston        |
| 7            | Confining Layer 3 (C3) | Aquitard | Silt and clay                     |                  |                 |
| 8            | Aquifer 4 (A4)         | Aquifer  | Sand and gravel                   | 3 - 30           | Alliston        |
| Oldest – 9   | Top of Bedrock         |          |                                   |                  |                 |

 Table 1: Hydrostratigraphy of the NVCA Watershed

In the Nottawasaga Valley Watershed, regional groundwater flow in the deep and shallow aquifers generally follows topography and surface water drainage eastward towards Boyne River and its tributaries and Cooks Bay.

In general, there are four (4) major aquifer units in the general area of the Site: A1, A2, A3, and A4. A1 and A2 generally supply domestic water supply and are commonly unconfined. Only in a few areas is A1 confined by till. A3 and A4 are confined in nature and are connected in some areas. The Town of Alliston Municipal wells are screened within this aquifer.

#### 4.2 Background Water Quantity

A review of the Ministry of Environment, Conservation and Parks (MECP) Well Record Database revealed a total of 156 well records within 1 km of the subject property (Figure 6), with one (1) well record mapped within the Site boundaries. A summary table of the well records is included in Appendix A. In general, a review of the identified well records is summarized below:

- Of the 156 well records identified, 95 are domestic supply, 25 are monitoring wells or test holes, 7 are commercial supply and 4 wells are for livestock or farm water supply. The remaining wells were identified as abandonment records or were unidentified.
- Many of the wells are screened within overburden material, with only 2 completed in the shale bedrock. These wells report the overburden thickness in the area is approximately 80 mbgs to 100 mbgs.
- The water supply wells in the area are screened within sand to gravel overburden material and are completed to an average depth of approximately 30 mbgs.
- Static water levels range from 36.6 mbgs to 1.5 m above ground surface (mags). Only 9 wells are reported to have water levels at or above ground surface and are screened within a confined sand and gravel aquifer between 25 mbgs to 40 mbgs.
- The domestic water supply and commercial water supply wells in the area have a reported average well yield of 36.5 liters per minute (LPM).
- Well ID 5738137 is mapped within the subject property boundary. The well is a 152 mm steel cased domestic water supply well and is screened within a confined sand and gravel aquifer from 57.3 mbgs to 58.5 mbgs.
- An 8-hour pumping test was completed on Well ID 5738137 in 2003. The static water level was measured at 24.4 mbgs and the pumping water level was measured at a level 53.3 mbgs. The reported well yield of this well is 22.7 LPM or 5 gallons per minute (GPM).
- Well ID 7293607 is interpreted to be the water supply well for the Home Hardware adjacent to the subject property. This well is constructed within a confined sand and gravel aquifer from 30.5 mbgs to 32.9 mbgs and has a reported yield of 37.8 LPM or 10 GPM.

#### 4.3 Background Water Quality

Regional groundwater quality monitoring is conducted by the NVCA using the Provincial Groundwater Monitoring Network (PGMN) wells. Groundwater samples are collected and analyzed for general chemical parameters, biological parameters, metals, and nutrients. Two (2) PGMN wells are located near the subject property, W281-1 and W231-1. No exceedances of the measured parameters for the groundwater samples from the nearby wells were noted in the Nottawasaga Valley Source Protection Area Approved Assessment Report. The completed analysis of the Alliston Water Works wells notes that the groundwater in the area occasionally exceeds aesthetic and operational guidelines from Ontario Drinking Water Quality Standards (ODWQS) including hardness, iron, aluminum, and organic nitrogen and are considered to be naturally occurring. The assessment report notes that coliforms have been detected in raw water in municipal groundwater supply wells.

Groundwater sampling was completed by Crozier across the subject property to determine local background groundwater quality and complete the D-5-5 test well requirements. Discussion of the groundwater sampling is continued in Section 5.3 and Section 6.3.

#### 5.0 Field Work

#### 5.1 Well Construction

From June 7 to June 8, 2021, Crozier supervised the installation of five (5) groundwater monitoring wells and five (5) test water supply wells on the subject property as shown on Figure 5.

The monitoring well locations were selected to determine seasonal high groundwater elevation and flow direction across the Site. Table 2 below details the monitoring wells on the Site.

| Monitoring<br>Well | <b>Total Depth</b><br>(m) | Screened Interval<br>(m) | Material   |  |  |  |  |  |  |
|--------------------|---------------------------|--------------------------|--|--|--|--|--|--|--|
| MW21-1             | 6.10                      | 3.05 – 6.10              | Brown, medium, saturated sand; trace gravel  |  |  |  |  |  |  |
| MW21-2             | 6.10                      | 3.05 – 6.10              | Grey, dry, clay till with gravel and trace sand  |  |  |  |  |  |  |
| MW21-3             | 6.10                      | 3.05 – 6.10              | Brownish grey, low moisture, silty clay till with gravel and trace sand  |  |  |  |  |  |  |
| MW21-4             | 6.10                      | 3.05 – 6.10              | Grey, wet silt till with gravel, trace clay and<br>sand to grey, low moisture clayey silt till with<br>gravel and trace sand |  |  |  |  |  |  |
| MW21-5             | 6.10                      | 3.05 – 6.10              | Grey, low moisture, silty clay till with gravel<br>and trace sand  |  |  |  |  |  |  |

#### Table 2: 2021 Monitoring Well Details

All monitoring wells constructed as part of the 2021 program were installed with as 50 mm diameter Schedule 40 PVC monitor wells with #10 slot PVC screens. The sand packs were designed and placed such that the sand pack was contained within the unit being monitored and hydraulically isolated from overlying stratigraphic units via the placement of a bentonite seal. Monitoring well logs have been included in Appendix B. During the period of June to August 2021, five (5) test water supply wells were completed by Franklin Drilling Services Inc. to support the D-5-5 analysis for the proposed development. The locations for the test wells were evenly distributed across the subject property to create a dense network and were completed to different depths. The depth of the test well was determined during drilling and decided based on the anticipated well yield of the intercepted aquifer. All locations are shown on Figure 5 and test well records are included in Appendix C. The test well construction details are displayed in Table 3 below.

| Monitoring<br>Well | <b>Total</b><br>Depth<br>(m) | Total<br>DepthScreened<br>IntervalStick Up<br>(m)Static Level<br>(mbgs) |      | Material |                          |
|--------------------|------------------------------|---|------|----------|--------------------------|
| TW21-1             | 30.78                        | 22.30 - 30.78   | 0.45 | 6.30     | Brown sand<br>and gravel |
| TW21-2             | 47.85                        | 46.63 - 47.85   | 0.50 | 10.97    | Brown sand<br>and gravel |
| TW21-3             | 34.44                        | 32.91 – 34.44   | 0.45 | 15.54    | Grey sand<br>and gravel  |
| TW21-4             | 90.22                        | 89.00 - 90.22   | 0.50 | 21.24    | Brown sand               |
| TW21-5             | 72.84                        | 71.62 – 72.84   | 0.50 | 12.61    | Brown sand               |

| Table | 3. | 2021 | Test | Well | Details |
|-------|----|------|------|------|---------|
| IUDIC | υ. |      | 1631 | 1101 | Derails |

1. Static water level measured from top of casing to the measured water level on the date of pumping the specified well.

Well water records for test wells TW21-1 to TW21-5 are included in Appendix C.

#### 5.2 Groundwater Level Monitoring

Following the installation and development of the wells, Crozier installed data loggers into each of the five monitoring wells to assess the seasonally high groundwater level through the spring months. The data loggers were programmed to collect water levels on an hourly basis. Manual water level readings were also obtained on several occasions to confirm the accuracy of the values recorded by the data loggers.

#### 5.3 Groundwater Quality Sampling

Groundwater samples were collected from all monitoring wells and test wells on the subject property. Three rounds of groundwater sampling have been completed at the time of this report. Sampling of the monitoring wells was completed using purging methods with Waterra Tubing and three (3) well volumes were removed from each well prior to sampling and in-between samples. Test wells were sampled using a Grundfos Redi-Flo2- 2" Environmental Sampling Pump. Three (3) well volumes were removed prior to and in-between samples.

The first two sets of groundwater samples were submitted to AGAT Laboratories for analysis for the following parameters:

- E. Coli and Total Coliforms
- Anions including fluoride, chloride, nitrate, nitrite, bromide, sulphate and phosphate
- Cations including total calcium, magnesium, potassium and sodium
- Total metals

The third set of groundwater samples were analyzed for E. Coli, Total Coliforms, nitrate, and nitrite. Groundwater sampling results are attached in Appendix D.

#### 5.4 Hydraulic Testing

Pumping testing was carried out at TW21-1 to TW21-5 between June 11, 2021 to September 6, 2021. The pumping tests consisted of a pumping phase of 180 minutes using a submersible pump and a recovery phase of 180 minutes. The pumping rates were determined for each well by the Well Contractor depending on the estimated well yield. Water levels were measured at different time intervals throughout the testing period using a manual tape measure. Table 4 below displays the pumping rates used for each test well.

| Monitoring Well | Pumping Rate<br>(LPM) <sup>1</sup> | <b>Depth of Pump</b><br>(mbgs) |  |  |
|-----------------|------------------------------------|--------------------------------|--|--|
| TW21-1          | 22.73                              | 22.86                          |  |  |
| TW21-2          | 22.73                              | 45.11                          |  |  |
| TW21-3          | 13.63                              | 30.48                          |  |  |
| TW21-4          | 22.73                              | _ 2                            |  |  |
| TW21-5          | 22.73                              | 42.67                          |  |  |

| Table | 4: Test Well         | Pumpina   | Rates  |
|-------|----------------------|-----------|--------|
| Table | <b>H. ICSI WC</b> II | i vinping | NGIC 5 |

1. LPM - Litres per Minute.

2. Not reported in the well test data sheet.

Pumping test results are presented in Appendix E.

#### 6.0 Results

#### 6.1 Groundwater Levels

Manual groundwater level measurements at the monitoring well locations were taken from June 2021 to October 2021. Note groundwater monitoring is ongoing and will continue until at least Spring 2022. The results of the water level monitoring are included in Table 5.

|        | Ground                           | June 8, 2021             |                            | June 24, 2021            |                            | October 5, 2021          |                            | March 24, 2022           |                            |
|--------|----------------------------------|--------------------------|----------------------------|--------------------------|----------------------------|--------------------------|----------------------------|--------------------------|----------------------------|
| Well   | Elevation <sup>1</sup><br>(masl) | Water<br>Level<br>(mbgs) | <b>Elevation</b><br>(masl) | Water<br>Level<br>(mbgs) | <b>Elevation</b><br>(masl) | Water<br>Level<br>(mbgs) | <b>Elevation</b><br>(masl) | Water<br>Level<br>(mbgs) | <b>Elevation</b><br>(masl) |
| MW21-1 | 226.75                           | 2.53                     | 224.22                     | 3.03                     | 223.72                     | 2.31                     | 224.44                     | 1.43                     | 225.32                     |
| MW21-2 | 234.25                           | DRY                      | DRY                        | 4.64                     | 229.61                     | 2.06                     | 232.19                     | 1.20                     | 233.05                     |
| MW21-3 | 236.83                           | DRY                      | DRY                        | 5.34                     | 231.49                     | 3.06                     | 233.77                     | 1.36                     | 235.47                     |
| MW21-4 | 247.04                           | 1.12                     | 245.92                     | 1.23                     | 245.81                     | 1.85                     | 245.19                     | 1.01                     | 246.03                     |
| MW21-5 | 238.96                           | DRY                      | DRY                        | 1.89                     | 237.07                     | 1.97                     | 236.99                     | 1.29                     | 237.67                     |

Table 5: Water Level Monitoring Results

1. Estimated from Topographic Survey prepared by J.D. Barnes Ltd. dated March 10, 2021.

Manual water level readings were recorded in the wells by the Crozier staff on the dates presented in Table 5. In addition, data loggers were installed in each of the monitoring wells on June 24, 2021. On

March 24, 2022, the logger from MW21-5 was removed and replaced due to a logger reading error. The loggers record water levels in the well on an hourly basis to capture fluctuations in water levels that may occur during spring melt events and storm events. The results of the continuous water level monitoring are presented as hydrographs and attached in Appendix F. Please note the data from the level logger at MW21-5 was unable to be downloaded at the time of preparation of this report due to a logger reading error.

In general, water levels in all monitoring wells decreased from June to October 2021 and have been steadily increasing since October 2021. However, in MW21-2 and MW21-3 water levels have increased since installation. MW21-3 is located next to the existing farmhouse and could be installed in reworked material from the building of Highway 89 and therefore the water levels in the monitoring well are likely easily influenced by seasonal events. MW21-2 is in the centre of the field and could have also been installed in reworked material due to agricultural uses. Minor fluctuations are noted in all water level hydrographs. These fluctuations were consistent for each hydrograph and are likely due to daily barometric pressure fluctuations rather than the result of melt or rain events. Larger spikes in the hydrographs appear to be due to precipitation events.

The groundwater elevation across the subject property from northwest to southeast ranged from 246.03 masl to 225.32 masl from the period between June 2021 to March 2022. Therefore, groundwater is interpreted to flow from northwest to southeast across the Site. Water was encountered during drilling at approximately 2 mbgs – 3 mbgs within sandy seams in grey clay till material. The manual March 2022 are interpreted be near seasonally levels in to high-water levels. Therefore, seasonally high-water levels across the Site range from approximately 1 mbgs to 1.45 mbgs from northwest to southeast. Groundwater monitoring will continue until the end of at least Spring 2022 to confirm March 2022 levels.

#### 6.2 Groundwater Quantity

As described in Section 5.4, six (6) hour pumping tests were completed for each of the five (5) test wells. The pumping test results, and test curves are displayed in Appendix G.

Future use of the proposed development is determined to be light industrial and office space. For the development, using the OBC Table 8.2.1.3.B the proposed sewage flows are determined to be 3,750 L/day per lot. Therefore, the total sewage flows and therefore the water demand for the 22-lots will be 86,250 L/day. However, based on the recommendations of section 4.3.2 in the MECP procedure D-5-5, the minimum flow rate for each test well is 13.7 L/min. Therefore, over a six (6) hour period, the minimum volume needed to satisfy D-5-5 is 4,932 L per test well. Each well must also recover within 95% of the static water level prior to pumping within 24-hours of pumping.

Sections 6.2.1 to 6.2.6 summarize and discuss the results of each pumping test.

#### 6.2.1 <u>TW21-1</u>

TW21-1 was pumped at a rate of 22.73 lpm and the pump was set to a depth of 22.86 mbtoc. Prior to pumping, the static water level was reported to be 6.30 mbtoc. As shown in the pump test curve in Appendix G, the water level steadily declined through the 6 hours of pumping to a final water level of 6.85 mbtoc for a total drawdown of 0.55 m. Given that the top of the well screen is located at a depth of approximately 22.30 m bgs, this leaves over 15.5 m of available drawdown. After the recovery phase of the pumping test, the water level was reported to be 6.58 mbgs or approximately 96% of the original static water level.

#### 6.2.2 <u>TW21-2</u>

TW21-2 was pumped at a rate of 22.73 lpm and the pump was set to a depth of 45.11 mbtoc.

Prior to pumping, the static water level was reported to be 10.97 mbtoc. As shown in the pump test curve in Appendix G, the water level dropped steadily through the first 5 hours of pumping and then reached a point of equilibrium at a pumping level of 38.95 mbtoc. Given that the top of the well screen is located at a depth of 46.63 mbgs, this leaves in excess of 7.5 m of available drawdown at TW21-2. After the recovery phase of the pumping test, the water level was reported to be 15.81 mbgs or approximately 69% of the original static water level.

#### 6.2.3 <u>TW21-3</u>

TW21-3 was pumped at a rate of 13.63 lpm and the pump was set to a depth of 30.48 mbtoc.

Prior to pumping, the static water level was reported to be 15.54 mbtoc. As shown in the pump test curve in Appendix G, the water level steadily declined through the hour pumping test duration to a final water level of 19.07 mbtoc. Extrapolating the curve out to 1-year of continuous pumping at the test rate and given that the top of the well screen is located at a depth of 32.91 mbgs, this leaves approximately 12.91 m of available drawdown at this well location. After the recovery phase of the pumping test, the water level was reported to be 15.54 mbgs or approximately 100% of the original static water level.

#### 6.2.4 <u>TW21-4</u>

TW21-4 was pumped at a rate of 22.73 lpm and the pump was set to a depth of 42.67 mbtoc.

Prior to pumping, the static water level was reported to be 12.61 mbtoc. As shown in the pump test curve in Appendix G, the water level steadily declined throughout the first 20 minutes of pumping and then reached an equilibrium state and remained constant for the duration of the 6-hour pumping test at a level of 16.81 mbtoc. Given that the top of the screen is located approximately 89.00 mbgs, this leaves approximately 74.00 m of available drawdown at this well location. After the recovery phase of the pumping test, the water level was reported to be 12.61 mbgs or approximately 100% of the original static water level.

#### 6.2.5 <u>TW21-5</u>

TW21-5 was pumped at a rate of 22.73 lpm and the pump was set to a depth of 30.48 mbtoc.

Prior to pumping, the static water level was reported to be 21.24 mbgs. As shown in the pump test curve in Appendix G, the water level dropped 0.01 m between 0 and 1 minute of pumping and then remained constant for the remainder of the 6-hour pumping test at a level of 21.25 mbtoc. Given that the top of the well screen is located at a depth of 71.62 mbgs, there would be approximately 50.0 m of available drawdown remaining at this well after 1-year of continuous pumping at the test rate. After the recovery phase of the pumping test, the water level was reported to be 21.24 mbgs or approximately 100% of the original static water level.

#### 6.2.6 <u>Groundwater Quantity Discussion</u>

Appendix G presents the pumping test curves on a logarithmic scale for all five (5) test wells for the period of the pumping test. The slope of the curve for each well was forecasted to a period of approximately 1-year to determine the available drawdown and the long-term pumping response of the aquifer. The results of the analysis are presented in Table 6 below.

| Well                                      | TW21-1  | TW21-2        | TW21-3            | TW21-4        | TW21-5        |
|---|---|---------------|-------------------|---------------|---------------|
| Depth<br>(m)                              | 30.78   | 47.85         | 34.44             | 90.22         | 72.84         |
| Pumping Rate<br>(Ipm)                     | 22.73   | 22.73         | 22.73 13.63 22.73 |               | 22.73         |
| Pump Depth<br>(mbgs)                      | Pump Depth<br>(mbgs) 22.86                      |               | 30.48             | _1            | 42.67         |
| Material <sup>2</sup>                     | Material <sup>2</sup> Sand, gravel Sand, gravel |               | Sand, gravel Sand |               | Sand          |
| Screened<br>Interval<br>(mbgs)            | 22.30 - 30.78                                   | 46.63 - 47.85 | 32.91 – 34.44     | 89.00 - 90.22 | 71.62 – 72.84 |
| Available<br>Drawdown at<br>1-year<br>(m) | 15.10   | 7.50          | 12.91             | 74.00         | 50.08         |

#### Table 6: Summary of Pumping Test Analysis

1. Not reported on water well record.

2. As reported in water well record tag number A309223, A335252, A299793, A299789, A299790.

Overall, four (4) of five (5) wells were tested at a rate greater than the minimum MECP D.5.5. requirement of 13.7 L/min, at a rate of 22.73 L/min. Test well TW21-3 was tested at a rate of 13.63 L/min, just under the minimum flow requirement. Forecasted for a period of one year, test wells, TW21-1, TW21-3, TW21-4 and TW21-5 were estimated to have an available drawdown of greater than 7.5 mbgs.

Based on the water well records and OGS mapping, the water bearing sand and gravel units occur as early as 26 mbgs. Additional sand and gravel units occur deeper, separated by silt and clay material. The wells screened within both the shallow units (>30 mbgs) and the deeper units (>50 mbgs) meet the water quantity requirements stated in MECP Procedure D-5-5.

Therefore, all wells satisfy the MECP Procedure D-5-5 requirements for water quantity.

#### 6.3 Groundwater Quality

All test wells and monitoring wells on Site were sampled for chemical, physical, and bacteriological parameters and submitted to a licensed third-party laboratory for analysis on three (3) separate occasions. The first water quality samples were collected on July 30, 2021. Groundwater samples were taken from monitoring wells MW21-1 to MW21-5. The second water quality sampling event occurred on September 7, 2021, and test wells TW21-1 to TW21-5 were sampled. To confirm the first two sets of sampling results, all test wells and MW21-1 and MW21-2 were resampled for bacteriological parameters and nitrate and nitrate concentrations on October 7, 2021. Sampling methods are further discussed in Section 5.3.

The certificates of analysis for both sampling visits and overall sampling results are presented in Appendix H. All water quality results were compared to the Groundwater Quality Parameter Tables listed in the MECP's D-5-5 Private Wells: Water Supply Assessment guidance document.

Based on the first and second rounds of sampling, the following exceedances were noted:

- Total coliforms in all monitoring wells ranging from 700 CFU/100 mL to 3100 CFU/100 mL
- Total coliforms in all test wells ranging from 2 CFU/100 mL to 1500 CFU/100 mL
- Sodium in all test wells
- Chloride in MW21-4
- Aluminum in MW21-1 and TW21-5
- Iron in MW21-1, TW21-1, TW21-4 and TW21-5
- Manganese in all monitoring wells and all test wells except for TW21-3
- E. Coli in TW21-2

Based on the results of the first and second round of sampling, all test wells were resampled to confirm the elevated biological parameters across the Site. Monitoring wells MW21-1 and MW21-2 were also resampled for nitrate and nitrite as the concentrations at these locations were much higher than the concentrations in MW21-3 – MW21-5.

Following the third round of sampling, TW21-1, TW21-2, TW21-3, MW21-1 and MW21-2 still exceeded the MECP standards for total coliforms of 0 colony forming units per 100 mL. Since E. Coli was undetectable in all samples, it is unlikely that fecal pollution from an onsite sewage system has occurred. Although all test wells and monitoring wells were purged for a minimum of three well volumes prior to sampling and three well volumes in between sampling, the total coliforms were still present in the groundwater samples. It is possible that since the water in the deeper test wells were stagnant for a few weeks to months since drilled, bacteria formed in the casing storage water. It is recommended that the test wells be shock chlorinated and resampled for biological indicators to determine if further treatment units will be required for the future water supply well.

It should be noted that historical microbiological water quality data collected from the Township of Adjala-Tosorontio Water Supply System indicated that some samples tested positive for total coliforms but negative for E. Coli.

#### 6.3.1 <u>Groundwater Quality Discussion</u>

Overall, except for Total Coliforms, TW21-1 to TW21-5 display reasonably good water quality and meet all health-related quality criteria of D-5-5 and ODWQS. It is recommended that the future water supply wells be subjected to routine water sampling on at least an annual basis by the well owner. Sampling materials are generally available for free from the local health unit. Routine sampling will assist owners in identifying potential well contamination and maintaining potable water quality.

#### 6.4 Source Protection Considerations

A review of the Ministry of Environment, Conservation and Parks (MECP) Source Protection Information Atlas reveals the subject property is located within the Nottawasaga Valley and is regulated by the policies outlined in the South Georgian Bay Lake Simcoe Source Protection Plan (SGBLS SPA).

Source Protection Information mapping notes that the subject property is not located within a Wellhead Protection Area (WHPA), Intake Protection Zone (IPZ), Significant Groundwater Recharge

Area (SGRA) and Highly Vulnerable Aquifer (HVA). Therefore, no legally binding policies are identified in the SGBLS SPP. However, moderate to low drinking water threats are identified within the area and apply to the Site. Best management practices must be established for the duration of the activities to reduce the potential for impacted groundwater from the proposed development:

- The establishment, operation or maintenance of a system that collects, stores, transmits, treats, or disposes of sewage.
- The establishment, operation, or maintenance of a waste disposal site within the meaning of Part V of the Environmental Protection Act.
- The storage or application of agricultural source material to land.
- The handling, storage or application of commercial fertilizer to land.
- The handling, storage or application of non-agricultural source material to land.
- The handling, storage or application of pesticide to land.
- The handling, storage or application of road salt.
- The establishment, operation or maintenance of a system that collects, stores, transmits, treats or disposes of sewage.
- The handling and storage of an organic solvent.
- The handling and storage of fuel.
- The management of runoff that contains chemicals used in the de-icing of aircraft.
- The storage of snow.
- The use of land as livestock grazing or pasturing land, an outdoor confinement area or a farm-animal yard (O. Reg. 385/08, s. 3.).
- The establishment and operation of a liquid hydrocarbon pipeline.

No additional threats to local drinking water are identified in the South Georgian Bay Lake Simcoe Source Protection Plan in reference to the subject property.

#### 7.0 Onsite Sewage Impact Assessment

Municipal wastewater servicing is not available in the vicinity of the Site; therefore, it is proposed that the development will be serviced with individual onsite sewage systems. The following section provides a sewage impact assessment for the proposed development. As the proposed concept plan is to develop 22 employment lots on the Site, the assessment has been completed following the MECP's D-5-4 Procedure to assess potential groundwater impacts.

Individual onsite sewage systems typically serve one (1) employment building and are typically owned and operated by the landlord of the lot. Onsite sewage systems generally consist of a below grade septic tank, followed by a leaching bed. The leaching bed may be below or above grade, depending on the nature of the receiving soils. In some instances, advanced treatment units may be considered.

Onsite sewage systems with a total daily design sanitary sewage flow of less than 10,000 L/day are regulated by Part 8 of the Ontario Building Code. A building permit must be obtained prior to the construction of the system. Systems with sewage flows exceeding 10,000 L/day are regulated by the MECP. It is important to note that the 10,000 L/day threshold is a cumulative value that includes all the sewage systems on a property.

#### 7.1 Onsite Sewage System Design Flows

According to the concept plan prepared by MHBC (March 2022) and correspondence with MHBC, 22 lots are proposed for the Site. The total daily design sewage flow was calculated in accordance with Table 8.2.1.3.B of the Ontario Building Code, Part 8, as shown in Table 7. Sewage flows are considered maximum day flows, and are based on the proposed facility, building area, as well as number of units and unit flow for the occupancy. For sanitary design purposes, we have assumed that the units will consist of a proposed building with a maximum area of 2,000 m<sup>2</sup> and a 40 m x 50 m footprint.

| Proposed Facility<br>Description | Area<br>(m²) | Unit         | Unit Flow | Number of Units | Total Flow Per Unit<br>(L/day) |
|----------------------------------|--------------|--------------|-----------|-----------------|--------------------------------|
| Stores                           | n/a          | per employee | 75        | 50              | 3,750                          |
| Τα                               | 3,750        |              |           |                 |                                |

| Tahle 7: | Total | Maximum | Daily | Sanitary | <sup>,</sup> Desian | Flows  | for ( | Onsite S | Svetem                                  | Servicina  |
|----------|-------|---------|-------|----------|---------------------|--------|-------|----------|---|------------|
|          | 10101 | Maximum | Dany  | sannary  | Design              | 110113 |       |          | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | Schrieling |

In accordance with the OBC, it was determined that the total maximum day sanitary sewage flow for the proposed individual lots is 3,750 L/day.

#### 7.2 Onsite Sewage System Footprint

Onsite sewage systems consist of two main components, a below grade septic tank, and a leaching bed. Depending on the nature of the receiving soils, the leaching bed may be constructed in the native soils, or, if soils are poor, constructed with imported sand raised above grade. The footprint of the leaching bed increases as the percolation rate of the receiving soils increases. If the percolation rate exceeds 50 min/cm, conventional leaching beds must be constructed in imported sand and are typically raised above grade. The leaching bed is typically sized according to the maximum total sanitary sewage flow, and the T-time of the daily design underlying soils.

As indicated above, the T-time for the soils on the Site are considered to range from 20 min/cm to 50 min/cm, therefore fill-based raised leaching beds will be required.

The design T-time will be verified by each lot owner upon the time of installing their private onsite sewage system. In very poor soils, or on Sites where space for the leaching bed is constrained, advanced treatment systems may be considered. Advanced treatment systems generally consist of a type of aeration unit that precedes the leaching bed and improves the treatment of the effluent prior to discharge to the bed.

Due to the enhanced treatment prior to discharge, alternative leaching beds, such as Type A dispersal beds and shallow buried trenches may be considered. These types of systems have considerably smaller footprints than more conventional systems.

Advanced treatment technologies must demonstrate that they can consistently meet "Level IV" effluent objectives as defined by the OBC to be used with smaller types of leaching beds. The testing standard for Ontario is the CAN/BNQ 3680 standard for residential onsite wastewater treatment technologies. A number of technologies are certified to this standard, including the Waterloo Biofilter, the Norweo Hydrokinetic, and the EcoBiofilter, among others.

#### 7.3 Minimum Lot Sizing

The construction of an onsite sewage system must conform with the requirements of the OBC, which includes minimum mandatory setback distances from components of the sewage system to critical environmental and Site features. Table 8 shows the minimum mandatory OBC setback distances.

Table 8: Minimum Setback Distances for Onsite Sewage System Components

| Site Feature                | Horizontal Setback Distance<br>(m) |
|-----------------------------|------------------------------------|
| Water Well <sup>1</sup>     | 15                                 |
| Any other well <sup>2</sup> | 30                                 |
| Structure                   | 1.5                                |
| Property Line               | 3                                  |
| Surface Water Source        | 15                                 |

1. Must be equipped with a watertight casing to a depth of 6 m.

2. Only applies to "distribution pipe", not septic tanks or treatment units.

In addition to OBC setback distances the lot must also respect local zoning bylaws (Township Zoning By-Law 13-14), which include minimum front and side yard setbacks. For the purposes of this report, yard standard setback distances have been provided below based on the employment (E) zone provisions for Zone E1 and have been accounted for in the design. Table 9 outlines the minimum setback distances for buildings according to the local zoning.

| Yard Standard | Minimum Setback Distance<br>(m) |
|---------------|---------------------------------|
| Front         | 15.0                            |
| Internal Side | 5.0                             |
| External Side | 15.0                            |
| Rear          | 7.5                             |

#### 

In addition to the setback distances, the zoning bylaw permits a maximum lot coverage of 25%, which would allow for a building footprint of 2,000 m<sup>2</sup> on a 0.8 ha lot, which is the minimum allowable lot size. Therefore, the proposed maximum development area of 29.54 ha could accommodate approximately 22 lots (assuming 15 - 20% of the area is required for roads, etc.). Detailed design of the employment lands layout would be required to further refine this number.

#### 7.4 D-5-4 Assessment

The proposed development consists of 22 lots and will be a mix of industrial and commercial units. For the purposes of this report, we have assumed that the sewage systems will be individually owned. Note if the sewage systems are not individually owned, the Site would be subject to a Reasonable Use assessment in accordance with Chapter 22 of the MECP Design Guideline for Sewage Works.

Developments that consist of more than five (5) lots that will be serviced with individual onsite sewage systems are subject to the MECP Procedure D-5-4 Technical Guidelines for Individual Onsite Sewage Systems: Water Quality Impact Risk Assessment (Procedure D-5-4). This analysis evaluates the cumulative impact of the proposed sewage systems on the local groundwater regime. The potential for impacts to occur depends on the local hydrogeological setting, the volume of effluent discharged as well as the concentration of nutrients discharged in the effluent. The nutrient of concern is typically nitrate nitrogen.

Procedure D-5-4 outlines a three-step assessment process as follows.

- Step 1 Assessment considers the minimum lot size for each private lot.
  - For developments where the lot size is one hectare or larger, it is assumed that the attenuative processes will be sufficient to reduce nitrate nitrogen to an acceptable concentration below the adjacent property. If smaller lots are proposed, the assessment proceeds to Step 2.
- Step 2 System Isolation.
  - This considers the relationship between the individual onsite sewage systems and the groundwater. Developments are considered to be a low risk where it can be demonstrated that the effluent is hydrogeologically isolated from existing or potential supply aquifers. Where it cannot be demonstrated that the systems are isolated from existing or potential groundwater supplies, it is necessary to progress to the third step of the assessment.
- Step 3 If lots smaller than 1.0 ha are proposed, and system isolation cannot be demonstrated a detailed examination of contaminant loading to the groundwater must be completed.
  - A predictive contaminant attenuation calculation must be completed that demonstrates that the proposed development will not cause concentrations of nitrate nitrogen in the groundwater to exceed the Ontario Drinking Water Quality Standards (ODWQS) value of 10 mg/L at the downgradient development boundary.

As noted in Section 7.4 the minimum lot size proposed is 0.80 ha. Therefore Step 1 cannot be satisfied and we must proceed to Step 2. As discussed in Sections 4 and 6 above, hydrogeological information for the area indicates that there are both shallow and deep-water supply wells near the subject property. Therefore, the assessment must progress to Step 3, the predictive contaminant attenuation assessment. Crozier has completed a mass balance calculation to predict the concentration of nitrate nitrogen at the development boundary, using the following general assumptions, per D-5-4 guidelines:

- The concentration of nitrate in the effluent is 40 mg/L.
- The average volume of effluent generated by each building is approximately 1,500 L/day. A peaking factor of 2.5 was applied to the maximum total daily sewage flow.
- The only dilution mechanism is by infiltration of surface precipitation. An infiltration value of 200 mm/year has been assigned, based on the soils encountered on the Site (silty loam).
- Based on the assumption that the entire property area is available for dilution purposes, a background concentration of nitrate (as N) in the groundwater was calculated using the average nitrate groundwater sample concentrations from the monitoring program for the wells on the Site of 3.24 mg/L.

Using this approach, the resulting concentration of theoretical total nitrogen at the Site boundary is predicted to be 9.67 mg/L, which is below the maximum allowable concentration of 10 mg/L. Refer to Appendix I for detailed D-5-4 Impact Assessment calculations. It must be noted that this calculation is based on the development of only 22 lots, which is what can be supported on the Site with a minimum lot size of 0.8 ha, as described in the preceding section. Therefore, the proposed development of 22 lots can be serviced by individual onsite sewage systems.

There is an opportunity to decrease the effluent nitrate nitrogen loading from the Site through the implementation of nitrate treatment systems on the proposed lots, in addition to the conventional onsite sewage design recommendation. This consideration would be viable if there is limited space on a particular lot, due to the smaller sub-surface disposal footprint. Advanced Treatment Technologies of Level N-I have been certified to remove 50% total nitrogen, and Level N-II are certified for 75% nitrogen. It is proposed to use Waterloo Biofilter treatment systems or an approved equivalent advanced treatment system, as part of the development.

#### 8.0 Conclusions & Recommendations

Based on the field work and analysis completed, we can make the following conclusions.

- The general surficial geology of the Site and surrounding area is characterized by silty clay to clay silt till with stones and sand to gravel layers. The water bearing units are characterized as semi-confined in nature and are comprised of sand and gravel layers within the clayey silt to silty clay till.
- Seasonally high-water levels are expected to range from 1.0 mbgs to 1.45 mbgs from northwest to southeast across the Site. Groundwater level monitoring will continue until at least the end of Spring 2022 to confirm seasonal groundwater elevations.
- Groundwater flows generally in a northwest to southeast direction towards the tributaries of the Boyne River and the Nottawasaga River.
- Five (5) test wells were constructed and tested in accordance with MECP Procedure D.5.5 for water quantity and water quality. Based on the results of short-term pumping tests, long-term pumping test forecasting and water quality sampling, Crozier is of the opinion that all five (5) test wells are suitable for water supply at above the minimum pumping rate of 13.7 L/min on a long-term sustainable basis.

- Water quality sampling was conducted at all monitoring well and all test wells on the Site on three (3) occasions. The final round of water sampling revealed elevated total coliforms in the test wells and below the ODWQS for all other parameters listed in MECP procedure D-5-5. Crozier is of the opinion that total coliforms present in the water following sampling suggest stagnant casing storage water in the wells was not all removed and is not suggestive of fecal or alternative contamination.
- It is recommended that groundwater sampling be conducted on an annual basis by the well owners for microbiological, inorganic and organic indicators and results be compared to the ODWQS. Sampling bottles can be obtained for free through the local health unit in most municipalities.
- Source Protection Information mapping notes that the subject property is not located within a Wellhead Protection Area (WHPA), Intake Protection Zone (IPZ), Significant Groundwater Recharge Area (SGRA) or Highly Vulnerable Aquifer (HVA). Therefore, no legally binding policies are identified in the SGBLS SPP. The Owner should follow best management practices in the application, handling and storage of pesticides, fertilizers, chemicals, snow and road salt on the property.
- The estimated maximum daily sewage flows for the proposed development are determined to be 3,750 L/day per lot. Note this value was determined using a proposed land use of industrial/commercial. Individual flows will be further defined in the detailed design of individual sewage systems to be completed by others.
- Based on the soil type across the Site, a percolation time of approximately 20 min/cm to 50 min/cm was assumed and a raised fill leaching bed design for onsite sewage is required.
- The minimum lot size required for the Site is assumed to be 0.80 ha.
- Based on the groundwater sampling results to date, the average nitrate nitrogen groundwater sample concentration is approximately 3.24 mg/L across the Site.
- The impact assessment calculations show that the combined effluent discharged from all of the individual onsite sewage systems in this development will have a minimal effect on the groundwater. With a total nitrate-nitrogen concentration of 9.67 mg/L at the Site boundary. The proposal to develop 22 lots is feasible based on the impact assessment.
- Additional nitrate treatment via treatment units capable of meeting Level N-II standards is optional.

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Should you have any questions or require further information, please do not hesitate to contact the undersigned.

Respectfully submitted,

#### C.F. CROZIER & ASSOCIATES INC.

mm

Chris Gerrits, M.Sc., P.Eng. Senior Project Manager

#### C.F. CROZIER & ASSOCIATES INC.

K. Patsel

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CM/cj

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## APPENDIX A

Wells Records Summary Table

|                 | MECP WATER WELL RECORDS   |                         |                      |                 |                  |                 |   |                      |                        |           |
|-----------------|---------------------------|-------------------------|----------------------|-----------------|------------------|-----------------|---|----------------------|------------------------|-----------|
| Project Nun     | nber:                     | 1101-4125               |                      |                 |                  |                 | Address:                                | 7723 Hwy 89, J       | Alliston               |           |
| Prepared b      | y:                        | CM                      |                      |                 |                  |                 | Date completed:                         | 2021-10-13           |                        |           |
| Key<br>Number   | Well ID                   | <b>Diameter</b><br>(mm) | <b>Depth</b><br>(m)  | Static<br>Level | Pumping<br>Level | Pumping<br>Rate | Material                                | Aquifer <sup>1</sup> | Use                    | Notes     |
| 1               | 5706153                   | 762                     | 3.7                  | 1.8             | -                | 3.8             | clay/sand/clay                          | OB                   | domestic               |           |
| 2               | 5711567                   | 762                     | 9.4                  | 3.0             | 9.1              | 3.8<br>18.9     | sand/clay                               | OB<br>OB             | domestic               |           |
| 4               | 7316155                   | 32                      | 4.0                  | -               | -                | -               | sand/clay                               | OB                   | monitoring             |           |
| 5               | 5731607                   | 914                     | 10.1                 | 1.8             | -                | 11.4            | sand/clay                               | OB                   | domestic               |           |
| 6               | 5738137                   | 152                     | 73.2                 | 24.4            | 53.4             | 18.9            | clay/sand/clay                          | OB                   | domestic               |           |
| / 8             | 7308342                   | 152                     | 34.1                 | 3.0             | -4 1             | 22.7            | cidy/sana/cidy<br>sand/clay/aravel/silt | OB                   | domestic               |           |
| 9               | 5707123                   | 762                     | 5.5                  | 1.8             | 2.4              | 3.8             | clay/sand/clay                          | OB                   | domestic               |           |
| 10              | 7286387                   | 51                      | 7.6                  | -               | -                | -               | sand/silt                               | OB                   | monitoring             |           |
| 12              | 7273608                   | 152                     | 44.2                 | 10.1            | 16.8<br>45.7     | /5./            | clay/gravel                             | OB                   | domestic               |           |
| 13              | 5713324                   | 152                     | 58.5                 | 16.5            | 30.5             | 26.5            | clay/sand/gravel                        | OB                   | domestic               |           |
| 14              | 5710955                   | -                       | 45.7                 | -               | -                | -               | clay/sand                               | OB                   | testhole               |           |
| 15              | 5706290                   | 762                     | 15.2                 | 10.7            | - 19.3           | 3.8             | sand/clay                               | OB                   | domestic               |           |
| 16              | 5711820                   | 152                     | 21.3                 | 3.0             | 21.3             | 7.6             | clay                                    | OB                   | domestic               |           |
| 18              | 7311300                   | 51                      | 4.0                  | -               | -                | -               | silt/clay                               | OB                   | monitoring             |           |
| 19              | 7296621                   | 51                      | -                    | -               | -                | -               | -                                       | -                    | testhole               |           |
| 20              | 5737530                   | 762<br>51               | 7.0                  | 2.4             | 6.1              | /.6             | clay/sand                               | OB                   | domestic               |           |
| 22              | 5704559                   | 102                     | 93.3                 | 36.6            | 54.9             | 15.2            | clay/silt/sand                          | OB                   | domestic               |           |
| 23              | 5728622                   | 152                     | 53.3                 | 0.9             | 22.3             | 15.2            | clay/silt/sand                          | OB                   | domestic               |           |
| 24              | 5709038                   | 762                     | 8.5                  | 5.5             | 9.1              | 3.8             | clay/sand                               | OB                   | domestic               |           |
| 25              | 5700160                   | 914                     | <u>45.7</u><br>9.8   | 4.0             | - 41.1           | <u> </u>        | clay/sand                               | OB                   | livestock              |           |
| 27              | 7302045                   | 152                     | 31.1                 | 1.2             | -                | 56.8            | silt/clay/sand                          | OB                   | domestic               |           |
| 28              | 5715616                   | 762                     | 13.7                 | 4.6             | 9.1              | 15.2            | sand/clay/sand                          | OB                   | domestic               |           |
| <u>29</u><br>30 | 5737993                   | 152                     | 9.1                  | 3.0             | 4.6              | 36.4            | clay/sand                               | OB                   | domestic               |           |
| 31              | 7293607                   | 152                     | 33.5                 | 7.9             | 22.8             | 37.8            | clay/gravel                             | OB                   | domestic               |           |
| 32              | 5700184                   | 102                     | 28.4                 | -               | -                | -               | silt/clay/sand                          | OB                   | domestic               | artesian  |
| 33              | 5738136                   | 762                     | -                    | -               | -                | -               | -                                       | -<br>                | abandoned              |           |
| 35              | 5700190                   | 762                     | <u>4.3</u><br>9.1    | 6.1             | -                | 7.6             | clay/sand                               | OB                   | domestic               |           |
| 36              | 7136141                   | 152                     | 25.9                 | -0.6            | 4.0              | 75.7            | silt/clay/gravel                        | ОВ                   | domestic               |           |
| 37              | 5700189                   | 762                     | 5.2                  | 1.8             | -                | 7.6             | clay/sand                               | OB                   | domestic               |           |
| <u>38</u><br>39 | 5730333                   |                         | - 32.3               | -               | -                | -               | -<br>clav/sand                          | -<br>OB              | abandoned              |           |
| 40              | 5730336                   | -                       | 32.9                 | -               | -                | -               | clay/sand                               | OB                   | abandoned              |           |
| 41              | 5724683                   | 152                     | 36.0                 | 9.4             | -                | 56.8            | clay/gravel                             | OB                   | testhole               |           |
| 42              | <u>/145204</u><br>5704557 | - 127                   | - 85.3               | -               | -                | -               | -<br>clay/silt/sand/shale               | -<br>BR              | domestic               |           |
| 43              | 5711127                   | 762                     | 22.9                 | 21.3            | 21.3             | 11.4            | clay/sand                               | OB                   | domestic               |           |
| 45              | 5738501                   | 152                     | 35.0                 | 8.2             | 18.3             | 60.6            | clay/gravel                             | OB                   | domestic               |           |
| 46              | 7316154                   | 51                      | 4.0                  | -               | -                | -               | sand/clay                               | OB                   | testhole<br>monitoring |           |
| 47              | 5741375                   | 159                     | 32.0                 | 4.6             | 25.9             | 45.5            | clay/sand                               | OB                   | commercial             |           |
| 49              | 7311301                   | 152                     | 4.0                  | -               | -                | -               | silt/clay                               | OB                   | monitoring             |           |
| 50              | 7220335                   | 152                     | 8.2                  | -               | -                | -               | silt/clay                               | OB                   | monitoring             |           |
| 51              | 7296618                   | 51                      | -                    | 3.0             | - 13./           | /.6<br>_        | ciay/sana<br>-                          | OB                   | monitoring             |           |
| 53              | 5730337                   | 178                     | 54.0                 | -               | -                | -               | -                                       | -                    | abandoned              |           |
| 54              | 5741017                   | 159                     | 33.5                 | 0.0             | 3.0              | 378.5           | sand/clay/gravel                        | OB                   | domestic               |           |
| 55<br>54        | 5707022                   | 762<br>127              | 8.5                  | 1.5<br>12.8     | 7.6              | 7.6<br>37.9     | clay/sand/gravel                        |                      | domestic               | l         |
| 57              | 5711514                   | 762                     | 13.1                 | 9.8             | 17.0             | 11.4            | clay/sand                               | OB                   | domestic               |           |
| 58              | 7286388                   | 51                      | 7.6                  | -               | -                | -               | sand/silt                               | OB                   | monitoring             |           |
| 59              | 5722582                   | 152                     | 41.1                 | 9.8             | 15.2             | 56.8            | clay/sand                               | OB                   | domestic               |           |
| 60              | 7288689                   | - 152                   | 36.U<br>48.8         | - 30.3          | - 35.0           | - 75.7          | -<br>clav/aravel                        | -<br>OB              | domestic               |           |
| 62              | 5713494                   | 762                     | 20.7                 | 18.3            | 20.1             | 7.6             | clay/sand                               | OB                   | domestic               |           |
| 63              | 5704558                   | 152                     | 40.2                 | 16.5            | 18.6             | 102.2           | clay/gravel                             | OB                   | testhole               |           |
| 64<br>75        | 5740428                   | /62                     | - /.9                | 3./             |                  | /.6<br>-        | clay/gravel                             | - OR                 | aomestic               | clean out |
| 66              | <u>57</u> 07124           | 762                     | 24.4                 | 12.2            | 13.2             | 7.6             | clay/sand                               | ОВ                   | livestock              |           |
| 67              | 5708978                   | 762                     | 4.6                  | 2.1             | 2.4              | 3.8             | sand/gravel                             | OB                   | domestic               |           |
| 68              | 7324770                   | 152                     | 30.5                 | 0.0             | 10.7             | 56.8            | sand/clay/gravel                        | OB<br>na             | domestic               |           |
| 70              | 5737126                   | 152                     | 14.6                 | 4.3             | 10.7             | 30.3            | clay/graver/shale                       | OB                   | domestic               |           |
| 71              | 5710177                   | 762                     | 6.1                  | 2.4             | 9.1              | 3.8             | clay                                    | OB                   | livestock              |           |
| 72              | 5740645                   | 159                     | 38.1                 | 0.0             | 15.8             | 37.8            | sand/clay/gravel                        | OB                   | domestic               |           |
| /3<br>74        | 5707848                   | 152                     | <u>37.2</u><br>131 1 | 7.0<br>28.0     | 129 5            | 56.8<br>3.8     | sana/ciay/gravel/sand                   | OB<br>OB             | abandoned              |           |
| 75              | <u>5700</u> 187           | 762                     | 6.1                  | 1.8             | . 27.0           | 7.6             | clay/sand                               | OB                   | domestic               |           |
| 76              | 5737531                   | 102                     | -                    | -               | -                | -               | -                                       | -                    | abandoned              |           |
| 77              | 5712429                   | 762                     | 5.8                  | 2.7             | 4.6              | 7.6             | sand/clay/gravel                        | OB                   | domestic               |           |
| 70              | 5715617                   | 762                     | 13.4                 | 4.6             | 6.1              | 30<br>15.1      | sand/clay/sand                          | OB                   | domestic               |           |
| 80              | 5700185                   | 762                     | 8.5                  | 2.1             |                  | 7.6             | clay/gravel                             | OB                   | domestic               |           |
| 81              | 5704575                   | 762                     | 6.4                  | 3.0             | 5.8              | 3.8             | sand                                    | OB                   | domestic               |           |
| 82<br>83        | 5721236<br>5711128        | 762                     | 87.3<br>23.8         | 22.6            | 33.5             | 11.4            | ciay/sana<br>clav/sand                  | OB                   | commercial             |           |
|                 | 27 1 1 1 20               | ,                       | _0.0                 |                 |                  |                 |   |                      |                        | 1         |

| Key<br>Number | Well ID            | <b>Diameter</b><br>(mm) | <b>Depth</b><br>(m) | Static<br>Level<br>(mbgs) | Pumping<br>Level   | Pumping<br>Rate | Material                 | Aquifer <sup>1</sup> | Use                     | Notes       |
|---------------|--------------------|-------------------------|---------------------|---------------------------|--------------------|-----------------|--------------------------|----------------------|-------------------------|-------------|
| 84            | 5740908            | 152                     | 35.0                | 0.9                       | 12.0               | 56.8            | gravel/clay/sand         | ОВ                   | industrial,<br>domestic |             |
| 85            | 7284222            | -                       | -                   | -                         | -                  | -               | -                        | -                    | abandoned               |             |
| 86            | 7296620            | 51                      | -                   | -                         | -                  | -               | -                        | OB                   | monitoring              |             |
| 87            | 7313430            | 152                     | 15.2                | 1.2                       | 8.2                | 37.8            | clay/sand                | OB                   | domestic                |             |
| 88            | 5724682            | 152                     | 39.0                | 7.0                       | 07.4               | 75.7            | clay/gravel/sand         | OB                   | domestic                |             |
| 89            | 7293715            | 152                     | 39.3                | 13.4                      | 27.4               | 37.8            | <u>clay/gravel/shale</u> | OB                   | domestic                |             |
| 90            | 5/3/5/4            | 152                     | 76.2                | 22.3                      | 44.1               | 18.9            | cidy/gravei/sana         | OB                   | domestic                |             |
| 91            | /3151/9            | 60                      | 38.4                | 0.0                       | -                  | - 7/            | cidy/silf/sand           | OB                   | demostic                |             |
| 92            | 5720207            | 762                     | 26.5                | 7.1<br>1.8                | <u>15.2</u><br>9.1 | 7.0<br>11.4     |                          | OB                   | domestic                |             |
| 94            | 5710179            | 762                     | 12.2                | 21                        | 2.1                | 3.8             |                          | OB                   | domestic                |             |
| 95            | 5704555            | 457                     | 12.2                | 2.1                       | 2./                | 5.0             | clay                     | OB                   | livestock               |             |
| <u>96</u>     | 5714465            | 152                     | 85.0                | 20.4                      | 21.3               | 22.7            | clay/silt/aravel         | OB                   | domestic                |             |
| 97            | 7321112            | 152                     | 62.5                | 9.8                       | 19.8               | 75.7            | clay/silt/aravel         | OB                   | domestic                |             |
| 98            | 5713493            | 762                     | 27.4                | 12.2                      | 27.4               | 3.8             | clay/gravel              | OB                   | domestic                |             |
| 99            | 5707427            | 762                     | 24.4                | 10.4                      |                    | 3.8             | clay                     | OB                   | domestic                |             |
| 100           | 5720903            | 762                     | 8.5                 | 0.9                       | 7.9                | 22.7            | clay/sand                | OB                   | domestic                |             |
| 101           | 5739706            | 159                     | 30.8                | 0.0                       | 12.2               | 37.9            | clay/gravel              | OB                   | domestic                |             |
| 102           | 5740295            | 159                     | 38.1                | 3.7                       |                    | 94.6            | clay/gravel              | OB                   | commercial              |             |
| 103           | 5705651            | 152                     | 28.0                | 6.1                       | 7.6                | 56.8            | clay/gravel              | OB                   | domestic                |             |
| 104           | 5737385            | -                       | -                   | -                         | -                  | -               | -                        | -                    | -                       | replacement |
| 105           | 5704561            | 762                     | 23.8                | 15.8                      |                    | 11.4            | gravel/clay/sand         | OB                   | commercial              |             |
| 106           | 5731574            | 152                     | 50.3                | 2.1                       | 47.2               | 75.7            | clay/gravel/silt         | OB                   | irrigation              |             |
| 107           | 5/362/5            | 152                     | 64.0                | 24.4                      | 57.9               | 22./            | clay/sand                | OB                   | domestic                |             |
| 108           | 5/3/532            | -                       | -                   | -                         | -                  | -               | -                        | -                    | abandoned               |             |
| 109           | 57315/5            | 152                     | 30.5                | 0.3                       | 16.2               | 37.8            | sana/ciay/silf           | OB                   | aomestic                |             |
| 110           | 7311302            | 70Z                     | 10.3                | 4.0                       | 10./               | ZZ./            |                          | OB                   | monitoring              |             |
| 112           | 5712225            | 762                     | 17.7                | 13.7                      | 16.0               | - 7.6           |                          | OB                   | domestic                |             |
| 112           | 7220826            | 51                      | 7.6                 | -                         | -                  | -               | sand/silt/aravel         | OB                   | monitoring              |             |
| 114           | 5700164            | 51                      | 30.8                | 4.0                       | _                  | _               | clay/silt/sand           | OB                   | testhole                |             |
| 115           | 7286385            | 51                      | 7.6                 | -                         | _                  | -               | sand/silt/clay           | OB                   | monitoring              |             |
| 116           | 5700161            | 51                      | 33.8                | 4.0                       | 6.7                | 113.6           | clay/sand/gravel         | OB                   | testhole                |             |
| 117           | 5737576            | 152                     | 26.5                | 0.3                       | 6.1                | 151.0           | sand/silt/gravel         | OB                   | domestic                |             |
| 118           | 5719005            | 762                     | 14.0                | 1.5                       | 12.8               | 22.7            | clay/sand                | OB                   | domestic                |             |
| 119           | 5704556            | 152                     | 37.8                | 14.6                      | 14.9               | 37.8            | clay/sand/gravel         | OB                   | domestic                |             |
| 120           | 5732118            | 152                     | 29.6                | 4.3                       | 340.7              | 56.8            | clay/silt/sand           | OB                   | domestic                |             |
| 121           | 7136135            | 152                     | 73.2                | 25.0                      | 49.4               | 11.4            | clay/silt/gravel         | OB                   | domestic                |             |
| 122           | 7270103            | -                       | -                   | -                         | -                  | -               | -                        | -                    | abandoned               |             |
| 123           | 7311299            | 51                      | 3.0                 | -                         | -                  | -               | silt/clay                | OB                   | monitoring              |             |
| 124           | 5/30332            | -                       | 29.0                | -                         | -                  | -               | -                        | -                    | abandoned               |             |
| 125           | 5734028            | 254                     | 31.4                | 13.1                      | 23.8               | 22./            | cidy/gravel/sand         | OB                   | domestic                |             |
| 120           | 3/12689<br>7204410 | /62                     | 9.8                 | 3./                       | 9.1                | 7.0             | cidy/sdnd                | Ов                   | abandonod               |             |
| 127           | 5714460            | - 762                   | - 11.3              | - 19                      | 10.4               | -<br>22 7       | sand/clay                |                      | domestic                |             |
| 120           | 5740429            | -                       | -                   | -                         | -                  |                 | -                        | -                    | abandoned               |             |
| 130           | 5713659            | 762                     | 21.6                | 7.6                       | 21.6               | 38              | clay/sand                | OB                   | domestic                |             |
| 131           | 5722026            | 762                     | 17.1                | 3.0                       | 15.2               | 11.4            | clay/sand                | OB                   | domestic                |             |
| 132           | 5720208            | 762                     | 14.3                | 2.7                       | 13.7               | 3.8             | clay/aravel              | OB                   | domestic                |             |
| 133           | 7284221            | -                       | -                   | -                         | -                  | -               | -                        | -                    | abandoned               |             |
| 134           | 7286389            | 51                      | 7.6                 | -                         | -                  |                 | sand/silt                | OB                   | monitoring              |             |
| 135           | 5700188            | 762                     | 10.7                | 7.6                       |                    | 7.6             | gravel/clay              | OB                   | domestic                |             |
| 136           | 5712683            | 762                     | 15.2                | 9.1                       | 14.6               | 7.6             | clay/sand                | OB                   | domestic                |             |
| 137           | 7286739            |                         | -                   | -                         | -                  | -               | -                        | -                    | abandoned               |             |
| 138           | 5705977            | 762                     | 11.6                | 4.0                       | 7.6                | 5.7             | sand/clay                | OB                   | commercial              |             |
| 139           | 7185449            | 152                     | 24.4                | 0.0                       | 15.5               | 15.1            | clay/sand                | OB                   | domestic                |             |
| 140           | 5713180            | 762                     | 22.9                | 2.1                       | 18.3               | 26.5            | clay                     | OB                   | domestic                |             |
| 141           | 5/36799            | 152                     | /3.5                | 20.1                      | 48.8               | 113.5           | sand/clay/gravel         | OB                   | domestic                |             |
| 142           | /165494            | 152                     | 25.9                | 0.0                       | 4.6                | 56.8            |                          | OR                   | domestic                |             |
| 143           | /3113/4            | 152                     | 51.5<br>0F.0        | 1.5                       | 7.3<br>1 E 1       | 11.4            | sana/ciay/gravel/silt    | OR                   | domestic                |             |
| 144           | 5702007            | 152                     | 20.7<br>02 0        | 3.4<br>1 0                | 13.1<br>017        | 3/.8<br>22.7    | clay/sand/araya          |                      | domostic                |             |
| 143           | 5700250            | 12/                     | 20.2<br>94 N        | 1.0<br>2.1                | ∠1.0<br>5.0        | 22.1<br>56 Q    | clay/sund/gravel         |                      | domestic                |             |
| 140           | 7279993            | 1.52                    | 38.1                | _1 5                      | 9.2                | 7.5 7           | sand/clay                | OB                   | domestic                |             |
| 148           | 5713657            | 762                     | 12.5                | 2.4                       | 12.2               | 76              | sand/clav                | OB                   | domestic                | 1           |
| 149           | 7296622            | -                       | -                   | -                         | -                  | -               | -                        | -                    | monitorina              |             |
| 150           | 5730339            | - 1                     | 54.9                | -                         | -                  | - 1             | clay/sand                | OB                   | abandoned               |             |
| 151           | 5733374            | 152                     | 36.6                | 4.3                       | 33.5               | 37.8            | clay/gravel              | OB                   | commercial              |             |
| 152           | <u>570</u> 6313    | 762                     | 13.7                | 9.1                       | 12.2               | 7.6             | sand                     | ОВ                   | domestic                |             |
| 153           | 5731976            | 152                     | 15.8                | 1.8                       | 13.7               | 56.8            | clay/sand/silt           | OB                   | domestic                |             |
| 154           | 5700163            | 102                     | 30.8                | 4.0                       | 9.1                | 10.2            | clay/silt/sand           | OB                   | testhole                |             |
| 155           | 5700162            | 51                      | 30.8                | 3.7                       | -                  | -               | clay/silt/sand           | OB                   | testhole                |             |
| 156           | 5707428            | 762                     | 29.0                | -                         | -                  | -               | clay                     | OB                   | abandoned               |             |

1. OB - Overburden BR - Bedrock

# APPENDIX B

Monitoring Well Logs



## WELL CONSTRUCTION REPORT (WELL #21-1)

#### REPORT NO.: 1 of 5

| PROJECT #: 1101-4125 PROJECT NAME: 7723 HWY 89 |                                  | WEATHER: 25         | °C, Sunny            |
|--|----------------------------------|---------------------|----------------------|
| DATE: June 7, 2021                             | CONTRACTOR: Walker Drilling Ltd. | PHOTOS: Yes         |                      |
| LOCATION: Alliston, Ontario                    |                                  | ON SITE:<br>8:00 AM | OFF SITE:<br>4:30 PM |
| CFCA REPRESENTATIVE: Evan Finl                 | woc                              | WELL SPECIFI        | С                    |
|  |                                  | START:              | END:                 |
| SITE VISITORS: Caitlyn MacPhee,                | Chris Gerrits, Alex Laleva       | 8:45 AM             | 10:00 AM             |

| EQUIPMENT & LABOUR ON SITE: | HOURS | EQUIPMENT & LABOUR ON SITE: | HOURS |
|-----------------------------|-------|-----------------------------|-------|
| Service Truck               | 7.5   | Operator (1)                | 7.5   |
| Drill Rig                   | 7.5   | Assistant (1)               | 7.5   |

WORK COMPLETED:

Well Cover

| ITEM :         | DESCRIPTION:                                      |         | LOC  | ATION:                              |            |
|----------------|---|---------|------|-------------------------------------|------------|
| Well #21-1     | Most easterly location.<br>Adjacent Concession 7. |         | ~20m | n W of Concession 7 C/L, ~295m S of | HWY 89 C/L |
| MATERIAL USED: | 0   |         |      |                                     |            |
| 11E/M.         | Q   | UANIII. |      | 11E/VI.                             | QUANIIT.   |
| Cone           |   | 1       |      | J Plug                              | 1          |
| 10 Foot Screen |   | 1       |      | Cement (Bag)                        | 1          |
| Riser (10ft)   |   | 1.2     |      | Well Sand (50lbs Bag)               | 4          |
|                |   |         |      |                                     |            |

1

Bentonite (50lbs Bag)

2



GEOLOGY:

| SOIL CLASIFICATION:   | DEPTH:    |
|---|-----------|
| SANDY-SILT: Brown, dry, loose W/ trace clay, and organics.                                    | 0-2 ft.   |
| SILTY-CLAY: Brownish grey, low moisture, dense, plastic W/<br>trace sand.                     | 2-4 ft.   |
| SILTY-CLAY TILL: Light brown, low moisture, very stiff W/<br>rounded gravel and trace sand.   | 5-7 ft.   |
| CLAY TILL: Brown, moist, dense, plastic W/ some silt, trace<br>rounded gravel and trace sand. | 7-9 ft.   |
| CLAY TILL: Brown, moist, dense, plastic W/ some silt, trace<br>rounded gravel and trace sand. | 10-12 ft. |
| SAND: Brown, medium, wet.   | 14-16 ft. |
| SAND: Brown, medium, moist, very dense, W/ trace<br>gravel.                                   | 18-20 ft. |
|   |           |
|   |           |
|   |           |

REMARKS:

- Sand pack at 8 ft.
- Water noted in bottom of borehole upon completion at 20 ft.
- Screen (10 ft.) installed at 20 ft.



## WELL CONSTRUCTION REPORT (WELL #21-2)

#### REPORT NO.: 2 of 5

| PROJECT #: 1101-4125 PROJECT NAME: 7723 HWY 89 |                                  | WEATHER: 25°C       | C, Sunny             |  |
|--|----------------------------------|---------------------|----------------------|--|
| DATE: June 7, 2021                             | CONTRACTOR: Walker Drilling Ltd. | PHOTOS: Yes         |                      |  |
| LOCATION: Alliston, Ontario                    |                                  | ON SITE:<br>8:00 AM | OFF SITE:<br>4:30 PM |  |
| CFCA REPRESENTATIVE: Evan Finb                 | w                                | WELL SPECIFIC       |                      |  |
|  |                                  | START:              | END:                 |  |
| SILE VISITORS: Califlyn MacPhee, C             | nris Gerrits, Alex Laleva        | 10:15 AM            | 12:00 PM             |  |

| EQUIPMENT & LABOUR ON SITE: | HOURS | EQUIPMENT & LABOUR ON SITE: | HOURS |
|-----------------------------|-------|-----------------------------|-------|
| Service Truck               | 7.5   | Operator (1)                | 7.5   |
| Drill Rig                   | 7.5   | Assistant (1)               | 7.5   |

WORK COMPLETED:

| ITEM :     | DESCRIPTION:              | LOCATION:  |
|------------|---------------------------|--|
| Well #21-2 | Central location of site. | ~345m W of Concession 7 C/L, ~285m S of HWY 89 C/L |

MATERIAL USED:

| ITEM:          | QUANTITY: | ITEM:                 | QUANTITY: |
|----------------|-----------|-----------------------|-----------|
|                |           |                       |           |
| Cone           | 1         | J Plug                | 1         |
|                |           |                       |           |
| 10 Foot Screen | 1         | Cement (Bag)          | 1         |
|                |           |                       |           |
| Riser (10ft)   | 1.2       | Well Sand (50lbs Bag) | 4         |
|                |           |                       |           |
| Well Cover     | 1         | Bentonite (50lbs Bag) | 2         |



GEOLOGY:

| DEPTH:    | SOIL CLASIFICATION:   |
|-----------|---|
| 0-2 ft.   | 4" SEAM > SILTY ORGANICS: Dark brown, low moisture,<br>loose.                     |
|           |   |
|           | CLAYEY-SILT: Greyish brown, low moisture, loose W/ trace                          |
|           | sand, and organics.   |
| 2-4 ft.   | CLAY TILL: Brownish grey, low moisture, dense, plastic W/<br>some rounded gravel. |
| 5-7 ft.   | CLAY TILL: Brownish grey, low moisture, dense, plastic W/<br>some rounded gravel. |
|           | 4" SEAM > SAND: Grey, low moisture, dense.  |
| 7-9 ft.   | CLAY TILL: Brownish grey, low moisture, dense, plastic W/<br>some rounded gravel. |
| 10-12 ft. | CLAY TILL: Dark grey, dry, dense, stiff W/ some rounded gravel and trace sand.    |
| 14-16 ft. | CLAY TILL: Dark grey, dry, dense, stiff W/ some rounded gravel and trace sand.    |
| 18-20 ft. | CLAY TILL: Dark grey, dry, dense, stiff W/ some rounded gravel and trace sand.    |
|           |   |
|           |   |
|           |   |

#### **REMARKS:**

- Sand pack at 8 ft.
- Water noted in bottom of borehole upon completion at 20 ft.
- Screen (10 ft.) installed at 20 ft.



## WELL CONSTRUCTION REPORT (WELL #21-3)

#### REPORT NO.: 3 of 5

| PROJECT #: 1101-4125              | PROJECT NAME: 7723 HWY 89        | WEATHER: 25°C,      | Sunny                |
|-----------------------------------|----------------------------------|---------------------|----------------------|
| DATE: June 7, 2021                | CONTRACTOR: Walker Drilling Ltd. | PHOTOS: Yes         |                      |
| LOCATION: Alliston, Ontario       |                                  | ON SITE:<br>8:00 AM | OFF SITE:<br>4:30 PM |
| CFCA REPRESENTATIVE: Evan Finbo   | W                                | WELL SPECIFIC       |                      |
|                                   |                                  | START:              | END:                 |
| SITE VISITORS: Caitlyn MacPhee, C | Chris Gerrits, Alex Laleva       | 12:30 PM            | 1:30 PM              |

| EQUIPMENT & LABOUR ON SITE: | HOURS | EQUIPMENT & LABOUR ON SITE: | HOURS |
|-----------------------------|-------|-----------------------------|-------|
| Service Truck               | 7.5   | Operator (1)                | 7.5   |
| Drill Rig                   | 7.5   | Assistant (1)               | 7.5   |

WORK COMPLETED:

| ITEM :     | DESCRIPTION:  | LOCATION:   |
|------------|---|---|
| Well #21-3 | Near old farmhouse and barn, central portion of site. | ~375m W of Concession 7 C/L, ~95m S of HWY 89 C/L |

MATERIAL USED:

| ITEM:          | QUANTITY: | ITEM:                 | QUANTITY: |
|----------------|-----------|-----------------------|-----------|
|                |           |                       |           |
| Cone           | 1         | J Plug                | 1         |
|                |           |                       |           |
| 10 Foot Screen | 1         | Cement (Bag)          | 1         |
|                |           |                       |           |
| Riser (10ft)   | 1.2       | Well Sand (50lbs Bag) | 4         |
|                |           |                       |           |
| Well Cover     | 1         | Bentonite (50lbs Bag) | 2         |



GEOLOGY:

| DEPTH:    | SOIL CLASIFICATION:  |
|-----------|--|
| 0-2 ft.   | SANDY-SILT: Brown, dry, loose W/ trace clay, and organics.   |
| 2-4 ft.   | SILTY-CLAY: Brownish grey, low moisture, dense, plastic W/<br>trace sand.                          |
|           | POCKETS > SAND: Loose W/ oraganics.  |
| 5-7 ft.   | CLAY TILL: Grey, low moisture, dense, plastic W/ rounded<br>gravel, trace silt, and trace sand.    |
| 7-9 ft.   | CLAY TILL: Grey, low moisture, dense, plastic W/ rounded<br>gravel, trace silt, and trace sand.    |
| 10-12 ft. | CLAY TILL: Grey, low moisture, dense, plastic W/ rounded gravel, trace silt, and trace sand.       |
| 14-16 ft. | SILTY-CLAY TILL: Brownish grey, low moisture, dense, plastic<br>W/ rounded gravel, and trace sand. |
| 18-20 ft. | SILTY-CLAY TILL: Brownish grey, low moisture, dense, plastic<br>W/ rounded gravel, and trace sand. |
|           |  |
|           |  |
|           |  |

REMARKS:

- Sand pack at 8 ft.
- No water noted in bottom of borehole upon completion at 20 ft.
- Screen (10 ft.) installed at 20 ft.



## WELL CONSTRUCTION REPORT (WELL #21-4)

#### REPORT NO.: 4 of 5

| PROJECT #: 1101-4125              | PROJECT NAME: 7723 HWY 89        | WEATHER: 25%        | C, Sunny             |
|-----------------------------------|----------------------------------|---------------------|----------------------|
| DATE: June 7, 2021                | CONTRACTOR: Walker Drilling Ltd. | PHOTOS: Yes         |                      |
| LOCATION: Alliston, Ontario       |                                  | ON SITE:<br>8:00 AM | OFF SITE:<br>4:30 PM |
| CFCA REPRESENTATIVE: Evan Finbe   | WC                               | WELL SPECIFIC       | ;                    |
|                                   |                                  | START:              | END:                 |
| SITE VISITORS: Caitlyn MacPhee, C | hris Gerrits, Alex Laleva        | 2:00 PM             | 4:00 PM              |

| EQUIPMENT & LABOUR ON SITE: | HOURS | EQUIPMENT & LABOUR ON SITE: | HOURS |
|-----------------------------|-------|-----------------------------|-------|
| Service Truck               | 7.5   | Operator (1)                | 7.5   |
| Drill Rig                   | 7.5   | Assistant (1)               | 7.5   |

WORK COMPLETED:

| ITEM :         | DESCRIPTION:                   |                | LOC | CATION:                      |           |
|----------------|--------------------------------|----------------|-----|------------------------------|-----------|
| Well #21-4     | Northwest cor<br>subject prope | ner of<br>rty. | NW  | Corner, ~45m S of HWY 89 C/L |           |
| MATERIAL USED: |                                |                |     |                              |           |
| ITEM:          |                                | QUANTITY:      |     | ITEM:                        | QUANTITY: |
| Cone           |                                | 1              |     | J Plug                       | 1         |
| 10 Foot Screen |                                | 1              |     | Cement (Bag)                 | 1         |
| Riser (10ft)   |                                | 1.2            |     | Well Sand (50lbs Bag)        | 4         |
| Well Cover     |                                | 1              |     | Bentonite (50lbs Bag)        | 2         |



GEOLOGY:

| DEPTH:    | SOIL CLASIFICATION:  |
|-----------|--|
| 0-2 ft.   | SANDY-SILT: Brown, dry, loose W/ trace clay, and organics.   |
| 2-4 ft.   | SILTY-CLAY: Brown, low moisture, dense, plastic W/ trace sand.   |
| 5-7 ft.   | CLAY TILL: Brown, low moisture, dense, plastic W/ rounded gravel, trace silt, and trace sand.                            |
| 7-9 ft.   | SILT TILL: Greyish brown, low moisture, dense, stiff W/<br>rounded gravel, trace cobbles, trace clay, and trace<br>sand. |
| 10-12 ft. | SILT TILL: Grey, wet, compact, dilatant W/ rounded gravel,<br>trace clay, and trace sand.                                |
| 14-16 ft. | SILT TILL: Grey, wet, compact, dilatant W/ rounded gravel,<br>trace clay, and trace sand.                                |
| 18-20 ft. | CLAYEY-SILT TILL: Dark grey, low moisture, very dense, stiff<br>W/ rounded gravel, trace cobbles, and trace sand.        |
|           |  |
|           |  |
|           |  |

REMARKS:

- Sand pack at 8 ft.
- No water noted in bottom of borehole upon completion at 20 ft.
- Screen (10 ft.) installed at 20 ft.



## WELL CONSTRUCTION REPORT (WELL #21-5)

#### REPORT NO.: 45 of 5

| PROJECT #: 1101-4125              | PROJECT NAME: 7723 HWY 89        | WEATHER: 28°C,      | Sunny                 |
|-----------------------------------|----------------------------------|---------------------|-----------------------|
| DATE: June 8, 2021                | CONTRACTOR: Walker Drilling Ltd. | PHOTOS: Yes         |                       |
| LOCATION: Alliston, Ontario       |                                  | ON SITE:<br>8:30 AM | OFF SITE:<br>12:00 PM |
| CFCA REPRESENTATIVE: Evan Finba   | WC                               | WELL SPECIFIC       |                       |
|                                   |                                  | START:              | END:                  |
| SITE VISITORS: Caitlyn MacPhee, C | chris Gerrits, Alex Laleva       | 9:00 AM             | 11:30 AM              |

| EQUIPMENT & LABOUR ON SITE: | HOURS | EQUIPMENT & LABOUR ON SITE: | HOURS |
|-----------------------------|-------|-----------------------------|-------|
| Service Truck               | 3.5   | Operator (1)                | 3.5   |
| Drill Rig                   | 3.5   | Assistant (1)               | 3.5   |

WORK COMPLETED:

| ITEM :         | DESCRIPTION:                          |           | LOCATION:                        |                       |           |
|----------------|---------------------------------------|-----------|----------------------------------|-----------------------|-----------|
| Well #21-5     | Southwest corner of subject property. |           | SW Corner, ~475m S of HWY 89 C/L |                       |           |
| MATERIAL USED: |                                       |           |                                  |                       |           |
| ITEM:          |                                       | QUANTITY: |                                  | ITEM:                 | QUANTITY: |
| Cone           |                                       | 1         |                                  | J Plug                | 1         |
| 10 Foot Screen |                                       | 1         |                                  | Cement (Bag)          | 1         |
| Riser (10ft)   |                                       | 1.2       |                                  | Well Sand (50lbs Bag) | 4         |
| Well Cover     |                                       | 1         |                                  | Bentonite (50lbs Bag) | 2         |



GEOLOGY:

| DEPTH:    | SOIL CLASIFICATION:  |
|-----------|--|
| 0-2 ft.   | SILTY-SAND: Brown, medium, moist, compact W/ some clay, and organics.          |
| 2-4 ft.   | SILTY-CLAY: Brown, low moisture, dense, plastic W/ trace sand.                 |
| 5-7 ft.   | SILTY-CLAY: Brown and grey, low moisture, dense, stiff W/<br>trace sand.       |
| 7-9 ft.   | SILTY-CLAY TILL: Grey, dry, dense, stiff W/ rounded gravel,<br>and trace sand. |
| 10-12 ft. | SILTY-CLAY TILL: Grey, dry, dense, stiff W/ rounded gravel,<br>and trace sand. |
| 14-16 ft. | SILTY-CLAY TILL: Grey, dry, dense, stiff W/ rounded gravel,<br>and trace sand. |
| 18-20 ft. | SILTY-CLAY TILL: Grey, dry, dense, stiff W/ rounded gravel,<br>and trace sand. |
|           |  |
|           |  |
|           |  |

#### REMARKS:

- Sand pack at 8 ft.
- No water noted in bottom of borehole upon completion at 20 ft.
- Screen (10 ft.) installed at 20 ft.
# ${}^{\text{APPENDIX}} C$

Water Well Records for Test Wells TW1 – TW5

|  |  | Conse  | rvation and  | I Parka   | Та  | a#:A309  | 223  | Andelas  | Regulatio  | on 903   | Ontario I  | Water R  | esource  |
|--|--|--|--|---|---|--|--|--|--|--|--|--|--|
| Measure  | ementa recer   | ded in: p  | Metric   | 🗌 Imperial  | 14  | 9  |  | ASOLD  | 3  |  | Pa   | ge   |  |
| First Nat  | wner's Inte  | ormation   | 11 and Name  | Denanutate  | -   |  | 1913   | E-mail Address   |  |  |  |  | Conto  |
|  | Joe  |  | Pi   | la (  | Pilla 1   | vestments  | (no)   | E-mail Hotal sala  |  |  |  | by V   | Val Own  |
| Mailing A  | Address (Stree   | It Number/N  | tame)  |   |   | Municipality   |  | Province   | Postal Cod   | 0-   | Telephon   | e No (in   | c anas co  |
| Well Lo  | ocation  | Hwy  | 10   | 1000  |   | Mono   |  | ON   | LINS   | 140  |  | 1  | 111  |
| Address  | of Well Locati   | on (Street N   | lumber/Nam   | e)  | 100   | Township   | -  |  | Lot  |  | Concess  | ion  |  |
| County/  | District Municip   | grulay   | 89   |   |   | Ad:  | ala  |  | 31   | Prov   | ince   | Post   | al Code  |
| -  | 5  | imcoe  | 2  |   |   | Alla   | itan   |  |  | On   | tario  | 19   | RI   |
| UTM Col  | D 8 3  | e Easting  | anul   | Northing  | 00  | Municipal Plan and   | Sublot No  | umber  |  | Ofhe   | br.  |  |  |
| Overbu   | rden and Be  | drock Mat  | erials/Aban  | donment S   | lealing Rec   | ard (see instruction   | on the be  | ick of this form)  | ALC: NOT   | -  |  |  |  |
| General  | Colour   | Most Cor   | mmon Mater   | ial   | 0   | ther Materials   |  | Gene   | eral Description   | n  |  | De<br>From   | pth (m/t   |
| Bro  | new  | Top  | 50.  |   |   | 1. 1.  | 1  |  |  |  |  | 0  | .3   |
| Bro  | nwn  | cle  | auf  |   | 1111111   |  |  |  |  | 1  |  | .3   | 3.   |
| Bra  | 20   | ck   | ay   | had   | 5   | tones  |  |  | •  |  |  | 3.35   | 7.6  |
| Bra  | aun  | san  | al -   | 11  | 5   | silt   |  |  |  |  |  | 7.62   | 9.1  |
| Brea   | wn   | san  | d  |   |   |  | -  |  |  | -  |  | 9.14   | 13   |
| Grey   | 1  | cla  | 4.   |   | St  | ones   |  |  |  |  |  | 13.10  | to.  |
| Bro  | neve   | sar  | d  |   | q   | avel   |  |  |  |  |  | 2651   | 3.   |
| Bra  | new  | gra  | vel  | 6-1-  | 5   | and  |  | Serve Harman   |  |  |  | 31.39  | 32.  |
| -  |  |  |  |   | -   |  |  |  |  |  |  |  | -  |
| Depth :  | Set at (71)  |  | Annul<br>Type of S   | ealant Used   | 0.3   | Volume Place   |  | er test of well vield  | Results of We<br>water was:  | oll Yie  | taw Down   | R  | ecovery  |
| From   | To   |  | (Material  | and Type)   | -   | (Chr)  | 0  | Clear and sand fr  | 00   | Time<br>(min)  | Water Lev  | el Time<br>(min)   | Water Lo   |
| 0  | 6.4  | -  | Bento  | nite  |   | .21  |  | untping discontinue  | d, give reason:  | Static   | 620  |  |  |
|  |  |  |  |   |   |  | _  |  |  | 1  | 650  | 1  | 662  |
|  | -  |  |  |   |   | 197.00   | Pur  | mp intake set at 💮   | n)   | 2  | 1.51   | 2  | 64   |
|  |  |  | 1 8  |   |   | 113.24   |  | 28:34  |  | 3  | 1.00   | 3  | 6.4  |
| Met<br>Cable 1   | thod of Cor  | Intruction   | 1  | huble   | Well Us   | e foi  | Pur  | 22.73  | -141)  | 4  | 100  | 4  | 1.1.1  |
| Rotary   | (Conventional)   |  |  | omestic   | Municipi  | al Dewate  | ing Dur  | ration of pumping  |  | 5  | 6.00   | E  | 6.61   |
| A Dates  | (represse)   | Driving  |  | ivestock<br>tigatión  | Coolina   | e 🗍 Monita<br>& Air Canditioning   | ng   | al water level end of  | pumping @m   | 10   | 6.50   |  | 6.6  |
| Boring   |  | L) Ligging   | 1  | the second s  |   |  | 11   |  |  | 10   | 6.00   | 10   | 6.61   |
| Boring   | specify  |  |  | dustrial<br>ther, specify   |   |  |  | 6.85   |  | 15   | 1 -  | 15   |  |
| Rotary       Boring     Air perce     Other, sp  | pecity<br>Con  | struction I  | Record - Ca  | idustrial<br>ther, specify<br>ising   |   | Status of We   | If flo   | 6.85<br>wing give rate (Immi   | (GPM)  | 15   | 6.59   | 15   | 6.6  |
| Rotary (<br>Boring<br>Air perci<br>Other, s<br>Inside<br>Diameter  | Open Hale<br>(Galvanized   | struction f<br>OR Material   | Record - Ca<br>Wat<br>Thippness  | idustriat<br>ther, specify<br>ustrig<br>Dept  | h (m/ll)  | Status of We   | Rec  | 6.85<br>wing give rate (times<br>commended pump d  | (GPM)<br>epth (GR)   | 15<br>20   | 6.59   | 15<br>20   | 6.60   |
| I Rotary (<br>Boring<br>Air perc<br>Other, s<br>Inside<br>Diameter<br>(onvin)  | Ópen Hale<br>(Galvanized<br>Concrete, P  | Struction F<br>OR Material<br>( Fibreglass,<br>lastic, Silcel)   | Wat<br>Thickness   | dustrial<br>ther, specify<br>Ising<br>Dept<br>From  | ћ (m/tt)<br>То  | Status of Wei<br>Water Supply<br>Replacement W   | If flo<br>Rec  | 6.85<br>wing give rate (times<br>commended pump d<br>28.34   | rGPM)<br>epth (G)II)   | 15<br>20<br>25   | 6.59   | 15<br>20<br>25   | 6.60   |
| Inside   | Open Hole<br>(Galvarized<br>Concrete, P  | struction f<br>OR Material<br>( Fibreglass,<br>iastic, Steel)  | Record - Ca<br>Wal<br>Thiones<br>On)<br>.4771  | idustrial<br>ther, specify<br>isting<br>Dept<br>From<br>+,45  | n (m/l)<br>To<br>31.64  | Status of Wei<br>Water Supply<br>Replacement W<br>Stest Hole<br>Recharge Weil<br>Dewatering Weil   | Rec  | 6.85<br>wing give rate (times<br>commended pump d<br>38.34<br>primended pump ta<br>gorenaled pump ta<br>gorenaled pump ta  | rGPM)<br>epth (()(1)<br>ite  | 15<br>20<br>25<br>30   | 6.59<br>6.60<br>6.61   | 15<br>20<br>25<br>30   | 6.60<br>6.60<br>6.60   |
| Air perc<br>Cother, si<br>Diameter<br>(crtvfs)<br>15.24<br>10.16   | Open Hale<br>(Galvanized<br>Concrete, P<br>Steel +   | struction f<br>OR Material<br>(Fibreglass,<br>instr. Stee)<br>21<br>K Rocker   | Record - Ca<br>Wat<br>Theress<br>On)<br>.471<br>.471   | idustrial<br>ther, specify<br>ising<br>Dept<br>From<br>+, 45<br>24.87   | n (m/tt)<br>To<br>31.64<br>30.78  | Status of Wel Water Supply Replacement W Fast Hole Recharge Well Dewatering Well Observation and Montione Hele   | If flo<br>Rec<br>Rec<br>Weil   | 6.85<br>wing give rate (times<br>ommended pump d<br>38.34<br>gramended pump ra<br>GCPM)<br>45.46<br>I production (timesGF  | rGPM)<br>epth @It)<br>ite<br>M)  | 15<br>20<br>25<br>30<br>40   | 6.59<br>6.59<br>6.60<br>6.61<br>6.62                                 | 15<br>20<br>25<br>30<br>40   | 6.60<br>6.60<br>6.60<br>6.60   |
| Incide<br>Boring<br>Air perc<br>Other, s<br>Diameter<br>(on/in)  | Open Hole<br>(Galvanized<br>Conrele, P<br>Steel +  | struction I<br>OR Material<br>(Birtegias,<br>lastic Steel)<br>21<br>K Rocker   | Record - Ca<br>West<br>Thickness<br>On)<br>.471<br>.471  | ising<br>Dept<br>From<br>+,45   | n (m.11)<br>To<br>31.64<br>30.78  | Status of Wei<br>Water Suppy<br>Replacement W<br>Stat Hole<br>Recharge Well<br>Dewatering Weil<br>Observation and<br>Monitoring Hole<br>Alteration<br>(Construction)   | Rep<br>Rep<br>or Weil  | 6.85<br>wing give rate (times<br>commended pump of<br>38.34<br>genmended pump ra<br>36PM)<br>45.46<br>i production (times)6F   | rGPM)<br>epth @tt)<br>tte<br>M()   | 15<br>20<br>25<br>30<br>40<br>50   | 6.59<br>6.60<br>6.61<br>6.62<br>6.63                                 | 15<br>20<br>25<br>30<br>40<br>50   | 6.60<br>6.60<br>6.60<br>6.59<br>6.59   |
| Rotary  <br>Boring<br>Ar perc<br>Other, s<br>Inside<br>Diameter<br>(cm/in)<br>IS, 34<br>IO, IG   | Con<br>Open Hole<br>(Garvanized<br>Concrete, P<br>Steel +  | struction f<br>OR Material<br>(Fibregians,<br>Instit: Steel)<br>21<br>K Parker   | Record - Ca<br>Wat<br>There are<br>On)<br>.471<br>-477   | ising<br>Brom<br>From<br>4,45   | n (m/t)<br>To<br>31.69<br>30.78   | Status of Wei<br>Water Supply<br>Replacement W<br>Test Hole<br>Dewatening Weil<br>Observation and<br>Monitoring Hole<br>Alteration<br>(Construction)   | Record   | 6.85<br>wing give rate (timer<br>ammended pump d<br>B.34<br>production (timer)GF<br>fected?<br>Yes No  | rGPM)<br>epth (()(T)<br>ite  | 15<br>20<br>25<br>30<br>40<br>50<br>60   | 6.59<br>6.59<br>6.60<br>6.61<br>6.63<br>6.63                         | 15<br>20<br>25<br>30<br>40<br>50<br>60   | 6.60<br>6.60<br>6.59<br>6.58<br>6.58   |
| Li Rotary I<br>Boring<br>Ar perce<br>Other, s<br>Inside<br>Diamber<br>(cristif)  | Constant   | struction f<br>OR Material<br>(Paregiase,<br>instr: Sleet)<br>21<br>K Recker   | Record - Ca<br>Weat<br>Therese<br>. 471<br>. 471<br>. 477  | Housing<br>Her, specify<br>Ising<br>Dept<br>From<br>4,45<br>24.87<br>1001   | n (m.11)<br>To<br>31.64<br>30.78  | Status of Wei<br>Weter Supply<br>Replacement W<br>Test Hole<br>Recharge Weil<br>Dewatering Weil<br>Dewatering Weil<br>Dewatering Weil<br>Dewatering Weil<br>Observation and<br>Montoring Hole<br>(Construction)<br>Attentione<br>(Construction)<br>Bandoned, Pool<br>Weter Observation   | If flo   | 6.25 wing give rate (time)<br>ommended pump d<br>38.34<br>gmmended pump d<br>32PM<br>45.46<br>tected?<br>Yes No  | GPM)<br>epth (Dit)<br>ite<br>Map of Wel  | 15<br>20<br>25<br>30<br>40<br>50<br>60   | 6.59<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63                         | 15<br>20<br>25<br>30<br>40<br>50<br>60   | 6.60<br>6.60<br>6.60<br>6.50<br>6.50<br>6.50                                 |
| Li Rotary I<br>Boring<br>Ar pero<br>Other, s<br>Dameter<br>(ornin)<br>IS-24<br>IO.16<br>Outade<br>Dameter<br>Contade<br>Dameter<br>(ornin)   | Con<br>OpenHale<br>(Gavanized<br>Contrelle, P<br>Steel +<br>Steel +<br>Mate<br>(Plastic, Carlys  | struction f<br>OR Mutural<br>(Rereptant,<br>India, Steet)<br>2<br>K Recker<br>Mruction R<br>riad<br>nized, Steet)  | Record - Sec<br>Sict No  | Hannal<br>Hor, specify<br>Ising<br>Dept<br>From<br>4, 45<br>64.87<br>Feen<br>Dept<br>From<br>Dept<br>From   | n (m/tt)<br>To<br>31.64<br>30.78  | Status of Wei<br>Weter Supply<br>Replacement W<br>East Noie<br>Recharge Weil<br>Dewatering Weil<br>Dewatering Weil<br>Dewatering Weil<br>Dewatering Weil<br>Attention<br>(Construction)<br>Attantioned<br>Insufficient Supp<br>Water Causity<br>Water Causity<br>Caustoned, other  | or Weil  | 6.25 Wing give rate (time)<br>commended pump a<br>28.34<br>genvended pump a<br>26PM<br>45.46<br>i protuction (time)GF<br>fector?<br>Yes No   | GPM)<br>opth (Dit)<br>ite<br>PM)<br>Map of Well<br>pelow following   | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>11 Loca<br>9 instru  | 6.59<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63<br><b>xiion</b>         | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>he back  | 6.60   |
| LI Rotary I<br>Bonng<br>Ar peror<br>Other, s<br>Inside<br>Dameter<br>Convention<br>IS-24<br>IO.16<br>Outside<br>Dispender<br>Dispender<br>Dispender<br>Dispender<br>Dispender<br>Dispender   | Ansion<br>pretty<br>Open Hale<br>(Gavariane<br>Controle, P<br>Steel +<br>Steel +<br>Cons<br>(Plastic, Carva  | struction f<br>OR Material<br>Fateglass,<br>inste: Stori)<br>2<br>K Recker<br>Mruction R<br>rial<br>nized, Stori)  | Resord - Ca<br>Wat<br>Thereas<br>O'n)<br>. 471<br>. 471<br>. 477<br>Stot No<br>1,2   | edustinal<br>ther, specify<br>ising<br>Dept<br>From<br>t, 45<br>SEI.87<br>Depth<br>From<br>25 1A  | n (m/tt)<br>To<br>31.64<br>30.78<br>(m/tt)<br>To<br>20.25   | Status of Wei<br>Status of Wei<br>Replacement W<br>Fast Hole<br>Recharge Veil<br>Devatering Weil<br>Devatering Weil<br>Devatering Weil<br>Devatering Weil<br>Devatering Weil<br>Devatering Weil<br>Attention<br>(Construction)<br>Abandoned.<br>Insufficient Supp<br>Nator Call.   | Pica   | 6.25<br>wing give rate (time)<br>ommended pump a<br>28.34<br>genrevelded pump a<br>2644<br>45.16<br>i protuction (time)G#<br>45.34<br>Ves No   | rGPM)<br>epth (Dit)<br>ite<br>Map of Wel<br>pelow fotmer   | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>II Loca<br>9 instru  | 6.59<br>6.60<br>6.61<br>6.63<br>6.63<br>6.63                         | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>he back  | 6.60   |
| Li Robery I<br>Borng<br>Borng<br>Other, s<br>Isside<br>Diameter<br>(onlin)<br>J.S. 24<br>JO. 16<br>Diameter<br>Diameter<br>(onlin)<br>J.S. 24<br>JO. 16  | Anison<br>presty<br>Open Hele<br>Constrained<br>Constrained<br>Steel +<br>Steel +<br>Const<br>Plastic Carrow<br>Stawn  | struction f<br>OR Material<br>Fateglass,<br>lastic, Steel)<br>2<br>K Rocker<br>Mruction R<br>riad<br>nizad, Steel)<br>Less   | Record - Ca<br>Wat<br>Thereas<br>. 4771<br>. 4771<br>. 4777<br>. 4777<br>. 4777<br>. 51ct No<br>12   | edustinal<br>ther, specify<br>ising<br>Dest<br>From<br>t, 45<br>of 1.87<br>of 1.87<br>Cent<br>From<br>30, 76  | n (m/tt)<br>To<br>31.64<br>30.78<br>(m/tt)<br>To<br>33.,30  | Status of Wei<br>Utter Supply<br>Replacement<br>Replacement<br>Deveteing Weil<br>Deveteing Weil<br>Attantomet<br>(Construction)<br>Attantomet, offweil<br>specify<br>Deveteing Weil<br>Attantomet, offweil<br>specify<br>Deveteing Weil<br>Deveteing Weil<br>Attantomet, offweil<br>specify<br>Deveteing Weil<br>Deveteing Weil<br>Attantomet, offweil<br>specify<br>Deveteing Weil<br>Deveteing Weil<br>Deveteing Weil<br>Attantomet, offweil<br>specify<br>Deveteing Weil<br>Deveteing Weil<br>Deveteing Weil<br>Attantomet, offweil<br>specify<br>Deveteing Weil<br>Deveteing Weil<br>Deveteing<br>Deveteing Weil<br>Deveteing Weil<br>Deveteing Weil<br>Deveteing<br>D   | or Weil  | 6.25<br>Wing give rate (time)<br>ommended pump of<br>28.34<br>gmmended pump of<br>29Min<br>45.16<br>(imatGA<br>iso provide a mag   | CPM)<br>sph @II)<br>tto<br>Map of Weal<br>below following<br>comparison  | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>11 Local<br>9 instru   | 6.59<br>6.60<br>6.61<br>6.63<br>6.63<br>6.63<br>1000<br>ections on b | 15<br>20<br>25<br>30<br>40<br>50<br>60   | 6.60   |
| Li Robery I<br>Boring<br>Boring<br>Ar period<br>Other, s<br>Isside<br>Diameter<br>(onlin)<br>IS-24<br>IO.16<br>Outside<br>Diameter<br>(onlin)<br>IS-24<br>IO.16  | Ansien<br>pretty<br>Open Helle<br>Contrefe P<br>Steel +<br>Steel +<br>Cons<br>(Plaste, Calva<br>Stalin,  | struction I<br>OR Metantal<br>Foreglass,<br>and: Sheet)<br>21<br>K Rocker<br>Aruction R<br>riad<br>riad, Sheet)<br>1055  | Record - Ca<br>Wed<br>Thereon<br>(Cm)<br>.471<br>.471<br>.471<br>.417<br>Sict No<br>12   | ecustral<br>ther, specify<br>ising<br>Dest<br>From<br>t, 45<br>of 1.87<br>Dest<br>From<br>Dest<br>From  | n (m/tt)<br>To<br>31,64<br>30,78<br>(m/tt)<br>To<br>33,30   | Status of Wei<br>Status of Wei<br>Status Supply<br>Reptocempt<br>Reptocempt<br>Development<br>Observation and<br>Montioning Hele<br>Attenation<br>(Construction)<br>Abandomed, Pool<br>Abandomed, Ook<br>Vater Quality<br>Abandomed, othus<br>specify<br>Other, specify<br>Interation<br>(Onter, specify)<br>Interation<br>(Interational Supplementation<br>(Interational Supplementation)<br>(Interational Supplementation)<br>(Interatio   | Record   | 6.85<br>Wing give rate (time)<br>pommended pump of<br>28.34<br>generation of the second<br>portugination of the second<br>portuginat  | CPM)<br>sph @tt)<br>tto<br>http<br>http<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/<br>http://web/   | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>81<br>1 Loca<br>9 instru   | 6.59<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63<br>tition<br>consont    | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>he back  | 6.60   |
| Li Robery I<br>Boring<br>Boring<br>Ar period<br>Other, s<br>Isside<br>Diameter<br>(on/in)<br>IS-24<br>IO.16<br>Octade<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter  | Antion<br>pecity<br>Open Hele<br>Contrefs. P<br>Steel +<br>Steel +<br>Cons<br>(Plaste, Galva<br>Staum<br>Staum   | struction I<br>Performant<br>Performant<br>india Sheeti<br>2<br>K Recher<br>Aruation R<br>riad<br>Intacid, Steeti<br>Less<br>Water Det   | Record - Ca<br>Wed<br>Therewise<br>On)<br>. 471<br>. 471<br>. 471<br>Sot No<br>12<br>Sot No<br>12<br>Sot No<br>12  | edustrial<br>More, specify<br>Bising<br>Dept<br>From<br>+, 45<br>OCL.87<br>Depth<br>From<br>30, 76<br>Cuntested   | n (m/tt)<br>To<br>31.64<br>30.78<br>(m/tt)<br>To<br>30.,30<br>He<br>Depth   | Status of Wei<br>Status of Wei<br>Status Supply<br>Reptocent Supply<br>Test Hole<br>Recharge Weil<br>Observation and<br>Montoring Keile<br>Observation and<br>Montoring Keile<br>Attenation<br>(Construction)<br>Abandored, Poo<br>Water Quality<br>Other, specify<br>In District Supplements<br>Supplements<br>District Supplements<br>Supplements<br>District Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Supplements<br>Sup   | Record Re | 6.85<br>wing give rate (time)<br>ommended pump d<br>96/Hit<br>45.14<br>production (time)GF<br>dected?<br>Yes No  | CPM)<br>sph @tt)<br>sto<br>74.6)<br>Map of Well<br>poly following of the following o   | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>11 Loca<br>9 instru  | 6.59<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63<br>80m                  | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>he back  | 6.60   |
| Li Robery I<br>Boring<br>Boring<br>Arr perce<br>Other, s<br>Isside<br>Diameter<br>(onvin)<br>IS-24<br>IO.16<br>Outside<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diam | Antien<br>pecify<br>Con<br>Open Helle<br>Conrete. P<br>Steel +<br>Cons<br>Plaste. Carve<br>Steel A<br>Cons<br>Plaste. Carve<br>Steel A<br>Cons<br>Plaste. Carve<br>Steel A<br>Cons<br>Plaste. Carve<br>Steel A<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons<br>Cons | struction I<br>Partechan,<br>Instruction R<br>Partechan,<br>instruction R<br>R Racker<br>druction R<br>riad<br>nizod, Steel)<br>Less<br>Water DeL<br>of Water<br>Other, spec   | Record - Ca<br>Wed<br>The control - Ca<br>The con  | Hors specify<br>Ising<br>Dept<br>From<br>4,45<br>04.87<br>04.87<br>From<br>Depth<br>From<br>30,78<br>Currented  | h (m/t)<br>То<br>31.64<br>30.78<br>30.78<br>то<br>до.78<br>На<br>Сорт   | Status of Wei<br>Status of Wei<br>Status Supply<br>Repacement<br>Repacement<br>Repacement<br>Repacement<br>Repacement<br>Repacement<br>Repacement<br>Beautions<br>Mentioned Hole<br>Attendion<br>(Construction)<br>Abandoned, Poo<br>Water Cuasity<br>Abandoned, other<br>specify<br>Other, specify<br>In<br>Diameter<br>To<br>Construction<br>To<br>Construction<br>To<br>Construction<br>To<br>Construction<br>To<br>Construction<br>To<br>Construction<br>To<br>Construction<br>To<br>Construction<br>Construction<br>State<br>Construction<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State<br>State | Pilea  | 6.85<br>wing give rate (time)<br>ommended pump of<br>38.34<br>grownended pump of<br>36PM)<br>45.46<br>yrs No<br>45.46<br>yrs No  | CPM)<br>sph @tt)<br>sto<br>*//)<br>Map of Well<br>helps/folger<br>gm   | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>11 Local<br>2 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)  | 6.59<br>6.69<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63<br>80m          | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>he back  | 6.60   |
| Li Robery I<br>Borng<br>Borng<br>Cother, s<br>Inside<br>Diameter<br>(onVin)<br>IS-24<br>IO.16<br>Outside<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Di<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diam 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  | struction I<br>Perception<br>Perception<br>inter-Steel<br>2<br>K Rocker<br>Muction R<br>rist<br>nized, Steel<br>Uses<br>Water Det<br>d of Water<br>Other, spec<br>d of Water   | Record - Ca<br>Wed<br>The control of the 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  | edustrial<br>More, specify<br>Bang<br>Dept<br>From<br>4, 45<br>021.87<br>021.87<br>Cent<br>From<br>30, 78<br>Cuntested<br>Untested  | h (m/t)<br>То<br>З1.64<br>З0.78<br>(m/t)<br>То<br>З0.78<br>На<br>Сорт<br>Гот<br>Сорт<br>Сорт  | Status of Wei<br>Status of 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  | Rec Veal   | 6.85<br>wing give rate (time)<br>ommended pump of<br>38.34<br>grownended pump of<br>GPM)<br>grownended pump of<br>GPM)<br>the of the second<br>production (time)GP<br>fectod?<br>the provide a mag<br>the provide a mag  | GPM)<br>aph @T0<br>ato<br>Map of Wel<br>Pelov follawor<br>Charlen<br>Charlen<br>All<br>All<br>All<br>All<br>All<br>All<br>All<br>Al  | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>11 Locat   | 6.59<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63<br>80m                  | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | 6.60<br>6.60<br>6.50<br>6.50<br>6.50<br>6.50                                 |
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Steel<br>2<br>K Racker<br>Mater Det.<br>d of Water<br>Other, spec<br>d of Water   | Record - Ca<br>Record - Ca<br>Wat<br>The second<br>- 477<br>-                                   | dustinal<br>More, specify<br>Bing<br>Dept<br>From<br>4,45<br>Depth<br>From<br>Bogth<br>From<br>30,78<br>Cuntested<br>Untested   | h (m/ti)<br>То<br>З1.64<br>З0.78<br>(m/ti)<br>То<br>З0.78<br>на<br>Сорт<br>Рассание<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт<br>Сорт | Status of Wei       Øder Supply       Replacement       Replacement       Bezharge Weil       Dewetragen and<br>Montorng Weil       Deversion and<br>Montorng Weil       Deversion and<br>Montorng Weil       Deversion and<br>Montorng Weil       Atteration<br>(Construction)       Atteration<br>(Construction)       Abandoned, not<br>Water Cushty       Abandoned, othus<br>specify       Other, specify       Ma Dianteter       To       To       G3, 30     19, 6   | H foo  | 6.85<br>wing give rate (time)<br>ommended pump of<br>38.34<br>grownended pump of<br>GPMA<br>GPMA<br>(tectod?<br>Yes No<br>tse provide a mag  | CPM)<br>aph @TD<br>ato<br>Map of Wel<br>Philor followprotection<br>aph @ Company<br>Aph Aph & Company<br>Aph &   | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>11 Loca<br>2 instru  | 6.59<br>6.60<br>6.60<br>6.61<br>6.63<br>6.63<br>6.63<br>80m          | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | 6.60   |
| LI Robery I<br>Boring<br>Boring<br>Other, s<br>Inside<br>Diameter<br>(onvin)<br>IS-24<br>IO.16<br>Outside<br>Diameter<br>(onvin)<br>IS-24<br>IO.16<br>Outside<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>(onvin)<br>IS-24<br>IO.16<br>Outside<br>Cottade<br>IS-24<br>IO.16<br>Outside<br>Cottade<br>IS-24<br>IS-24<br>IS-24<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-   | Correly Conrel Hele Conrels Steel Conrels Steel Cons Cons Cons Cons Cons Cons Cons Cons  | struction I<br>Parents Steel<br>Parents Steel<br>2<br>K Rector<br>K Rector<br>Mater Det<br>d of Water<br>Other, spec<br>Other, spec<br>Other, spec   | Record - Ca<br>Record - Ca<br>Provention<br>Provention<br>Provention<br>Provention<br>Stor No<br>12<br>Stor No | edustrial<br>More, specify<br>Bing<br>Dept<br>From<br>4, 45<br>OCI.87<br>Contested<br>Contested<br>Untested   | n (m/l)<br>10<br>31.64<br>30.78<br>10<br>30.78<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10  | Status of Wei<br>Status of Wei<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>Replacement<br>R   | a Reco   | 6.25<br>Wing give rate (time)<br>ommended pump a<br>28.34<br>GPMi<br>45.46<br>ise provide a map  | CPM)<br>oph @T)<br>to<br>Map of Wel<br>Philor following<br>of Wel<br>Anne  | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>8<br>11 Locat  | 6.59<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63<br>6.63<br>80 m         | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | 6.60   |
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Ca<br>Weat<br>Thermostan<br>Solution<br>- 477<br>- 4                                   | konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konstand<br>konsta  | n (m/l)<br>To<br>31.64<br>30.78<br>30.78<br>(m/l)<br>To<br>30.78<br>0<br>0<br>0<br>0<br>0<br>6,4<br>Informatio<br>Wet (   | Status of Wei       Øder Suppl       Replacement       Replacement       Replacement       Replacement       Beviarion       Observation and<br>Monitoring Heid<br>Abandoned, Poo<br>Water Cashly       Abandoned, Poo<br>Water Cashly       Abandoned, of the<br>specty       Other, specity       In       Contractor 5 Licenco 1  | A Record Dama A Plana A A A A A A A A A A A A A A A A A A  | 6.25<br>Wing give rate (time)<br>ommended pump a<br>28.34<br>GPMi<br>45.16<br>iprotuction (time)GF<br>fector?<br>Yes No  | CPM)<br>oph @T0<br>to<br>Map of Wel<br>Map of Wel<br>A<br>A<br>A<br>A<br>A<br>A<br>A<br>A<br>A<br>A<br>A<br>A<br>A   | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>11 Local<br>2<br>50<br>60<br>60<br>11 Local<br>2<br>50<br>50<br>60<br>50<br>50<br>60<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50 | 6.59<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63<br>6.63<br>80m          | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | 6.60   |
| Li Robery I<br>Boring<br>Boring<br>Ar perc<br>Other, s<br>Irada<br>Dameter<br>(onvin)<br>IS-24<br>IO.I6<br>Dometer<br>Onto<br>IS-24<br>IO.I6<br>Dometer<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>Dismeter<br>D   | Com<br>Open Hole<br>(Gavanized<br>Cotorels, P<br>Steel +<br>Steel +<br>Cons<br>(Plastic, Gava<br>(Plastic, Gava)<br>(Plastic, Gava<br>(Plastic, Gava)<br>(Plastic, Gava<br>(Plastic, Gava)<br>(Plastic, Ga  | struction I<br>Participant<br>Participant<br>Interchank<br>Mater Steel)<br>State<br>Mater Det<br>Mater Det<br>Mater Det<br>Mater Det<br>Other, space<br>d of Water<br>Other, space<br>d of Water<br>Other, space<br>d of Water<br>Other, space<br>d of Water<br>Other, space<br>d of Water   | Record - Ca<br>Wed<br>Thereas<br>Thereas<br>Thereas<br>Second - Second<br>Second - Sec   | Hor, specify<br>Ising<br>Dept<br>From<br>4,45<br>261.87<br>Con<br>Depth<br>From<br>30.18<br>Cuntested<br>Untested<br>Untested<br>Connician<br>S /AC   | h (m/t)<br>To<br>31.64<br>30.78<br>30.78<br>(m/t)<br>To<br>30.78<br>0<br>0<br>0<br>0<br>0<br>6,4<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1   | Status of Wei       Øder Suppl       Replacement       Replacement       Ret Hole       Retains       Beweineng Weil       Deweineng Weil       Abandoned, Poo       Water Cashty       Abandonet, Rob       Water Cashty       Abandonet, end       Water Cashty       Abandonet, end       Water Cashty       Abandonet, end       Other, specity       In       Greinactor & Losnoor I       Contractor & Losnoor I       7     1   | A Record Control of Co | 6.25<br>Wing give rate (time)<br>ommended pump a<br>28.34<br>GPMi<br>45.16<br>iprotuction (time)GH<br>fector?<br>Yes No  | CPM)<br>oph @10<br>to<br>Map of Well<br>Map of Well  | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>11 Loca<br>9 instru  | 6.59<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63<br>80m                  | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | 6.60<br>6.60<br>6.60<br>6.55<br>6.55   |
| Li Robery I<br>Borng<br>Borng<br>Other, s<br>Iraide<br>Dameter<br>(onvin)<br>IS-24<br>IO.16<br>Outset<br>Doughter<br>Diameter<br>(onvin)<br>IS-24<br>IO.16<br>Outset<br>IO.16<br>Outset<br>IS-24<br>IO.16<br>Outset<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-25<br>IS-2   | Ansien<br>pretty<br>Con<br>Conrel Hele<br>(Gavariace<br>(Gavariace<br>Steel +<br>Steel +<br>Conrel<br>Steel +<br>Steel +<br>Conrel<br>Steel +<br>Steel +<br>Conrel<br>Steel +<br>Steel +<br>Steel +<br>Conrel<br>Steel +<br>Steel +<br>St   | struction I<br>Participant<br>Participant<br>Inter-Steel<br>K Rocker<br>K Rocker<br>Mutuation R<br>rial<br>nizod, Steel<br>I<br>Cotter, spece<br>Cotter, spece<br>Cotter, spece<br>Cotter, spece<br>Cotter, spece<br>Contractor<br>Intercor<br>Cotter, spece<br>Contractor<br>Intercor<br>Cotter, spece<br>Contractor  | Record - Ca<br>Wed<br>Thereas<br>Solve<br>1-2<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve<br>Solve                                 | edustrial<br>More, specify<br>Bing<br>Dept<br>From<br>4,45<br>Sel.87<br>Con<br>From<br>30,78<br>CUntested<br>Untested<br>Untested<br>Connician<br>S /AC   | n (m/t)<br>To<br>31.64<br>30.78<br>(m/t)<br>To<br>30.78<br>Me<br>Bar, 30<br>He<br>Depth<br>From<br>0<br>6.4<br>Informatio<br>Well (<br>7<br>Munk  | Status of Wei       Øder Suppl       Replacement       Replacement       Recharge Weil       Dewetering Weil       Devetering Weil       Devetering Weil       Devetering       Abandomed.       Abandomed. Poo       Water Cushty       Abandomed. Poo       Water Cushty       Abandomed. Other specify       Other. specify       In       Contractor s Leance n       To       Sold. 4       25, 30       19, 6  | r Hito   | 6.85<br>wing give rate (time)<br>promoved pump a<br>28.34<br>2749<br>2749<br>1 production (time) GA<br>set provide a map   | CPM)<br>oph @11)<br>so<br>Map of Well<br>Map of Well   | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>9 instru   | 6.59<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63<br>6.63<br>80m          | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | 6.60<br>6.60<br>6.60<br>6.50<br>6.50<br>6.50                                 |
| Ar perc<br>Danetar i<br>Danetar i<br>Da   | Ansien<br>pretty<br>Corr<br>Corr<br>Conrele<br>Steel +<br>Corres<br>Steel +<br>Corres<br>Steel +<br>Corres<br>Steel +<br>Corres<br>Steel +<br>Corres<br>Mate<br>(Plastic, Galva<br>Statum<br>Statum<br>Corres<br>Mate<br>(Plastic, Galva<br>Statum<br>Statum<br>Corres<br>Steel +<br>Corres<br>Mate<br>(Plastic, Galva<br>Statum<br>Corres<br>Steel +<br>Corres<br>Mate<br>(Plastic, Galva<br>Statum<br>Corres<br>Steel +<br>Corres<br>Mate<br>(Plastic, Galva<br>Statum<br>Corres<br>Statum<br>Corres<br>Steel +<br>Corres<br>Corres<br>Corres<br>Steel +<br>Corres<br>Corres<br>Steel +<br>Corres<br>Steel +   | struction I<br>Paregiana,<br>Index Steel<br>2<br>K Recker<br>Mutuction R<br>rial<br>riad<br>riad<br>riad<br>riad<br>riad<br>riad<br>riad<br>riad   | Record - Ca<br>Wed<br>The form<br>- 477<br>-                                  | Hor, specify<br>Ising<br>Dept<br>From<br>+, 45<br>SEI.87<br>Con<br>   | n (m/t)<br>To<br>31.64<br>30.78<br>30.78<br>10<br>30.78<br>10<br>30.78<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10  | Status of Wei         Øder Supply         Replacement         Recharge Weil         Dewetering Weil         Dewetering Weil         Devetage weil         Devetage weil         Observation and<br>Monitoring Medi         Abandoned, Devetage         Water Cushty         Abandoned, One<br>specify         Other, specify         Other, specify         Balance         Other, specify         Other, specify         Diameter         Ghty         Sp. 30       19,6         To       Specify         Art For Pst   | I I foo  | 6.85<br>wing give rate (time)<br>primeroled pump of<br>28.34<br>genranced pump of<br>28.34<br>1 production (time) GA<br>fectod?<br>Yes No<br>sel provide a mag   | CPM)<br>oph @11)<br>so<br>Map of Well<br>Map of Well<br>Map of Well<br>of Well | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60<br>60<br>60   | 6.59<br>6.60<br>6.61<br>6.62<br>6.63<br>6.63<br>6.63<br>80m          | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | 6.66<br>6.66<br>6.66<br>6.58<br>6.58<br>6.58                                 |
| Ar perc<br>Other, s<br>Boring<br>Other, s<br>Iraide<br>Dameter<br>(onvin)<br>IS-24<br>IO.16<br>Outside<br>Dameter<br>(onvin)<br>IS-24<br>IO.16<br>Outside<br>Dameter<br>Other, s<br>IS-24<br>IO.16<br>Outside<br>Dameter<br>Other, s<br>IS-24<br>IO.16<br>Outside<br>IS-24<br>IO.16<br>Outside<br>IS-24<br>IO.16<br>IS-24<br>IO.16<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24<br>IS-24  | Ansien<br>pecty<br>Con<br>Open Hele<br>(Gavariae<br>Concrete, P<br>Steel +<br>Cons<br>Steel +<br>Cons<br>(Paustic, Galva<br>(Paustic, Galva<br>(Paust   | struction I<br>Paregians,<br>instruction R<br>Receiptions,<br>instruction R<br>read<br>read<br>read<br>read<br>read<br>read<br>read<br>read  | Record - Ca<br>Wed<br>The form<br>- 477<br>-                                  | Hor, specify<br>Ising<br>Dept<br>From<br>+, 45<br>of 1.87<br>From<br>Bogth<br>From<br>30, 76<br>Cuntested<br>Untested<br>Untested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cuntested<br>Cun  | n (m/t)<br>To<br>31.64<br>30.78<br>30.78<br>1.64<br>30.78<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>30.78<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.64<br>1.      | Status of Wei         Øder Supply         Replacement         Recharge Weil         Dewetering Weil         Dewetering Weil         Devetering Weil         Devetering Weil         Observation and<br>Monitoring Weil         Mandoned, Dow         Abandoned, One<br>Water Cuality         Abandoned, One<br>Water Cuality         Abandoned, One<br>Water Cuality         Other, specify         Other, specify         In         Contractors & Leanco I         To         Opality         Apart Forest   | I I I I I I I I I I I I I I I I I I I  | G.25<br>Wing give rate (time)<br>ommended pump of<br>DBAS<br>DPMI<br>GPMI<br>(production (time)GF<br>fectod?<br>Yes No<br>see provide a mag  | CPM)<br>oph @TI)<br>do<br>Map of Well<br>Map of Well<br>Map of Well<br>Map of Well<br>Ange Delowered<br>Asage Delowered  | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60<br>60<br>60   | 6.59<br>6.60<br>6.60<br>6.61<br>6.63<br>6.63<br>6.63<br>80m          | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60  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| CPM)<br>Sph (DT)<br>Ito<br>Map of Well<br>Peloy follown<br>Completed<br>Kage Detivered<br>Kage Detivered<br>Kage Detivered   | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60   | 6.59<br>6.60<br>6.61<br>6.63<br>6.63<br>6.63<br>80m                  | 15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60 | 0.64<br>6.64<br>6.60<br>6.60<br>6.56<br>6.56<br>6.56<br>6.56<br>6.56<br>6.56 |

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| From  | To  |  | (Material a  | nd Type)  | _   | (C  | (inf)  | Clear and sand  | free   | Time<br>(min)  | Water Lew   | el Time  | Water Level   |
| 0   | 604   | E  | sentor   | vite  |   |   | 1  | If pumping discontinue  | ed, give reason:   | Static   | 10.97   | (mary  | trank   |
|   |   |  |  |   |   | And to  |  |   |  | 1  | 1244  | 1  | 28.00   |
|   | -   |  | -  |   | -   |   |  | Pump intake set at  | m)   | 2  | 13 50   | 2  | 37 12   |
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| Met   | nod of Cor  | ISUUCUON :   | ASHNED!  |   | Well Us   | 0   |  | Pumping rate (min) (  | 3PM)   | -  | 14.00   | 3  | 20:07   |
| Cable To<br>Rotary (  | conventional)   | Diamond  |  | ublic<br>omestic  | Well Us Commer  | eitik<br>cial [<br>il [   | ] Not used<br>] Dewatering   | Pumping rate<br>22.73<br>Duration of pumping  | GPM)   | 4  | 14.63   | 4  | 35.38   |
| Met<br>Cable To<br>Rotary (<br>Rotary (<br>Boring   | nod of Cor<br>col<br>Conventional)<br>Reverse)  | Diamond<br>Jetting   |  | ublic<br>omestic<br>vestock<br>igation  | Well Us Commer Municips Municips Continue   | e<br>cial [<br>al [<br>a [<br>& Air Contain   | ] Not used<br>] Dewatering<br>] Monitoring   | Pumping rate(mi) (<br>22.73<br>Duration of pumping<br>_6_hrs + 0_1<br>Final water level and   | 3PM)<br>min<br>nf numping 658  | 4 5  | 14.63   | 3<br>4<br>5<br>5   | 35.38   |
| Met<br>Cable To<br>Rotary (I<br>Rotary (I<br>Boring<br>Vir perce<br>Other set   | nod of Cor<br>conventional)<br>Reverse)<br>ussion   | Diamond<br>Jetting<br>Driving<br>Digging   |  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther specific   | Well Us Commer Municips Municips Cooling  | e<br>al<br>& Air Condition  | ) Not used<br>) Dewatering<br>) Monitoring<br>oning  | Pumping rate(Imp) (<br>22,73<br>Duration of pumping<br>hrs +<br>Final water level end (<br>38,95  | min<br>of pumping (M)T   | 4<br>5<br>10   | 14.63   | 3<br>4<br>5<br>5<br>10   | 35.38<br>34.59<br>30.99   |
| Met<br>Cable Tc<br>Rotary (<br>Rotary (<br>Boring<br>Air parc.<br>Other, sp   | conventional)<br>Conventional)<br>Reverse)<br>ussion<br>pecify<br>Con   | Diamond<br>Jetting<br>Driving<br>Digging   |  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>sing   | Well Us Commer Municips Mi Test Hok Cooling a   | e<br>cial<br>al<br>& Air Condition<br>& Air Condition   | ) Not used<br>) Dewatering<br>) Monitoring<br>pning  | Pumping rate(Imp) (<br>20,73<br>Duration of pumping<br>hrs +<br>Final water level end (<br>   | SPM)<br>min<br>of pumping (Mit<br>S<br>sin/GPM)  | 4<br>5<br>10<br>15   | 14.63<br>15.63<br>18.40<br>21.06  | 3<br>4<br>5<br>10<br>10<br>15  | 35.38<br>34.59<br>30.99<br>27.85  |
| Met<br>Cable To<br>Rotary (I<br>Rotary (I<br>Boring<br>Air pero.<br>Other, sp<br>nside<br>ameter  | Conventional)<br>Reverse)<br>ussion<br>pecify<br>Con<br>Open Hole   | Diamond<br>Jetting<br>Driving<br>Digging   | Cord - Ca  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>sing<br>Dept   | Well Us Conner Municipe Municipe Test Hold Cooling  | e cial cial d d Status  | ) Not used<br>) Dewatering<br>) Monitoring<br>oning<br>: of Well<br>Supply   | Pumping rate (Imp) (  | SPM)<br>min<br>of pumping (DR)<br>S<br>invGPM)<br>o depth (DR)   | 3<br>4<br>5<br>10<br>15<br>20  | 14.63<br>15.63<br>18.40<br>21.06<br>23.10   | 3<br>4<br>5<br>10<br>15<br>20  | 35.38<br>34.59<br>30.91<br>27.85<br>25.23   |
| Met<br>Cable Tc<br>Rotary (I<br>Rotary (I<br>Boring<br>Air perc.<br>Other, sp<br>Inside<br>iameter  | conventional) Conventional) Roverse) Ussion pecify Con  | Diamond<br>Jetting<br>Driving<br>Digging<br>Struction Re<br>OR Material<br>d, Fibreglass,<br>Yastic, Steel   | Cord - Ca<br>Wal<br>Thickness  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>sing<br>Dept<br>From   | Well Us Commer Municipe X Test Hok Cooling i Cooling i h(0)ft) To   | e<br>cial<br>ll<br>& Air Condition<br>& Air Condition<br>& Condition | ) Not used<br>) Dewatering<br>) Monitoring<br>oning<br>oning<br>s of Well<br>Supply<br>ement Well<br>ble   | Pumping rate $(1, 1, 2, 2, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3,$  | SPM)<br>of pumping (OTR<br>S<br>in/GPM)<br>depth (TTR)   | 3<br>4<br>5<br>10<br>15<br>20<br>25  | 14.63<br>14.63<br>15.63<br>18.40<br>21.06<br>23.10<br>24.01   | 3<br>4<br>5<br>10<br>10<br>15<br>20<br>20  | 20.97<br>35.38<br>34.59<br>30.99<br>27.85<br>25.23<br>23.43   |
| Met<br>Cable Tc<br>Rotary (<br>Rotary (<br>Boring<br>Air pero.<br>Other, sp<br>ameter<br>Din)   | conventional)<br>Reverse)<br>ussion<br>pecify<br>Open Hole<br>(Galvanizes<br>Concrete, F  | Istruction Istruction Istruction Istruction Re OR Material Foreglass, Pastic, Steel  | Cord - Ca<br>Wall<br>Thickness   | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>sing<br>Dept<br>From<br>+,50   | Well Us Commer Municipe X Test Hold Cooling hmmt) To 46.63  | e<br>cial<br>& Air Condition<br>& Air Condition<br>& Air Condition<br>& Replace<br>& Replace<br>& Replace<br>& Replace<br>& Replace   | Not used<br>Dewatering<br>Monitoring<br>ming<br>Supply<br>sement Well<br>sle<br>rge Well<br>aring Well   | Pumping rate (Imp) (<br>20.7.3<br>Duration of pumping<br>6 hrs + 0<br>Final water level and a<br>38.9 =<br>1f flowing give rate (Im<br>Recommended pump<br>(Imp) CPM) 22.   | min<br>of pumping (Cont<br>invGPM)<br>o depth (Cont)<br>in table<br>73   | 4<br>5<br>10<br>15<br>20<br>25<br>30   | 14.63<br>14.63<br>15.63<br>18.40<br>21.06<br>23.10<br>23.10<br>25.31  | 3       4       5       10       15       20       7       25       30   | 25.38<br>34.59<br>30.99<br>27.85<br>25.23<br>23.43<br>23.43<br>21.73  |
| Met<br>Cable Tr<br>Cotary (<br>Cotary (<br>C  | Conventional)<br>Reverse)<br>ussion<br>pecify<br>Con<br>Open Hole<br>(Galvanize<br>Concrete, F<br>Steel +   | Diamond<br>Jatting<br>Driving<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Extruction Re<br>OR Material<br>4, Fornglass,<br>Pastic, Steel<br>Extruction Re<br>Construction Re<br>Cons  | P. P   | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>sing<br>Dept<br>From<br>+, 50<br>45,7,2  | Well Us Commer Omnor Municipe Def Test Hole Cooling (  h@mt) To 46.63 46.63   | e<br>tial<br>& Air Condition<br>Status<br>Water S<br>Replace<br>X Test Hc<br>Rechar<br>Dewate<br>Observ   | Not used<br>Dewatering<br>Monitoring<br>oning<br>s of Well<br>Supply<br>ement Well<br>ole<br>ring Well<br>ening Well<br>ration and/or<br>free Mel-   | Pumping rate (Imp) (<br>20.7.3<br>Duration of pumping<br>6_hrs + 0_1<br>Final water level and (<br>38.9 =<br>If flowing give rate (Im<br>Recommended pump<br>45.1<br>Recommended pump<br>(Im) GPM)<br>20.7<br>Well production (Imiw)  | SPM)<br>min<br>of pumping (Dit<br>in/GPM)<br>of depth (Tig)<br>)<br>rate<br>73<br>(GPM)  | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40   | 14.60<br>14.63<br>15.63<br>18.40<br>21.06<br>23.10<br>23.10<br>23.10<br>23.10<br>23.10<br>25.31<br>27.55  | 3       4       5       10       15       20       7       25       30       3       4   | 25.38<br>34.59<br>30.99<br>27.85<br>25.23<br>23.43<br>23.43<br>21.73<br>19.01   |
| Met<br>Cable Tr<br>Rotary ((<br>Rotary ()<br>Boring<br>Air pero.<br>Other, sp<br>inside<br>iameter  | Conventional)<br>Roverse)<br>ussion<br>pecify<br>Open Hole<br>(Galvanize,<br>Conventional)  | Istruction  | Wall<br>Wall<br>Wall<br>Wall<br>Wall<br>Wall<br>Wall<br>Wall   | ublic<br>ormestic<br>westock<br>tigation<br>dustrial<br>ther, specify<br>Sting<br>Dept<br>From<br>4,50<br>45.7,2  | Weil Us     Commer     Municipe     Municipe     ØT Test Hold     Cooling     To     To     46.63     46.63   | e cial cial Status Status VaterS Replac Q Test He Dewate Observ Monito Atteration   | Not used<br>Dewatering<br>Monitoring<br>ming<br>soft Well<br>Supply<br>ament Well<br>also<br>groe Well<br>ening Well<br>ration and/or<br>ring Hole<br>on   | Pumping rate (Imp) (<br>23,73<br>Duration of pumping<br>6 http://www.mithing.org/<br>Final water level and (<br>38,95<br>If flowing give rate (Imm<br>Recommended pump<br>45,1<br>Recommended pump<br>Mind GPM)<br>28,7<br>Well production (Imm)<br>Disinforter?  | SPM)<br>min<br>of pumping (Dit<br>in/GPM)<br>or depth (Dit)<br>or rate<br>13<br>GPM)   | 3       4       5       10       15       20       25       30       40       50   | 14.63<br>14.63<br>15.63<br>18.40<br>21.06<br>23.10<br>23.10<br>23.10<br>23.10<br>23.10<br>23.31<br>27.51<br>27.51<br>27.51  | 3       4       5       10       15       20       7       25       3       30       30       30       30       30       30       30   | 25-38<br>34.59<br>30.99<br>27.95<br>25.23<br>23.43<br>23.43<br>21.73<br>19.01<br>17.28  |
| Met<br>Cable Tc<br>Rotary (I<br>Rotary (I<br>Boring<br>Air perc.<br>Other, sp<br>aneter<br>Din)   | noa or Cor<br>ool<br>conventional)<br>Roverse)<br>ission<br>pedity<br>Connette, f<br>Steel +  | Burnond     Jetting     Driving     Driving     Drigging     Digging   | Cord-Ca<br>Wal<br>Thioness<br>(Cord-Ca<br>Mal<br>Thioness<br>(Cord-Ca  | ablic<br>mestic<br>vestock<br>igation<br>dustrial<br>her, specify<br>sting<br>From<br>+1,5D<br>45:72  | Weill Us           □ Commer           □ Municipe           ☑ Tost Hold           □ Cooling :           □ </td <td>cial</td> <td>Not used     Dewatering     Monitoring     ming     sof Well     supply ement Well     ale     eng Well aring Well aring Well aring Hole     on     nuction)     oned,</td> <td>Pumping rate (Imp) (<br/>23,73<br/>Duration of pumping<br/></td> <td>SPM)<br/>min<br/>of pumping (Dit<br/>in/GPM)<br/>orate<br/>13<br/>IGPM)</td> <td>3<br/>4<br/>5<br/>10<br/>15<br/>20<br/>25<br/>30<br/>40<br/>50<br/>60</td> <td>14.00<br/>14.03<br/>15.63<br/>15.63<br/>18.40<br/>21.04<br/>23.00<br/>24.01<br/>25.33<br/>27.55<br/>27.55<br/>27.26<br/>30.45</td> <td>3       4       5       10       12       15       20       25       30       340       50       50       60</td> <td>25.38<br/>34.59<br/>30.99<br/>27.85<br/>25.23<br/>23.43<br/>21.73<br/>19.01<br/>17.28<br/>15.8</td>   | cial  | Not used     Dewatering     Monitoring     ming     sof Well     supply ement Well     ale     eng Well aring Well aring Well aring Hole     on     nuction)     oned,   | Pumping rate (Imp) (<br>23,73<br>Duration of pumping<br>  | SPM)<br>min<br>of pumping (Dit<br>in/GPM)<br>orate<br>13<br>IGPM)  | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60  | 14.00<br>14.03<br>15.63<br>15.63<br>18.40<br>21.04<br>23.00<br>24.01<br>25.33<br>27.55<br>27.55<br>27.26<br>30.45   | 3       4       5       10       12       15       20       25       30       340       50       50       60   | 25.38<br>34.59<br>30.99<br>27.85<br>25.23<br>23.43<br>21.73<br>19.01<br>17.28<br>15.8   |
| Met<br>Cable Tc<br>Rotary (I<br>Rotary (I<br>Boring<br>Air purc.<br>Other, sy<br>Inside<br>Inside   | India of Cor<br>ad Conventional)<br>Roverse)<br>ussion<br>pedity<br>Converse)<br>Converse, F<br>Steel +<br>Steel +<br>Con   | Instruction Instru   |  | ablic<br>mestic<br>restock<br>igation<br>dustrial<br>ther, specify<br>From<br>45:77,2<br>45:77,2  | Well Us           □ Commer           □ Municipe           ☑ Test Hold           □ Cooling :           □ <td>Status     Ar Condition     Status     Ar Condition     Ar Condition     Ar Condition     Atternation     Construct     Abande     Abande     Abande</td> <td>Not used     Deviatering     Monitoring     aning     softWell'     Supply     ement Well     ation and/or     ing Hole     on     unction)     oned, Poor</td> <td>Pumping rate (Imp) (</td> <td>SPM)<br/>min<br/>of pumping (Dit<br/>in/GPM)<br/>odepth(Tigt)<br/>1<br/>rate<br/>73<br/>(GPM)<br/>Map of W</td> <td>4<br/>5<br/>10<br/>15<br/>20<br/>25<br/>30<br/>40<br/>50<br/>60</td> <td>14.00<br/>14.03<br/>15.63<br/>18.40<br/>21.04<br/>23.00<br/>24.01<br/>25.33<br/>27.58<br/>24.30<br/>30.45<br/>30.45</td> <td>3       4       5       10       15       20       7       25       300       40       50       60</td> <td>25.38<br/>34.59<br/>30.99<br/>27.95<br/>25.23<br/>23.43<br/>21.73<br/>21.73<br/>19.01<br/>17.28<br/>15.81</td>  | Status     Ar Condition     Status     Ar Condition     Ar Condition     Ar Condition     Atternation     Construct     Abande     Abande     Abande  | Not used     Deviatering     Monitoring     aning     softWell'     Supply     ement Well     ation and/or     ing Hole     on     unction)     oned, Poor   | Pumping rate (Imp) (  | SPM)<br>min<br>of pumping (Dit<br>in/GPM)<br>odepth(Tigt)<br>1<br>rate<br>73<br>(GPM)<br>Map of W  | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60   | 14.00<br>14.03<br>15.63<br>18.40<br>21.04<br>23.00<br>24.01<br>25.33<br>27.58<br>24.30<br>30.45<br>30.45  | 3       4       5       10       15       20       7       25       300       40       50       60   | 25.38<br>34.59<br>30.99<br>27.95<br>25.23<br>23.43<br>21.73<br>21.73<br>19.01<br>17.28<br>15.81   |
| Met<br>Cable Tr.<br>Rotary (f<br>Rotary (<br>Boring<br>Vir porc.<br>Dither, sp<br>Dither, sp<br>Dithe   | India or Con-<br>ad Conventional)<br>Roverse)<br>ussion<br>pecify<br>Con-<br>Con-<br>Con-<br>Con-<br>Con-<br>Con-<br>Con-<br>Con-   | In the ternal analog, Steel)   | Cord - Sci<br>Storko   | Ablic<br>mestic<br>vestock<br>igation<br>dustrial<br>her, specify<br>From<br>+1,5D<br>45:7,2<br>vestock<br>recent<br>Dept   | Weill Us           □ Commer           □ Municipe           ☑ Tost Hold           □ Cooling :           □           □           ↓           □           ↓           □           ↓ </td <td>Status     Ar Condition     Status     Ar Condition     Ar Condition     Ar Condition     Abande     Abande     Abande     Abande     Abande</td> <td>Not used     Deviatering     Monitoring     softwell***     Supply ement Well     se     ring Well     ring Well     ring Well     ring Hole     on     uction)     oned,     poor     Zuality     oned, Poor     Zuality</td> <td>Pumping rate (<math>M_{12}</math>) (<br/><math>A^3, 73</math>)<br/>Duration of pumping<br/><math>b_{175} + 0</math> 1<br/>Final water level and 0<br/><math>38, 9 \leq</math><br/>If flowing give rate (<math>M_{12}</math><br/>Recommended pump<br/>45.1<br/>Recommended pump<br/>(<math>M_{12}</math>) (<math>M_{12}</math>)<br/>Wel production (<math>M_{12}</math>)<br/>Wel production (<math>M_{12}</math>)<br/><math>B_{12}</math> No<br/>Please provide a ma</td> <td>SPM)<br/>min<br/>of pumping (Dit.<br/>invGPM)<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>odepth(Trit)<br/>()<br/>()<br/>()<br/>()<br/>()<br/>()<br/>()<br/>()<br/>()<br/>(</td> <td>4<br/>5<br/>10<br/>15<br/>20<br/>25<br/>30<br/>40<br/>50<br/>60<br/>60</td> <td>14.00<br/>14.03<br/>15.03<br/>18.40<br/>21.06<br/>23.00<br/>24.01<br/>25.30<br/>27.56<br/>27.56<br/>27.56<br/>27.56<br/>27.56<br/>27.56<br/>27.56</td> <td>3       4       5       10       15       20       25       300       40       50       50       60</td> <td>25.38<br/>34.59<br/>30.99<br/>27.95<br/>25.23<br/>23.43<br/>23.43<br/>21.73<br/>19.01<br/>17.28<br/>15.81</td>   | Status     Ar Condition     Status     Ar Condition     Ar Condition     Ar Condition     Abande     Abande     Abande     Abande     Abande  | Not used     Deviatering     Monitoring     softwell***     Supply ement Well     se     ring Well     ring Well     ring Well     ring Hole     on     uction)     oned,     poor     Zuality     oned, Poor     Zuality  | Pumping rate ( $M_{12}$ ) (<br>$A^3, 73$ )<br>Duration of pumping<br>$b_{175} + 0$ 1<br>Final water level and 0<br>$38, 9 \leq$<br>If flowing give rate ( $M_{12}$<br>Recommended pump<br>45.1<br>Recommended pump<br>( $M_{12}$ ) ( $M_{12}$ )<br>Wel production ( $M_{12}$ )<br>Wel production ( $M_{12}$ )<br>$B_{12}$ No<br>Please provide a ma   | SPM)<br>min<br>of pumping (Dit.<br>invGPM)<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>odepth(Trit)<br>()<br>()<br>()<br>()<br>()<br>()<br>()<br>()<br>()<br>(  | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | 14.00<br>14.03<br>15.03<br>18.40<br>21.06<br>23.00<br>24.01<br>25.30<br>27.56<br>27.56<br>27.56<br>27.56<br>27.56<br>27.56<br>27.56   | 3       4       5       10       15       20       25       300       40       50       50       60  | 25.38<br>34.59<br>30.99<br>27.95<br>25.23<br>23.43<br>23.43<br>21.73<br>19.01<br>17.28<br>15.81   |
| Met<br>Cable Tc<br>Rotary ()<br>Rotary ()<br>String<br>Rotary ()<br>Rotary ()<br>Rotary ()<br>String<br>Rotary ()<br>String<br>Rotary ()<br>String<br>Rotary ()<br>String<br>Rotary ()<br>String<br>Rotary ()<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>String<br>S  | ritod or Cor<br>sol<br>conventional)<br>Roverse)<br>ussion<br>peelly<br>Conrete, f<br>Conrete, f<br>Steel +<br>Steel +<br>Con<br>(Plastic, Galv   | Bitruction     Biamond     Jetting     Digging     Digging     Digging     Digging     Digging     Struction Re     A     Kpacker     struction Re     terial     anized, Steel)   | Cord - Sci<br>Siot No.   | Ablic<br>mestic<br>vestock<br>igation<br>dustrial<br>her, specify<br>From<br>+, SD<br>45:7,2<br>vestock<br>From<br>-, SD<br>-, SD<br>- | Weill Us           □ Commer           □ Municipe           ☑ Tost Hold           □ Cooling :           □           □           ↓           □           ↓ </td <td>Cial     Cial     Cial     Cial     Status     Air Condition     Air Condition     Cial     Cial</td> <td>Not used     Deviatering     Monitoring     soft Well     Supply     ement Well     sle     ring Well     ring Well     ring Well     ring Hole     on     unicinn)     oned,     inet.Supply     aned, Other,</td> <td>Pumping rate@mpin(</td> <td>min<br/>of pumping (Diff.<br/>invGPM)<br/>odepth(frigh)<br/>1<br/>1<br/>rate<br/>73<br/>rGPM)<br/>GPM)<br/>Sp below follow<br/>Husy (E)</td> <td>4<br/>5<br/>10<br/>15<br/>20<br/>25<br/>30<br/>40<br/>50<br/>60<br/>Hell Loc</td> <td>14.00<br/>14.03<br/>15.63<br/>18.40<br/>21.06<br/>23.00<br/>24.01<br/>25.33<br/>27.55<br/>24.36<br/>30.45<br/>30.45<br/>attion</td> <td>3       4       5       10       15       20       25       30       40       50       30       40       50       300       40       50       50       50       60</td> <td>25-38<br/>34.59<br/>30.91<br/>27.95<br/>25.23<br/>23.43<br/>23.43<br/>21.73<br/>19.01<br/>17.28<br/>15.8<br/>15.8</td> | Cial     Cial     Cial     Cial     Status     Air Condition     Air Condition     Cial  | Not used     Deviatering     Monitoring     soft Well     Supply     ement Well     sle     ring Well     ring Well     ring Well     ring Hole     on     unicinn)     oned,     inet.Supply     aned, Other,   | Pumping rate@mpin(  | min<br>of pumping (Diff.<br>invGPM)<br>odepth(frigh)<br>1<br>1<br>rate<br>73<br>rGPM)<br>GPM)<br>Sp below follow<br>Husy (E)   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>Hell Loc   | 14.00<br>14.03<br>15.63<br>18.40<br>21.06<br>23.00<br>24.01<br>25.33<br>27.55<br>24.36<br>30.45<br>30.45<br>attion  | 3       4       5       10       15       20       25       30       40       50       30       40       50       300       40       50       50       50       60   | 25-38<br>34.59<br>30.91<br>27.95<br>25.23<br>23.43<br>23.43<br>21.73<br>19.01<br>17.28<br>15.8<br>15.8  |
| Met<br>Cable Tc<br>Cable Tc<br>Rotary ()<br>Soring<br>Air parce<br>20ther, sp<br>ameter<br>ameter<br>20th<br>15<br>24<br>16<br>16   | conventional)<br>assion<br>pedfy<br>Convertional<br>ssion<br>open Hole<br>(Calvanime<br>Concrete, F<br>Steel +<br>Con<br>Maste, Calv<br>Steel +<br>Con<br>Maste, Calvani<br>Steel +<br>Con<br>Con<br>Con<br>Con<br>Con<br>Con<br>Con<br>Con   | Burucuon  Bannod  Jotting Diagnod Briting Digging  struction Re  oR Material A Fonglass, Pastic, Steel  struction Re  terial anized, Steel  Aless  | Cord - Ca<br>Water<br>Water<br>Com<br>Jan<br>Jan<br>Stor No.   | Ablic<br>mestic<br>vestock<br>igation<br>dustrial<br>her. specify<br>From<br>1,5D<br>45.7,2<br>Vestock<br>From<br>46.63   | Meil Us<br>□ Comme<br>Municipa<br>() Test Hold<br>□ Cooling :<br>16070)<br>To<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.75<br>46.75<br>47.855   | Cial Cial Cial Cial Cial Cial Cial Cial   | Not used     Deviatering     Monitoring     soft Well     serent Well     serent Well     ain     went Well     aring wel  | Pumping rate (Imp) (  | min<br>of pumping (Dit<br>invGPM)<br>odepth(Tit)<br>1<br>orate<br>73<br>(GPM)<br>GPM)<br>Map of M<br>sp below follow<br>Huxy E   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>Hell Loo   | 14.00<br>14.03<br>15.63<br>18.40<br>21.06<br>23.10<br>24.01<br>25.33<br>21.55<br>24.30<br>30.45<br>30.45  | 3         4           5         5           10         10           15         20           125         300           3         40           5         50           3         60   | 25-38<br>35-38<br>34.57<br>30.71<br>27.85<br>25.23<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>21.73<br>19.01<br>17.28<br>15.8<br>15.8   |
| Met<br>Cable Tc<br>Cable Tc   | ritod of Cor<br>sol<br>conventional)<br>Reverse)<br>assion<br>pedfy<br>Open Hole<br>(Calvanize<br>Concrete, F<br>Steel +<br>Con<br>(Plastic, Calv<br>Steel Steel<br>Steel Steel   | Instruction Re<br>I Diamond<br>J Jatting<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>Digging<br>D | water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Water<br>Solor<br>No.<br>12   | Ablic<br>mestic<br>vestock<br>(gation<br>dustrial<br>her, specify<br>From<br>1,5D<br>45:7,2<br>45:7,2<br>From<br>46,63  | Well Us           □ Commer           □ Municipy           □ Municipy           □ Municipy           □ Cooling           □ Cooling           □ 46.63           46.63           - 46.83           - 47.85   |   | Not used     Deviatering     Monitoring     soft Well     serent Well     aring Well     ar  | Pumping rate (Imp) (<br>20.713<br>Duration of pumping<br>has a second and a second<br>If flowing give rate (Im<br>Recommended pump<br>  | sPM)<br>min<br>of pumping (Diff.<br>invGPM)<br>odepth(Tigft)<br>1<br>orate<br>73<br>GPM)<br>Spelow follow<br>Huxy E  | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>40<br>60   | 14.00<br>14.03<br>15.63<br>18.40<br>21.66<br>23.10<br>24.01<br>25.33<br>27.58<br>24.20<br>30.48<br>30.48  | 3     3       4     5       5     10       0     15       0     20       7     25       3     30       3     40       >     50       3     60  | 25-38<br>35-38<br>34.57<br>30.71<br>27.85<br>25.23<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>21.73<br>19.01<br>17.28<br>15.8  |
| Met<br>Cable Tr.<br>Rotary (I<br>Boring)<br>Air parco<br>Other, sp<br>Inside<br>ameter<br>Din)<br>5.24<br>(I<br>S. 24<br>(I<br>S. 24<br>(I<br>S. 24<br>(I<br>S. 24)<br>(I<br>S. 24)<br>(I | conventional of Cor<br>conventional<br>sistion<br>poetly<br>Open Hold<br>(Galvanize<br>Concrete, F<br>Steel +<br>Steel +<br>Concrete, Steel +<br>Steel +<br>Concrete, Steel +<br>Steel +<br>Concrete, Steel +<br>Concrete, Steel +<br>Steel +<br>Concrete, Steel +<br>Concrete, Steel +<br>Steel +<br>Concrete, Steel +<br>Concrete,   | Instruction Restruction Restru   | stored - See<br>stores - See<br>itls   | Ablic<br>mestic<br>vestock<br>(gation<br>Austrial<br>her, specify<br>From<br>+,-5D<br>45:7,2<br>From<br>46,-63<br>VUntested   | Well Us           ○ comme           ○ damme           ○ damme <t< td=""><td></td><td>Not used     Dewatering     Monitoring     sof Well     Supply     ement Well     sig Well     aring Hole     on     nuction)     oned,     poor     Duality     aned, other,     specify     det     Diameter</td><td>Pumping rate (Imp) (<br/>23.7.3<br/>Duration of pumping<br/>has a second<br/>Final water level and (<br/>38.95<br/>If flowing give rate (Im<br/>Recommended pump<br/></td><td>SPM)<br/>min<br/>of pumping (Dit<br/>in/GPM)<br/>orate<br/>73<br/>(GPM)<br/>Map of M<br/>up below follow<br/>Auxy (E)</td><td>4<br/>5<br/>10<br/>15<br/>20<br/>25<br/>30<br/>40<br/>60<br/>60<br/>10<br/>15<br/>50<br/>60</td><td>14.00<br/>14.03<br/>15.03<br/>18.40<br/>21.06<br/>23.00<br/>24.01<br/>25.35<br/>27.55<br/>27.55<br/>27.55<br/>27.36<br/>30.45<br/>30.45</td><td>3         4           5         10           10         15           20         7           25         300           3         40           &gt; 50         3           60         50           3         60</td><td>25-38<br/>34-57<br/>30-71<br/>27-85<br/>25-23<br/>23-43<br/>23-43<br/>23-43<br/>23-43<br/>23-43<br/>23-43<br/>21-73<br/>19-01<br/>17-28<br/>15-81</td></t<>  |   | Not used     Dewatering     Monitoring     sof Well     Supply     ement Well     sig Well     aring Hole     on     nuction)     oned,     poor     Duality     aned, other,     specify     det     Diameter   | Pumping rate (Imp) (<br>23.7.3<br>Duration of pumping<br>has a second<br>Final water level and (<br>38.95<br>If flowing give rate (Im<br>Recommended pump<br>   | SPM)<br>min<br>of pumping (Dit<br>in/GPM)<br>orate<br>73<br>(GPM)<br>Map of M<br>up below follow<br>Auxy (E)   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>60<br>60<br>10<br>15<br>50<br>60   | 14.00<br>14.03<br>15.03<br>18.40<br>21.06<br>23.00<br>24.01<br>25.35<br>27.55<br>27.55<br>27.55<br>27.36<br>30.45<br>30.45  | 3         4           5         10           10         15           20         7           25         300           3         40           > 50         3           60         50           3         60  | 25-38<br>34-57<br>30-71<br>27-85<br>25-23<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>21-73<br>19-01<br>17-28<br>15-81   |
| Met<br>Cable TX<br>Rotary (I<br>Boring<br>Air parce<br>Dines<br>aneter<br>Din)<br>5.24<br>5.24<br>5.24<br>5.24<br>5.24<br>5.24<br>5.24<br>5.24  | trod or Cor<br>conventional)<br>ssion<br>poetly<br>Con<br>Open Held<br>Open Held<br>Concrete, F<br>Steel +<br>Concrete, Galv<br>Steel +<br>Con<br>(Plastic, Galv<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>S   | Instruction Re<br>Instruction Re   |  | Ablic<br>messic<br>vestock<br>(gation<br>dustrial<br>ther, specify<br>From<br>+,-SD<br>45:7,2<br>reen<br>Dept<br>From<br>46:63  | Well Us           □ Comme           □ Municipy           ☑ Test Hok           □ Cooling           ☑           □ Municipy           ☑ Test Hok           □ Cooling           ☑           □ Municipy           ☑ Test Hok           □ Cooling           □ 46.63           ↓ 46.63           ↓ 10.64 <tr< td=""><td>Status     Status     Status     Status     Status     Status     Observ     Monito     Abandk     Specity     Other, s     Other, s     Other, s</td><td>Not used     Dewatering     Monitoring     soft Well     Well     watering     Wonitoring     soft Well     water     watering     Well     well     wether     wether     wether     wether     wether     wether     wether     wether</td><td>Pumping rate (Imp) (<br/>20,713<br/>Duration of pumping<br/>(</td><td>SPM)<br/>min<br/>of pumping (Dit<br/>in/GPM)<br/>odepth (Trift)<br/>11<br/>12<br/>13<br/>IGPM)<br/>Map of M<br/>ap below follow<br/>Hwy E</td><td>4<br/>5<br/>10<br/>15<br/>20<br/>25<br/>30<br/>40<br/>60<br/>60<br/>60<br/>15</td><td>14.00<br/>14.03<br/>15.03<br/>18.40<br/>21.04<br/>23.00<br/>24.01<br/>25.33<br/>27.58<br/>27.58<br/>27.58<br/>27.58<br/>27.58<br/>27.58<br/>27.58</td><td>3     3       4     5       5     10       10     15       20     7       25     3       3     40       &gt; 50     50       3     60</td><td>25-38<br/>35-38<br/>34.59<br/>27.85<br/>25.23<br/>23.43<br/>21.73<br/>21.73<br/>19.01<br/>17.28<br/>15.8</td></tr<>   | Status     Status     Status     Status     Status     Status     Observ     Monito     Abandk     Specity     Other, s     Other, s     Other, s   | Not used     Dewatering     Monitoring     soft Well     Well     watering     Wonitoring     soft Well     water     watering     Well     well     wether     wether     wether     wether     wether     wether     wether     wether   | Pumping rate (Imp) (<br>20,713<br>Duration of pumping<br>(  | SPM)<br>min<br>of pumping (Dit<br>in/GPM)<br>odepth (Trift)<br>11<br>12<br>13<br>IGPM)<br>Map of M<br>ap below follow<br>Hwy E   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>60<br>60<br>60<br>15   | 14.00<br>14.03<br>15.03<br>18.40<br>21.04<br>23.00<br>24.01<br>25.33<br>27.58<br>27.58<br>27.58<br>27.58<br>27.58<br>27.58<br>27.58   | 3     3       4     5       5     10       10     15       20     7       25     3       3     40       > 50     50       3     60   | 25-38<br>35-38<br>34.59<br>27.85<br>25.23<br>23.43<br>21.73<br>21.73<br>19.01<br>17.28<br>15.8  |
| Met<br>Sable Tr<br>Sable Tr<br>S  | trod or Cor<br>conventional)<br>main and the second<br>conventional<br>main and the second<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>convention  | Instruction Re<br>Instruction Re<br>OR Material<br>A Foreglass,<br>Pastic, Steel)<br>EX<br>EX<br>EX<br>EX<br>EX<br>EX<br>EX<br>EX<br>EX<br>EX  | Cord - Ca<br>Wal<br>The freese<br>Stot No.<br>12<br>Fresh<br>ity<br>Fresh  | Ablic<br>messic<br>vestock<br>kgation<br>ther, specify  | Well Us           □ Commer           □ Municipe           ☑ Test Hold           □ Cooling :   | Status     Status     Status     Status     Status     Status     Over status     Status     Over status  | Not used Deviatering Monitoring aning Supply ement Well ato and/or ing Hole on nuction oned, Poor Duality oned, other, specify ter: Diameter Diame  | Pumping rate (Imp) (<br>20.713<br>Duration of pumping<br>(  | SPM)<br>min<br>of pumping (Dit<br>in/GPM)<br>o depth (Tit)<br>11<br>13<br>13<br>13<br>13<br>13<br>13<br>13<br>13<br>13   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>10<br>10<br>15<br>50<br>60   | 14.00<br>14.03<br>15.03<br>18.40<br>21.04<br>23.00<br>24.01<br>25.33<br>27.55<br>27.55<br>27.56<br>30.45<br>30.45   | 3     4       5     10       9     15       0     20       7     25       3     30       3     40       >     50       3     60  | 25-38<br>35-38<br>34.59<br>27.95<br>25.23<br>23.43<br>21.73<br>21.73<br>19.01<br>17.28<br>15.81   |
| Met<br>Cabbe TC<br>Rotary (I<br>Rotary (I<br>Rot   | tradi of Lor<br>conventional)<br>conventional<br>main and the second<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventional<br>conventer<br>conventeri<br>conventional<br>conventional<br>con  | Barnond     B  |  | Ablic<br>mestic<br>vestock<br>igation<br>dustrial<br>her, specify<br>From<br>+, 5D<br>45:7,2<br>Vestor<br>From<br>46.63<br>Untested   | Weill Us           □ Commer           □ Municipe           ☑ Test Hold           □ Cooling           <  | Status     Abande     Construction     Abande     Construction     Abande     Construction     Abande     Construction     Abande     Construction     Abande     Status     Construction     Abande     Secily     Other, s     Construction     Abande     Secily     Other, s     Construction     Abande     Secily     Construction     Abande     Secily     Construction     Abande     Secily     Construction     Abande     Secily     Secily     Construction     Abande     Secily     Construction     Secily     Construction     Secily   | Not used<br>Deviatering<br>Monitoring<br>aning<br>softwell<br>Supply<br>ement Well<br>ato<br>and well<br>ming Well<br>aton and/or<br>ring Hole<br>on<br>uction)<br>oned, aton<br>and/or<br>ring Hole<br>on<br>uction)<br>oned, other,<br>specify<br>ter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter  | Pumping rate (Imp) (<br>20.713<br>Duration of pumping<br>6 hrs + 0<br>Final water level and (<br>38.95<br>If flowing give rate (Im<br>Recommended pump<br>45.1<br>Recommended pump<br>(Imi) GPM)<br>20.7<br>Well production (Imin<br>Disinfected?<br>8 Yes No<br>Please provide a me<br>341 m   | SPM)<br>min<br>of pumping (Dit<br>in/GPM)<br>of depth (Tit)<br>1<br>T3<br>GPM)<br>Map of M<br>p below follow<br>Awy E  | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>16I Loc   | 14.00<br>14.03<br>15.03<br>18.40<br>23.00<br>24.01<br>25.30<br>27.56<br>27.56<br>27.56<br>27.56<br>27.56<br>27.56<br>27.56  | 3     4       5     10       0     15       0     20       7     25       3     30       3     40       >     50       3     60  | 25-38<br>35-38<br>34.59<br>30.99<br>25-23<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-73<br>19.01<br>17.28<br>15.81   |
| Met<br>Zaba Tri<br>Zaba Y ()<br>Zatary   | trod or Cor<br>conventional)<br>Roverse)<br>assion<br>pedfy<br>Corn<br>Open Hole<br>(Calvanize<br>Conrete, f<br>Steel →<br>Con<br>(Plastic, Galv<br>Steel →<br>Con<br>(Plastic, Galv<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat  | Bunond     Banond     Betting     Diving     Digging     Digging     Digging     Digging     Digging     Digging     Digging     Distruction Re     Struction Re     Struct  | Pr           D   | Ablic<br>mestic<br>vestock<br>igation<br>dustrial<br>her, specify<br>From<br>+, SD<br>45.7,2<br>Vestor<br>From<br>46, 63<br>Untested<br>Untested  | Weill Us           □ Commer           Municipe           Windipe           QT Test Hold           □ Cooling           1           10           46.63           46.63           46.63           46.785           1           1           10           10           10           10           10           10           10           10           10           10           10           10           10           10           11           10           11           12           13           14           15           14           15           14           15           16           16           17           18           18           19           10           10           10           10           10           10  | Status     Ar Condition     Ar Condition     Atheration     Construction     Abandd     Construction     Abandd     Abandd     Construction     Abandd     Construction     Abandd     Specify     Other, s     Construction     Abandd     Specify     Other, s     Construction     Abandd     Abandd     Specify     Construction     Abandd     Construction     Abandd     Specify     Status  | Not used<br>Devalening<br>Johanian<br>Suppy<br>server Well<br>server Well<br>and Well<br>ration and/or<br>ring Hole<br>on<br>uuction)<br>oned, alter<br>atton and/or<br>ring Hole<br>on<br>uuction)<br>oned, diver,<br>specify<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter   | Pumping rate@mpi/G  | SPM)<br>min<br>of pumping (Dit<br>invGPM)<br>odepth(Trit)<br>1<br>T3<br>GPM)<br>GPM)<br>Map of M<br>p below follow<br>Huoy E   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>60<br>60   | 14.00<br>14.03<br>15.03<br>18.40<br>21.04<br>23.00<br>24.01<br>25.31<br>27.52<br>27.52<br>27.52<br>27.52  | 3     4       5     10       9     15       9     15       9     20       7     25       3     30       3     40       >     50       3     60   | 25-38<br>35-38<br>34.59<br>30.91<br>27.95<br>25.23<br>23.43<br>23.43<br>21.73<br>19.01<br>17.28<br>15.81  |
| Met<br>Cable Ti<br>Rotary (I<br>Rotary (I<br>Rot   | trod of Cor<br>ad Corventional)<br>Roverse)<br>assion<br>poelfy<br>Corn<br>Connel Ke<br>(Galvanime<br>Concrete, f<br>Steel →<br>Concrete, f<br>Steel →<br>Steel →<br>Concrete, f<br>Steel →<br>Concrete, f<br>Co  | Burdenton Barnord Bar  | Pr           D           D           D           D           D           D           D           D           D           COIT           COIT           Water           Torr           Stot No.           12           iiiis           Fresh           fy           Fresh           ify           and Weil  | Ablic<br>mestic<br>vestock<br>igation<br>dustrial<br>her, specify<br>From<br>+, SD<br>45.7,2<br>45.7,2<br>Vestock<br>46, 63<br>Untested<br>Untested<br>Technicia  | Meil Us<br>Comme<br>Municipe<br>Wit Test Hold<br>Cooling<br>Cooling<br>HOM<br>To<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>46.63<br>47.85<br>46.63<br>47.85<br>46.63<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>46.63<br>46.63<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.85<br>47.8  | Status     Abande     Status     Atronditic     Status     Atronditic     Status     Abande     Abande     Constr     Abande     Status     Observ     Other, s     Other   | Not used<br>Devalening<br>Johanization<br>Supply<br>ement Well<br>ate<br>Table and the second<br>part of the s   | Pumping rate@mpi/G<br>20.713<br>Duration of pumping<br>6_hrs+0_i<br>Final water level and 0<br>38.9€<br>If flowing give rate (I/m<br>Recommended pump<br>45.1<br>Recommended pump<br>(min)GCPM)<br>28.7<br>Well production (I/min)<br>Disinfected?<br>8 Yes □ No<br>Please provide a me<br>3.41 m   | SPM)<br>min<br>of pumping (Dit<br>invGPM)<br>odepth(Trit)<br>1<br>T3<br>GPM)<br>Second Map of M<br>invery E<br>invery E  | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60<br>15   | 14.00<br>14.03<br>15.63<br>18.40<br>21.04<br>23.00<br>24.01<br>25.33<br>27.55<br>27.34<br>30.45<br>30.45  | 3     4       5     10       9     15       9     15       9     20       7     25       3     30       3     40       >     50       3     60   | 25-38<br>34.59<br>30.71<br>27.95<br>25.23<br>23.43<br>23.43<br>21.73<br>17.01<br>17.28<br>15.81<br>*  |
| Met<br>Cable TC<br>Rotary (I<br>Rotary (I<br>Rot   | triod of Cor<br>acid conventional)<br>acid conventional<br>more and a second<br>conventional<br>more and a second<br>conventional<br>Conventional<br>Conventer, F<br>Steel →<br>Steel →<br>Conventer, F<br>Steel →<br>Conventer, F<br>Steel →<br>Conventer, F<br>Steel →<br>Conventer, F<br>Steel →<br>Steel →<br>Conventer, F<br>Steel →<br>Conventer, F<br>Steel →<br>Steel →<br>Conventer, F<br>Steel →<br>Steel →  | Burdenting  |  | Ablic<br>mestic<br>vestock<br>igation<br>dustrial<br>her, specify<br>From<br>1,5D<br>45.7,2<br>Vestock<br>46,63<br>Untested<br>Untested<br>Teichnicia<br>1,5-   | Well Us           □ Commer           □ Municipe           ₩ Will Us           □ Cooling           □ Cooling           □ Cooling           □ 46.63           46.63           46.63           46.63           90%           □ To           47.85           □ H           □ Dept           From           ○           6.09           In Informatic   | Status     Abrodd     Status   | Not used<br>Deviatering<br>Monitoring<br>soft Well<br>Supply<br>ement Well<br>ate<br>ring Well<br>pro Well<br>pro Well<br>ring Well<br>oned, other,<br>int Supply<br>and, Poor<br>Quality<br>oned, other,<br>ter<br>Diameter<br>Ø 5 . 4<br>/ 1.68<br>s Licence No.   | Pumping rate (Imp) (<br>∂∂,73<br>Duration of pumping<br>(hrs +)<br>Final water level and 0<br>38.9 €<br>H flowing give rate (Im<br>Recommended pump<br>(Imh)GPM)<br>∂∂.<br>Wel production (Imin)<br>Disinfected?<br>(B) Yes No<br>Please provide a ma<br>3.4 Im<br>J  | sPM)<br>min<br>of pumping (Dit.<br>invGPM)<br>odepth(Trit)<br>1<br>T3<br>GPM)<br>Composition<br>Auxy (E)<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composition<br>Composit | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60<br>15   | 14.00<br>14.03<br>15.63<br>18.40<br>21.06<br>23.00<br>24.01<br>25.33<br>27.55<br>24.36<br>30.45<br>30.45  | 3     4       5     10       9     15       10     20       7     25       3     30       3     40       >     50       3     60   | 25-38<br>34.59<br>30.71<br>27.95<br>25.23<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>23.43<br>21.73<br>17.06<br>17.28<br>*   |
| Met<br>Cable TC<br>Robary (I<br>Boring)<br>Char you<br>Coher, s<br>Sarneter<br>Din)<br>Coher, s<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sarneter<br>Sa   | trade of Cor<br>action of Cor<br>action of Cor<br>conventional<br>Reverse)<br>ssion<br>Open Hole<br>(Calvanize<br>Concrete, F<br>Steel +<br>Steel +<br>Concrete, F<br>Steel +<br>Steel +<br>Concrete, F<br>Steel +  | Burdeuton Barnord Bar  |  | Ablic<br>mestic<br>vestock<br>igation<br>ther, specify<br>From<br>Trop<br>1,5D<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7 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 |   | Not used Deviatering Monitoring Supply ement Well ate ge Well rring Well rri  | Pumping rate (Imp) (  | SPM)<br>min<br>of pumping (DTL<br>invGPM)<br>odepth(TCTL)<br>1<br>T3<br>T3<br>GPM)<br>Map of M<br>ap below follow<br>Husy (E)  | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>efell Loc  | 14.00<br>14.03<br>15.63<br>18.40<br>21.06<br>23.00<br>24.01<br>25.33<br>27.52<br>24.30<br>30.42<br>30.42  | 3     3       4     5       5     10       6     15       7     25       3     30       3     40       >     50       3     60   | 25-38<br>34.59<br>30.71<br>27.95<br>25.23<br>23.43<br>23.43<br>21.73<br>19.01<br>17.28<br>15.8<br>15.8  |
| Met<br>Cable TC<br>Robary (I<br>Boring)<br>Char you<br>Char you   | triod of Cor<br>conventional<br>podfy   | Buildun Biamond Biamo  |  | Ablic<br>mestic<br>vestock<br>gation<br>ther, specify<br>From<br>1,5D<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>0<br>46,63<br>Untested<br>Untested<br>Untested<br>Technicia  | Well Us           □ Commer           □ Municipa   |   | Not used Deviatering Monitoring Supply and Supply and  | Pumping rate (Imp) (<br>∂∂,73<br>Duration of pumping<br>(hrs + Oi<br>Final water level and o<br>38.9 €<br>If flowing give rate (Im<br>Recommended pump<br>(Im) GPM)<br>Ø∂,<br>Wel production (Imin)<br>Disinfected?<br>(B) Yes No<br>Please provide a ma<br>341 m<br>Comments:  | sPM)<br>min<br>of pumping (PM)<br>invGPM)<br>odepth(Traft)<br>1<br>73<br>T3<br>T3<br>T3<br>T3<br>T3<br>T3<br>T3<br>T3<br>T3<br>T   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>Hell Loo   | 14.00<br>14.03<br>15.63<br>18.40<br>21.06<br>23.10<br>24.01<br>25.33<br>21.55<br>24.20<br>30.45<br>30.45  | 3     3       4     5       5     10       5     10       5     20       7     25       3     30       3     60  | 25-38<br>34-57<br>30-71<br>27-85<br>25-33<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-71<br>17-28<br>15-8<br>15-8  |
| Met<br>Cable Ti<br>Robary (I<br>Boring)<br>Other, a<br>anneter<br>Din)<br>S. 24<br>(<br>), 16<br>(<br>), 16<br>(), 16)(),  | triod of Cor<br>and Conventional<br>Salary<br>Conventional<br>Reverse)<br>sssion<br>Open Hole<br>(Galvanzow<br>Concrete, F<br>Steel +<br>Steel +<br>Concrete, F<br>Steel +<br>Concrete, F<br>Concrete, F<br>Steel +<br>Concrete, F<br>S   | I Diamond I detting Diamond J detting Diamond J detting Digging I  | Cord - Sc<br>Sot No.<br>12<br>ify<br>Fresh<br>ify<br>Fresh<br>ify<br>Business<br>P<br>P<br>D<br>P<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D   | Ablic<br>mestic<br>vestock<br>(gation<br>Austral<br>her, specify<br>From<br>1,5D<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45:7,2<br>45  | Well Us           □ comme           □ Muricipa           Muricipa           □ To           □ Cooling           □ 46.63           46.63           46.63           46.63           46.63           46.63           46.63           46.63           46.63           46.63           46.63           46.63           46.63           46.63           46.63           47.85           0           6.99           n Informati           Mu           Mu           Mu           Mu           Mu           Muse           Muse  | Status   | Not used<br>Deviatering<br>Johanson<br>Suppy<br>ament Well<br>aring We | Pumping rate (Imp) /<br>20.713<br>Duration of pumping<br>(hrs +i)<br>Final water level and o<br>38.9<br>H flowing give rate (Im<br>Recommended pump<br>(Im) GPN)<br>Wel production (Imiv)<br>Disinfected?<br>(Im) GPN)<br>Please provide a me<br>341 m<br>Comments:<br>Well pumper   Duti   | sPM)<br>min<br>of pumping (m<br>invGPM)<br>odepth(fm)<br>1<br>rate<br>73<br>GPM)<br>Map of M<br>ap below follow<br>Huxy E<br>(99)  | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60<br>14<br>50   | 14.00<br>14.03<br>15.63<br>18.40<br>23.00<br>24.01<br>25.33<br>21.58<br>23.00<br>25.33<br>27.58<br>29.30<br>30.48<br>30.48  | 3     3       4     5       5     10       5     10       5     20       7     25       3     30       3     60  | 25-38<br>34-59<br>30-71<br>27-85<br>25-23<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>23-43<br>17-28<br>15-81   |
| Met<br>Cable Ti<br>Robary (I<br>Boring)<br>Other, a<br>meter<br>Diff<br>Diff<br>Diff<br>Diff<br>Diff<br>Diff<br>Diff<br>Dif   | Triba of Cor<br>Triba of Cor<br>Sol<br>Conventional<br>Reverse)<br>assion<br>Open Hole<br>(Galvanizes<br>Concrete, F<br>Steel +<br>Steel +<br>Con<br>(Plastic, Galv<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>Stat<br>St | Barnond Barno  | Cord - Ca<br>Wal<br>Wal<br>The fresh<br>is 477<br>.477<br>.477<br>.477<br>.477<br>.477<br>.477<br>.477   | Ablic<br>mestic<br>vestock<br>(gation<br>Austrial<br>her, specify<br>From<br>+,SD<br>45:7,2<br>45:7,2<br>Feen<br>0ept<br>From<br>46,63<br>Untested<br>Untested<br>Untested<br>Cechnician (I<br>econnician (I)   | Well Us           □ Comme           □ Municipy           ☑ Test Hok           □ Cooling           ☑           ☑           □ Municipy           ☑ Test Hok           □ Cooling           ☑   | Status   | Not used Deviating Noticering Noticering Noticering Noticering Noticering Note Provide Note Note Note Note Note Note Note Not  | Pumping rate (Imp) (<br>20.713<br>Duration of pumping<br>(  | Package Delivi   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>40<br>50<br>60<br>60<br>40   | 14.00<br>14.03<br>15.63<br>18.40<br>91.06<br>93.10<br>93.10<br>93.10<br>97.58<br>97.58<br>97.90<br>30.42<br>30.42<br>30.42  | 3     3       4     5       10     15       20     15       20     20       3     60   | 35-38       34.59       30.71       37.85       33.43       33.43       33.43       33.43       33.43       31.73       17.86       15.81       *       *       *       *       *       *       *       *       *   |
| Met<br>Aber To<br>Aber V<br>Aber V  | trod of Cor<br>rod of Cor<br>correntional<br>rotorer for<br>correntional<br>rotorer for<br>corrett, F<br>Corrett, F<br>Steel +<br>Steel +<br>Corrett, F<br>Steel +<br>Corrett, F<br>Corrett, F<br>Steel +<br>Corrett, F<br>Corrett, F<br>Steel +<br>Corrett, F<br>Steel +<br>Corrett, F<br>Steel +<br>Corrett, F<br>Steel +<br>Corrett, F<br>Corrett, F<br>Steel +<br>Corrett, F<br>Steel +<br>Corrett, F<br>Corrett,   | Struction Re<br>Struction Re<br>S  | Cord - Ca<br>Wal<br>Wal<br>Wal<br>Cord - Ca<br>Wal<br>Wal<br>Cord - Ca<br>Wal<br>Cord - Ca<br>Cord  | Ablic<br>mestic<br>vestock<br>(gation<br>Austrial<br>her, specify<br>From<br>+, SD<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2<br>45.7,2  | Well Us           □ Comme           □ Municipy           ☑ Test Hok           □ Cooling           ☑           ☑           □ Φ(π)           To           46.63           47.85           60.79           Mu   | Status   | Not used Devatering Monitoring Supply ament Well sering Well seri  | Pumping rate (Imp) (<br>20.713<br>Duration of pumping<br>(  | Package Deliv<br>SPM)<br>min<br>of pumping (Pit<br>in/GPM)<br>odepth (Tit)<br>1<br>T3<br>(GPM)<br>Map of M<br>p below follow<br>Hacy E<br>(SPM)<br>Package Deliv<br>(SPM)<br>SPALE (SPM)   | 3         4           5         10           15         20           25         30           40         50           60         60           Mell Loc         15           ered         14   | 14.00<br>14.03<br>15.63<br>18.40<br>91.06<br>93.10<br>93.10<br>93.10<br>93.10<br>97.58<br>97.58<br>97.58<br>97.58<br>97.58<br>97.58   | 3     4       5     10       0     15       0     20       7     25       3     30       3     60       3     60       4     50       5     50       5     50       3     60       5     50       5     50       5     50       5     50       5     50       5     60       5     50       5     50       5     60       5     50       5     50       5     60       5     50       5 | 25-38<br>34.59<br>30-71<br>27.85<br>25-23<br>23.43<br>21.73<br>19.01<br>17.28<br>15.81<br>*   |
| Met<br>Cable TC<br>Cable TC<br>Rotary ( )<br>Baring<br>Cher, s<br>made<br>metar<br>()<br>Cher, s<br>made<br>()<br>Cher, s<br>made<br>()<br>Cher, s<br>mater<br>()<br>Cher, s<br>()<br>Cher, s<br>()   | tribut of Lor         conventional         conventional         Reverse)         sssion          con         conventional         Conventional         conventional         conventional         convent         Convenve   |  | Cord - Ca<br>Wal<br>Wal<br>Thichess<br>Off)<br>3 477<br>.977<br>.977<br>.977<br>.977<br>.977<br>.977<br>.977   | Ablic<br>mestic<br>vestock<br>(gation<br>Austrial<br>her, specify<br>From<br>4,5D<br>45.7,2<br>45.7,2<br>From<br>46,63<br>Untested<br>Untested<br>Untested<br>Untested<br>Cennician<br>(L<br>Cennician (L<br>Cennician (L<br>Cennician (L<br>Cennician (L)<br>Cennician (L)<br>Cennic  | Well Us           Comme           Municipa           Mu   | Status   | Not used Deviatering Wonlocking Suppy ement Well set go Well rring Well rrin  | Pumping rate (Imp) (<br>20.713<br>Duration of pumping<br>6_hrs+0_i<br>Final water level and (<br>38.95<br>If flowing give rate (Im<br>Recommended pump<br>45.1<br>Recommended pump<br>(Im) CPM)<br>20.7<br>Vel production (Imin<br>Disinfected?<br>(Im) CPM)<br>20.7<br>Vel production (Imin<br>0<br>Comments:<br>Vel owner's<br>Information<br>package<br>delivered<br>Xes<br>Date<br>Information<br>Date<br>Information<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date<br>Date | Package Deliv<br>Package Deliv<br>Normalian<br>Package Deliv<br>Normalian<br>Package Deliv<br>Normalian<br>Package Deliv<br>Normalian<br>Package Deliv<br>Normalian<br>Package Deliv<br>Normalian<br>Package Deliv   | 3         4           5         10           15         20           225         30           40         50           60         60           Mail Local         60           India Local         60 | 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| Grey  |   | clay!   |  |   | 0  | silt   |   |  |   |   | 2.74   | 30   |
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| .!  |   |   |  |   |  | 0  | and an order  |  |   |   |  | -  |
| 1916  |   |   |  | I.  | il-inne  | A De la  |   |  | -   |   |  |  |
|   |   |   |  |   |  | 1. 63 . 34   |   |  |   |   |  |  |
| 1.1.1.4.2   |   |   |  |   |  | and the second second  | a subject of the set  |  |   |   |  |  |
| 1.5   |   |   |  |   |  | and and hered  |   | in the second  |   | Sector 1  |  |  |
| 5 20  |   |   |  |   |  | 1 1 1 1  |   |  |   |   |  |  |
| 20403   |   | 494751  | Annula   | r Space   | 1820 C   | CENSING STRAND   | 200 NA 120  | Results of W   | ell Yie   | ld Testing  | 124  | siege (  |
| Depth S   | Set at (n)  |   | Type of Se   | ealant Used   |  | Volume Placed  | After test of well yi   | eld, water was:<br>nd free   | Di  | Water Lev   | Fime   | Water  |
|   | 10  | -   | P. al  | .10   |  | 21   | Other, specify  | y  | (min)   | ( <b>O</b> n)   | (min)  | 0  |
| 0   | 6.7   |   | Seritor  | rite  |  |  | If pumping discont  | inued, give reason   | Level   | 155   | 4  |  |
| 1 100   | 1   |   |  |   |  |  |   |  | 1   | 16.41   | 1  | 18:5   |
|   | -   |   |  | 3   |  |  | Pump intake set at  | ( <b>A</b> n)  | 2   | 16:71   | 2  | 18.  |
|   |   | elines a  | and and  |   |  | a des alla des   | 30.4  | S COM  | 3   | 1696  | 3  | 17   |
| Mot   | thad of Co  | nstruction  | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1  | 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1  | Well L   | lee  | Pumping rates with  | GEMI   |   | 10.10   | -  |  |
| Cold returns  |   | insu ucuon  | 1.1 C  | A the surface   | C Days   | 196  | 13.63   | Sector Lot States  | 4   | 175   | - 4  | 170  |
| Cable To  | bol<br>Conventional   | Diamon  |  | ublic   |  | rencial Dewatering   | 13,63<br>Duration of pumpir   | 10   | 4   | 17.15   | - 4  | 17.  |
| Cable Te  | bol<br>Conventional<br>Raverse)   | Diamon  |  | ublic<br>Iomestic<br>ivestock   | Comm<br>Munici   | rencial Not used<br>Ipal Dewatering<br>Iole Monitoring   | 13,63<br>Duration of pumpin<br><u>b</u> hrs + O   | ng<br>min  | 4   | 17.15   | 5  | 17.  |
| Cable R<br>Cable R<br>Rotary (<br>Rotary (<br>Boring<br>Air perc.   | bol<br>Conventional,<br>Raverse)  | Diamon Diamon Jetting Driving Digging   |  | ublic<br>Iomestic<br>ivestock<br>rigation<br>idustrial  | Comm<br>Munici<br>Test H   | rercial Not used<br>pal Dewatering<br>ole Monitoring<br>g & Air Conditioning   | 13,63<br>Duration of pumpir<br>b hrs + O<br>Final water level er  | ng<br>min<br>Ind of pumping @M   | 4<br>5<br>10  | 17.15<br>17.33<br>17.92   | 4<br>5<br>10   | 17.9<br>17.<br>16.   |
| Cable R<br>Rotary (<br>Rotary (<br>Boring<br>Air perc.<br>Other, sp   | bol<br>Conventional,<br>Raverse)<br>ussion<br>pecify  | Diamon Diamon J Ustting Driving Digging   |  | ublic<br>tomestic<br>ivestock<br>rigation<br>idustrial<br>ther, specify   | Comm<br>Munici<br>Mart H   | rencial Not used<br>pal Dewatering<br>ole Monitoring<br>g & Air Conditioning   | 13,63<br>Duration of pumpin<br><u>b</u> hrs + O<br>Final water level er<br>/9.0<br>If flowing give rate   | ng<br>min<br>nd of pumping @ft<br>07<br>(/min/GPM)   | 4<br>5<br>10<br>15  | 17.15<br>17.33<br>17.92<br>18.06  | 4<br>5<br>10<br>3 15   | 17.<br>17.<br>16.<br>15  |
| Cable R<br>Cable R<br>Rotary (<br>Rotary (<br>Boring<br>Air perc.<br>Other, sp  | Conventional,<br>Raverse)<br>ussion<br>pecifyCo   | Diamon Jetting Diying Digging   | d   P<br>  D<br>  U<br>  III<br>  III   III<br>  III   II | Aublic<br>Aomestic<br>Avestock<br>rigation<br>dustrial<br>Other, specify  | Comm<br>Munici<br>St Test H<br>Coolin  | recial Not used<br>pal Dewatering<br>ole Monitoring<br>g & Air Conditioning  | 13,63<br>Duration of pumpir<br><u>b</u> hrs + <u>O</u><br>Final water level er<br><u>19.0</u><br>If flowing give rate   | ng<br>min<br>d of pumping @M<br>7<br>(Amin/GPM)<br>mp depth (MTD)  | 4<br>5<br>10<br>15<br>20  | 17.15<br>17.33<br>17.92<br>18.02<br>18.02   | 4<br>5<br>10<br>3<br>15<br>20  | 17.<br>17.<br>16.<br>15.   |
| Cable Tr<br>Cable Tr<br>Cable Tr<br>Cable Tr<br>Rotary (<br>Boring<br>Air perc.<br>Other, sp<br>Inside<br>Diamoter  | Conventional<br>Conventional<br>Reverse)<br>ussion<br>pecify<br>Con<br>Open Hol<br>(Galvanics<br>Convention   | Diamon     Diamon     Diating     Driving     Digging     Digging     Digging     Digging     driving     drivingiass,     dritretteteeeeeeeeeeeeeeeeeeeeeeeeeeeeee             | d P<br>D<br>L<br>I<br>I<br>I<br>Record - Ca<br>Wal<br>Thickness  | Aublic<br>komestic<br>ivestock<br>rigation<br>vdustrial<br>ther, specify<br>ising<br>Dep<br>From  | Comm<br>Munici<br>SC Test H<br>Coolin<br>coolin<br>th (C)T()<br>To   | recial Not used<br>pal Dewatering<br>ole Monitoring<br>g & Air Conditioning<br>Status of Well<br>Ø Water Supply<br>Replacement Well  | 13.63<br>Duration of pumpin<br><u>b</u> hrs + <u>O</u><br>Final water level er<br>/9.0<br>If flowing give rate  | rg<br>min<br>hd of pumping 例和<br>)7<br>(/min/GPM)<br>mp depth (例讯)<br> 各   | 4<br>5<br>10<br>15<br>20<br>25  | 17.15<br>17.33<br>17.92<br>18.02<br>18.95   | 4<br>5<br>10<br>3<br>15<br>20<br>25  | 17.<br>17.<br>16<br>16<br>15.  |
| Cable T<br>Cable T<br>Rotary (<br>Rotary (<br>Boring<br>Air perc.<br>Other, sp<br>Inside<br>Diamoter<br>Diamoter  | Conventional<br>Conventional<br>Raverse)<br>ussion<br>pecify<br>Con<br>(Galvaniz<br>Concrete,   | Diamon Diamon Diamon Diamon Diatting Driving Digging Digging Retruction F e OR Material ad, Fibreglass, Ad, Fibreglass, Steel)  | d P<br>D<br>U<br>U<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I  | wblic<br>kornestic<br>ivestock<br>rigation<br>dustrial<br>ther, specify<br>ising<br>Dep<br>From   | Comm     Munici     Monici     St Test H     Coolin     Coolin     th (1)     To     To     27 41  | ercial   Not used<br>pal   Dewatering<br>ole   Monitoring<br>g & Air Conditioning<br>  | 13.63<br>Duration of pumpin<br><u>b</u> hrs + <u>O</u><br>Final water level er<br>19.00<br>If flowing give rate<br>Recommended pu<br>30.4<br>Recommended pu<br>30.4   | ng<br>min<br>Ind of pumping @fit<br>(/min/GP/M)<br>mp depth (@fit)<br> 8<br>mp rake  | 4<br>5<br>10<br>15<br>20<br>25<br>30  | 17.15<br>17.33<br>17.92<br>18.02<br>18.95<br>18.40  | 4<br>5<br>10<br>3<br>15<br>5<br>20<br>25<br>30   | 17.<br>17.<br>16<br>15.<br>15.   |
| Cable TR<br>Totary (<br>Rotary (<br>Boring<br>Air perc.<br>Other, sp<br>Inside<br>Diamotor<br>Other, sp<br>Inside<br>Diamotor<br>()<br>()<br>()<br>()<br>()<br>()<br>()<br>()<br>()<br>()   | Conventional<br>Raverse)<br>ussion<br>pecify<br>Con<br>(Galvaniz<br>Concrete,   | Diamon Diamon Diating Diating Diying Digging Oigging  | d P<br>D<br>D<br>U<br>U<br>U<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I<br>I  | ublic<br>ormestic<br>ivestock<br>rigation<br>webstrial<br>ther, specify<br>sing<br>From<br>+,45   | Comm<br>Munici<br>Munici<br>Mirist H<br>Coolin<br>the (7011)<br>To<br>32.9(1   | so     creat     crea      | 13.63<br>Duration of pumpin<br><u>b</u> hrs + O<br>Final water level er<br>19.0<br>If flowing give rate<br>Recommended pu<br>30.4<br>Recommended pu<br>30.4<br>Recommended pu<br>13.63  | 9min<br>nd of pumping @11<br>07(MinivGPM)<br>mp depth (@11)<br>(8)<br>mp rate<br>233   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40  | 17.15<br>17.33<br>17.42<br>18.02<br>18.95<br>18.40<br>18.49   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40   | 17.<br>17.<br>16.<br>15.<br>15.  |
| Cable TR<br>Cable TR<br>Rotary (<br>Boring<br>Air pero.<br>Other, sy<br>Inside<br>Diarnoter<br>Other, sy<br>Inside<br>Diarnoter<br>Other, sy<br>Inside<br>Diarnoter   | Conventional<br>Raverse)<br>ussion<br>pecify<br>Open Hol<br>(Gatvarias<br>Concrete,   | Diamon Diamon Diating Diating Driving Digging e OR Material d, Fibreglass, Plastic, Steel)  | Ceccord - Ca<br>Wall<br>Thickness<br>Constraint<br>477<br>- 477  | ublic<br>kornestic<br>ivestock<br>rigation<br>kdustrial<br>ther, specify<br>ising<br>From<br>From<br>+.45<br>30.00  | Comm<br>Munici<br>20 Test H<br>Coolin<br>the (0011)<br>To<br>332.9(1<br>5) 332.9(1   | sectary Well     Observation and/or     Monitoring   | 13.63<br>Duration of pumpin<br><u>b</u> hrs + <u>O</u><br>Final water level er<br>19.0<br>If flowing give rate<br>Recommended pu<br>30.4<br>Recommended pu<br>13.6<br>Well production (fr   | min<br>min<br>of pumping (1)<br>of<br>(min/GPM)<br>mp depth (1)<br>(18<br>mp rate<br>33<br>min/GPM)  | 4<br>5<br>0 10<br>15<br>20<br>25<br>30<br>40<br>50                                  | 17.15<br>17.33<br>17.97<br>18.06<br>18.49<br>18.49<br>18.49   | 4<br>5<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>25<br>30<br>40<br>40  | 17.<br>17.<br>16<br>15<br>15   |
| Cable R<br>Cable R<br>Cable R<br>Cable R<br>Rotary (<br>Rotary (<br>Rotary (<br>Barrieg<br>Ar pero.<br>Other, s<br>Inside<br>Diamoter<br>(Diamoter<br>(Diamoter<br>(Diamoter<br>(Diamoter)<br>(Diamoter<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diamoter)<br>(Diam  | Convertional<br>Raverse)<br>ussion<br>perity<br>Convertional<br>(Galvanize<br>Concrete,<br>Steel =  | Diamon     Diamon     Diamon     Disting     Diving     Digging     Digging     differential     diferential     differe     | Record - Ca<br>Wall<br>Trickness<br>(97in)<br>- 477<br>- 477   | ublic<br>kornestic<br>kvestock<br>rigation<br>dustrial<br>ther, specify<br>ising<br>From<br>+, 45   | Comm<br>Munici<br>Munici<br>Test H<br>Coolin<br>To<br>32.91  | recial Not used<br>pal Dewatering<br>ole Monitoring<br>g & Air Conditioning<br>Status of Well<br>Status of Well<br>Status of Well<br>Replacement Well<br>Status Autor and/or<br>Recharge Well<br>Dewratering Well<br>Observation and/or<br>Monitoring Hole<br>Atteration<br>(Construction)   | 13.63<br>Duration of pumpir<br>http://www.endor.org/<br>Final water level er<br>If flowing give rate<br>Recommended pu<br>Recommended pu<br>13.6<br>Weil production (/m<br>Desinfected?   | min<br>min<br>of pumping @n<br>of<br>mp depth (@nt)<br>(8<br>mp rate<br>53<br>min/GPM)   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50                                    | 17.15<br>17.33<br>17.92<br>18.05<br>18.40<br>18.40<br>18.41<br>18.50<br>18.55   | 4<br>5<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>25<br>30<br>40<br>50  | 17.<br>17.<br>16.<br>15.<br>15.  |
| Cable R<br>Cable R<br>Cable R<br>Rotary (<br>Rotary (<br>Rotary (<br>Barnoter<br>Const<br>Const<br>(S.24)<br>/0.16  | Conventional<br>Conventional<br>Reverse)<br>ussion<br>peoly<br>Converse)<br>Converse<br>Converse<br>Converse<br>State   | Diamon<br>Diamon<br>Disting<br>Diving<br>Digging<br>nstruction F<br>e OR Material<br>A, Fibreglas, Steel)<br>el<br>k pocket   | tecord - Ca<br>Thickness<br>Thickness<br>(7)11<br>- 477<br>- 477   | ublic<br>kornestic<br>krestlock<br>rigation<br>dutshtal<br>ther, specify<br>ising<br>From<br>+,45<br>33,000   | Comm<br>Munici<br>Manici<br>Mariat H<br>Coolin<br>To<br>32.9(1<br>5) 32.9(1  | rectal   Not used<br>pal Dewatering<br>ole   Monitoring<br>g & Air Conditioning<br>Status of Well<br>  Status of Well<br>  Status of Well<br>  Replacement Well<br>  Bg Test Hole<br>  Dewatering Well<br>  Observation and/or<br>Monitoring Hole<br>  Abandoned,<br>  Instificioni Sundu  | 13.63           Duration of pumping   | min<br>min<br>of pumping @1<br>of<br>(min/GPM)<br>mp rate<br>3<br>3<br>min/GPM)  | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60                              | 17.15<br>17.33<br>17.17<br>18.05<br>18.40<br>18.41<br>18.41<br>18.51<br>18.55<br>18.55  | 4<br>5<br>5<br>10<br>3<br>15<br>20<br>25<br>30<br>25<br>30<br>40<br>50<br>7<br>60  | 17.<br>17.<br>16<br>15<br>15   |
| Cable R<br>Cable R<br>Cable Robury (<br>Robury (<br>Robury (<br>Dornet<br>Cober, sp<br>Cober, sp<br>Cobe  | Conventional<br>Conventional<br>Reverse)<br>ussion<br>poolly<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventional<br>Conventi  | Diamon<br>Diamon<br>Disting<br>Diving<br>Digging<br>nstruction F<br>e OR Material<br>d, Fibreglass, Steel)<br>el<br>K packet<br>nstruction F  | Vecord - Ca<br>Wall<br>Thickness<br>Copini<br>4477   | ublic<br>kornestic<br>krestlock<br>rigation<br>kalsstrial<br>ther, specify<br>sing<br>From<br>+,45<br>32,00   | Comr<br>Munici<br>St Test H<br>Coolin<br>To<br>S9.9(1<br>S9.9(1  | sector         erclai         Construction         Status of Well         Abandoned, Paos         Abandoned, Poor  | 13.63       Duration of pumping   | min<br>min<br>of pumping @fi<br>of<br>(min/GPM)<br>mp rate<br>3<br>3<br>min/GPM)<br>map below follow   | 4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60                        | 17.15<br>17.33<br>17.10<br>18.40<br>18.40<br>18.40<br>18.40<br>18.50<br>18.50<br>18.55<br>18.55   | 4<br>5<br>5<br>10<br>3<br>15<br>20<br>25<br>30<br>25<br>30<br>40<br>50<br>60   | 17.1   |
| Cable R<br>Cable R<br>Rotary (<br>Boring<br>Boring<br>Ar perco.<br>Other, sp<br>Diamoter<br>Diamoter<br>(C)(n)<br>/(C, C)<br>/(C, C)<br>/(C)<br>/(C, C)<br>/(C, C)<br>/(C, C)<br>/(C,  | Dod<br>Conventional<br>Raverse)<br>ussion<br>poolly<br>Converse)<br>Con<br>Con<br>Con Hol<br>(Calvania<br>Concrete,<br>Steel 4  | Diamon     Diamon     Diamon     Disting     Diving     Digging     Digging     differential     differ     | d P<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D   | ublic<br>tomestic<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treasfork<br>treas  | Comr<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Munici<br>Muni | sector         Air Conditioning         Status of Well         Status         Status of Well         Status of Well         Status of Well         Status of Well         Status         | 13.63       Duration of pumping   | min<br>min<br>of pumping @fl<br>of<br>(train/GPM)<br>mp rate<br>3<br>3<br>min/GPM)<br>map below follow<br>with St  | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>Well Loo                  | 17.15<br>17.33<br>17.92<br>18.40<br>18.40<br>18.49<br>18.49<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55  | 4<br>5<br>5<br>10<br>3<br>15<br>20<br>5<br>25<br>30<br>5<br>40<br>5<br>50<br>7<br>60   | 17.<br>17.<br>16.<br>15.<br>15.<br>15.                                   |
| Cable R<br>Cable R<br>Rotary (<br>Cable R<br>Boring<br>Darnoter<br>Diarnoter<br>Diarnoter<br>Cable<br>(<br>Cotes de<br>Cable<br>(<br>Cotes de<br>Cable<br>(<br>Cotes de<br>Cable<br>(<br>Cable R<br>Cable   | Doi<br>Conventional<br>Reverse)<br>ussion<br>pooly<br>Con<br>Open Hol<br>(Galvaniz<br>Concrete,<br>Steel 4<br>Steel 4<br>(Plastic, Gal  | Diamon     Diamon     Diamon     Disting     Diving     Digging     Orgging     Orgging     Orgging     Orgging     Arbregist     K. pocket     Instruction F aterial     Variad, Steel)  | d P<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D   | ublic<br>tomestic<br>twestock<br>trigation<br>dustrial<br>ther, specify<br>ising<br>Dep<br>From<br>+,45<br>32,00<br>reeen<br>Dep<br>From  | Comm     Munici  | Status of Well Statu  | 13.63       Duration of pumpin  | min<br>min<br>of of pumping @M<br>of<br>(train/GPM)<br>mp depth (ff(R)<br>[8<br>mp rate<br>3<br>3<br>min/GPM)<br>map below follow<br>aty 89  | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>Well Loo                  | 17.15<br>17.33<br>17.92<br>18.40<br>18.40<br>18.49<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55  | 4<br>5<br>5<br>10<br>3<br>15<br>20<br>5<br>25<br>30<br>5<br>40<br>5<br>50<br>60<br>50<br>1<br>60   | 17.<br>17.<br>16.<br>15.<br>15.  |
| Cable R<br>Cable R<br>Caury (<br>Cable R<br>Dornote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Canote<br>Cano   | Dol<br>Conventional<br>Reverse)<br>ussion<br>pooly<br>Con<br>Open Hol<br>(Galvaniz<br>Concrete,<br>Steel 4<br>Steel 4<br>(Plastic Gal<br>State)   | Diamon     Diamon     Diamon     Disting     Diving     Digging     Orgging     Orgging     Orgging     Krocket     Krocket     Krocket     Material     Krocket     Material     Krocket   | Record - Ca<br>Wall<br>Wall<br>Wall<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>Wall<br>COM<br>COM<br>COM<br>COM<br>COM<br>COM<br>COM<br>COM<br>COM<br>COM   | ublic<br>tomestic<br>twestock<br>trigation<br>dustrial<br>ther, specify<br>ising<br>Dep<br>From<br>+,45<br>32,00<br>reeen<br>Dep<br>From<br>32,21   | Comm     Munici  | Status of Well  Construction  Construction  Attention  Attention  Attention  Attention  Construction  Const  | 13.63       Duration of pumpin  | min<br>min<br>of of pumping @M<br>of<br>(Imir/GPM)<br>mp depth (ff(R)<br>8<br>mp rate<br>3<br>mir/GPM)<br>map below follow<br>with generation<br>map below follow  | 4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>60<br>60<br>Vieti Loo           | 17.15<br>17.33<br>17.92<br>18.40<br>18.40<br>18.49<br>18.49<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55  | 4<br>5<br>5<br>10<br>3<br>15<br>20<br>25<br>30<br>25<br>30<br>5<br>40<br>5<br>6<br>0<br>1<br>60  | 17. 16 15. 15<br>15  |
| Cable R<br>Cable R<br>Cable R<br>Caury (<br>Cable Ar perc<br>Other, s<br>Cable<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Const   | Dol<br>Conventional<br>Reverse)<br>ussion<br>pooly<br>Converse)<br>Converse<br>Converse<br>Steel 4<br>Steel 4<br>(Plastic Call  | Instruction F Construction F Constr | Image: Control of Con  | ublic<br>komestic<br>krestock<br>rigation<br>vdustrial<br>ther, specify<br>From<br>+,45<br>30.00<br>Freen<br>200<br>From<br>32.91   | Comm<br>Munici<br>St Test H<br>Coolin<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>Solution<br>S   | sector         Abandoned, other, specify   | 13.63<br>Duration of pumpin<br>hrs + O<br>Final water level er<br>179.0<br>If flowing give rate<br>Recommended pu<br>30.4<br>Recommended pu<br>30.4<br>Recommended pu<br>30.4<br>Recommended pu<br>30.4<br>Recommended pu<br>30.4<br>Please provide a<br>Please provide a   | min<br>d of pumping (1)<br>7<br>(MnivGPM)<br>mp depth (1)<br>(8<br>mp rate<br>3<br>mivGPM)<br>Map of M<br>map below follow<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10   | 4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>Well Low            | 17.15<br>17.33<br>17.92<br>18.46<br>18.49<br>18.49<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55  | 4<br>5<br>5<br>10<br>3<br>15<br>5<br>20<br>7<br>25<br>30<br>7<br>5<br>0<br>5<br>50<br>7<br>60<br>8<br>40<br>8<br>50<br>7<br>60   | 17.<br>17.<br>16.<br>15.<br>15.<br>15.                                   |
| Cable R<br>Cable R<br>Cable R<br>Caury (<br>Cables R<br>Cables  | Dol<br>Conventional<br>Reverse)<br>sssion<br>pooly<br>Concels<br>Concrete,<br>Stee<br>Stee<br>Automatic<br>Plastic, Gal   | Bianon     Diamon     Diamon     Disting     Diving     Digging     Digging     e OR Material     d. Fibreglass, Plastic, Steel)     el     k pocket     mstruction F aterial     wantzed, Steel     wantzed, Steel     wantzed, Steel  | d P<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D   | ublic<br>komestic<br>kvestock<br>rigation<br>xdustrial<br>ther, specify<br>ising<br>From<br>+.45<br>33.000<br>reen<br>pop<br>From<br>32.91  | Comm     Munici  | sec     secc     sec     secc     seccc     seccc     seccc     seccc     seccc     secccc     secccc     secccccccccc   | 13.63<br>Duration of pumpin<br>hrs + O<br>Final water level or<br>/9.0<br>If flowing give rate<br>Recommended pu<br>30.4<br>Recommended pu<br>30.4<br>Recommended pu<br>30.4<br>Recommended pu<br>30.4<br>Recommended pu<br>30.4<br>Please provide a<br>Please provide a  | min<br>min<br>of pumping (3)<br>7<br>(Amir/GPM)<br>mp depth (6)<br>(Map of M<br>may below follow<br>All y 8<br>(Map of M<br>map below follow<br>(All y 8<br>(All | 4<br>5<br>0<br>10<br>15<br>25<br>30<br>40<br>50<br>60<br>well Loo                   | 17.15<br>17.33<br>17.92<br>18.46<br>18.49<br>18.49<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55  | 4<br>5<br>5<br>10<br>3<br>15<br>5<br>20<br>5<br>25<br>30<br>5<br>25<br>30<br>5<br>40<br>5<br>5<br>60<br>3<br>60  | 17.<br>17.<br>16<br>15.<br>15  |
| Cable R<br>Cable R<br>R Rolary (<br>Rolary (<br>Rolary (<br>Rolary (<br>Rolary (<br>Rolary (<br>Cable R<br>Rolary (<br>Rolary (<br>Rola   | Dool<br>Conventional<br>Reverse)<br>sssion<br>pooly<br>Concrete,<br>Concrete,<br>Stee<br>stee<br>Concrete,<br>Stee<br>stee<br>concrete,<br>Stee<br>stee<br>concrete,<br>Concrete,<br>Stee<br>concrete,<br>Concrete,<br>Stee<br>concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concrete,<br>Concre   | Biamon     Diamon     Diamon     Disting     Diving     Digging     Digging     e OR Material     d, Fibredias, Plastic, Steel)     el     kendidate Steel     kendidate Steel     watter Dei     Kind of Water     E   | d P<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D   | ublic<br>komestic<br>ivestock<br>ingation<br>xdustrial<br>ther, specify<br>ising<br>From<br>+.45<br>30.00<br>From<br>500<br>From<br>30.00<br>From<br>30.00  | Comm     Munici  | sector      | 13.63       Duration of pumpin       b hrs + O       Final water level er       17 flowing give rate       Recommended pu       30.4       Recommended pu       30.4       Recommended pu       30.4       Production (tr      Disinfected?       Ø Yes       No  | min<br>dof pumping (9)<br>7<br>(knin/GPM)<br>mp depth (9)<br>(knin/GPM)<br>mp rate<br>3<br>min/GPM)<br>Map of M<br>map below follow<br>x5 y 8<br>e<br>e<br>e<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-  | 4<br>5<br>0<br>10<br>15<br>25<br>30<br>40<br>50<br>60<br>60<br>Well Low             | 17.15<br>17.33<br>17.92<br>18.40<br>18.49<br>18.49<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55   | 4<br>5<br>5<br>10<br>3<br>15<br>20<br>5<br>25<br>30<br>25<br>30<br>25<br>30<br>5<br>40<br>5<br>50<br>1<br>60   | 17.<br>17.<br>16.<br>15.<br>15.<br>15.<br>15.<br>15.<br>15.<br>15.<br>15 |
| Cable R<br>Cable R<br>R Rolary (<br>Rolary (<br>Rolary (<br>Rolary (<br>Rolary (<br>Check, s<br>Check, s<br>Check, 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ool<br>Conventional<br>Reverse)<br>sasion<br>pooly<br>Converse)<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Convers  | Diamon     Diamon     Diamon     Disting     Diving     Digging     Organg     Retriction F     e OR Material     Arbreglass, Plastic, Steel)     E     Kind of Watee     Kind of Watee   | d         P           d         P           D         D           D         D           Image: State of the state o  | tubic<br>kornestic<br>ivestock<br>ingation<br>dustrial<br>ther, specify<br>ising<br>From<br>+.45<br>30.00<br>From<br>Construction<br>From<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45<br>1.45 | Comm     Munici  | Status of Well  Status of Wel  | 13.63       Duration of pumpin  | min<br>dof pumping (5)<br>7<br>(kmin/GPM)<br>mp depth (5)<br>(B<br>mp rate<br>3<br>min/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(kmin/GPM)<br>(   | 4<br>5<br>0<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60                   | 17.15<br>17.33<br>17.92<br>18.40<br>18.49<br>18.49<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55   | 4<br>5<br>5<br>10<br>3<br>15<br>20<br>5<br>25<br>30<br>25<br>30<br>25<br>30<br>5<br>0<br>25<br>30<br>60<br>8<br>8<br>40  | 17. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15                               |
| Cable R<br>Cable R<br>Cable R<br>Caury (<br>Boring<br>Doring<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Diameter<br>Constance<br>Constance<br>Diameter<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Const   | ool<br>Conventional<br>Reverse)<br>sasion<br>pocify<br>Converse)<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Conve   | Diamon     Diamon     Disting     Diving     Digging     Orging     Orging     of Addrial     Affrequess,     Plastic, Steel)     E     E     Kind of Water     Other, spe     Kind of Water  | d P<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D   | ublic<br>kornestic<br>ivestock<br>ingation<br>dustrial<br>ther, specify<br>ising<br>From<br>+.45<br>30.00<br>From<br>From<br>30.00<br>From<br>30.00<br>From   | Comm     Munici  | Air Conditioning     Status of Well     Dewatering     de    Monitoring     Status of Well     Status       | 13.63<br>Duration of pumpir<br><u>b</u> hrs + <u>0</u><br>Final water level er<br>If flowing give rate<br>Recommended pu<br><u>30.7</u><br>Well production (/m<br>Disinfected?<br><u>80</u> Yes <u>No</u><br>Please provide a<br><u>4</u><br><u>4</u><br><u>4</u><br><u>4</u><br><u>4</u><br><u>4</u><br><u>4</u><br><u>4</u> | min<br>min<br>of of pumping @M<br>of<br>(min/GPM)<br>mp rate<br>33<br>min/GPM)<br>Map of M<br>map below follow<br>of y 81<br>e<br>e<br>e<br>e<br>e<br>e<br>e<br>e<br>e<br>e<br>f<br>+7m  | 4<br>5<br>0<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>Well Loo       | 17.15<br>17.33<br>17.92<br>18.46<br>18.49<br>18.49<br>18.49<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55   | 4<br>5<br>5<br>10<br>3<br>15<br>20<br>25<br>30<br>25<br>30<br>40<br>50<br>40<br>60   | 17.<br>17.<br>16.<br>15.<br>15.<br>15.                                   |
| Cable R<br>Cable R<br>Cable R<br>Caury (<br>Boring<br>Doring<br>Constance<br>Diameter<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>Constance<br>C  | Conventional     Conventional     Reverse)      sasion     pod     Conventional     Co   | Diamon     Diamon     Disting     Diving     Digging     Orging     Orging     of Material     Arbredass, Plastic, Steel)     E     E     Kind of Water     Other, spe     Kind of Water  | d P<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D   | Ublic<br>kornestic<br>ivestock<br>ingation<br>dustrial<br>ther, specify<br>ising<br>Perem<br>+,45<br>30.00<br>reen<br>Dop<br>From<br>30.00<br>From<br>30.00<br>Untested<br>Untested   | Comm     Municia     Muni  | Abandoned, other, specify Content Cont | 13.63<br>Duration of pumpir<br><u>b</u> hrs + <u>0</u><br>Final water level er<br>If flowing give rate<br>Recommended pu<br><u>13.6</u><br>Recommended pu<br><u>13.6</u><br>Well production (In<br>Disinfected?<br><u>8</u> [Yes] No<br>Please provide a<br><u>1</u>  | min<br>min<br>of pumping @M<br>7<br>(min/GPM)<br>mp rate<br>33<br>min/GPM)<br>Map of M<br>map below follow<br>x3 y 8<br>4<br>2<br>4<br>2<br>4<br>7 m   | 4<br>5<br>0<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>Well Loo       | 17.15<br>17.33<br>17.92<br>18.40<br>18.49<br>18.49<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55   | 4<br>5<br>5<br>10<br>3<br>15<br>20<br>5<br>25<br>30<br>25<br>30<br>40<br>5<br>0<br>40<br>0<br>25<br>30<br>0<br>40<br>0<br>160  | 17. 17.<br>17. 16<br>15.<br>15.<br>15.                                   |
| Cable R<br>Cable R<br>R Rolary (<br>Chury (<br>Chur) (<br>Chur) (<br>Chury (<br>Chur) (<br>Chu   | Conventional<br>Reverse)<br>Ission<br>Converse)<br>Ission<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Converse<br>Conver   | Diamon     Diamon     Disting     Diving     Diving     Digging     OR Material     Arroglass, Plastic, Steel)     E     E     Kind of Water     Other, spe     Kind of Water     Other, spe  | d         P           d         P           D         D           lin         P  | ublic<br>kornestic<br>ivestock<br>ingation<br>dustrial<br>ther, specify<br>ising<br>From<br>+, 4, 45<br>33, 000<br>From<br>a, 2, 41<br>Signature<br>(Untestee<br>Untestee   | Comm     Municia     Muni  | Abandoned, other, specify Cother, Specify Coth | 13.63       Duration of pumpin  | min<br>min<br>of pumping (Min<br>(min/GPM)<br>mp rate<br>3<br>mp rate<br>3<br>min/GPM)<br>map below follow<br>ot y 8<br>c + 7 m.   | 4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60                        | 17.15<br>17.33<br>17.92<br>18.42<br>18.42<br>18.42<br>18.42<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55  | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | 17. 17. 16 15. 15<br>15. 15  |
| Cable R<br>Cable R<br>Cable R<br>Caury (<br>Coury  | dat Depth     //t) _ Gas     dat Depth     //t) _ Gas     dat Depth     //t) _ Gas  | Diamon     Diamon     Disting     Diving     Digging     Orging     Orgi     | d         P           d         P           d         D           d         D           d         D           d         D           d         D           d         D           d         D           d         D           d         D           d         D           d         Mail           middness         O           d         Mail           middness         O           d         Mail           d  | ublic<br>kornestic<br>ivestock<br>ingation<br>dustrial<br>ther, specify<br>sing<br>From<br>+,45<br>33,000<br>recen<br>Dop<br>From<br>32,91  | Comm     Municia     Muni  | Abandoned, other, specify  | 13.63         Duration of pumpin  | min<br>min<br>of pumping (Min<br>(min/GPM)<br>mp rate<br>3<br>min/GPM)<br>map below follow<br>sty 8<br>e<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c<br>c   | 4<br>5<br>0<br>10<br>15<br>20<br>25<br>30<br>40<br>40<br>50<br>60<br>₩eff Loo       | 17.15<br>17.33<br>17.92<br>18.42<br>18.42<br>18.42<br>18.42<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55  | $\begin{array}{c c}       4 \\       5 \\       1 \\       10 \\       3 \\       15 \\       20 \\       25 \\       30 \\       25 \\       30 \\       50 \\       40 \\       50 \\       60 \\       \hline       60 \\       \hline       Bo \\       Bo \\      Bo \\      Bo \\      Bo \\     $ | 17. 17. 16 15. 15<br>15. 15  |
| Cable R<br>Cable R<br>R Rolary (<br>Charles Air perc<br>Charles Air perc<br>Charles Air perc<br>Charles Air perc<br>Charles Air Perc<br>Charles Air Charles<br>Diameter<br>Charles<br>Air perc<br>Charles Air Charles<br>Air Charles<br>Charles<br>Air Charles<br>Charles<br>Air Charles<br>Charles<br>Air Charles<br>Charles<br>Air Charles<br>Charles<br>Charles<br>Air Charles<br>Charles<br>Charles<br>Air Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles<br>Charles   | A conventional<br>Reverse)<br>ussion<br>pooly<br>Conventional<br>Reverse)<br>ussion<br>Open Hol<br>(Galvania<br>Concrete,<br>Steel<br>Steel<br>(Plastic, Gal<br>Me<br>(Plastic, Gal<br>Stat<br>(Plastic, Gal<br>(Plastic, Ga  | Mater Del     Kind of Water     Other, spe     Kind of Water     Other     Other     So     Other     Other     Other     So     Other     Other     So       | d         P           d         P           d         D           d         D           d         D           d         D           d         D           d         D           d         D           d         D           d         D           d         D           d         D           d         Mail           midness         Gin           d         477           d         477           d         477           d         477           d         477           d         Gon           d         Con           d         Con           d         Con           d         Con           d         Fresh           cdfy  | Ublic<br>Kornestic<br>ivestock<br>ingation<br>dustrial<br>ither, specify<br>ising<br>Perom<br>4,45<br>3,200<br>From<br>3,291<br>Untested<br>Untested<br>Untested<br>Technicia   | Comm     Municia     Muni  | Abandoned, Other, Specify  Status of Well  Status of Well Status of Well Status of Well Status of Well Status  | 13.63         Duration of pumpin  | min<br>min<br>nd of pumping (Min<br>7<br>(min/GPM)<br>mp rate<br>3<br>min/GPM)<br>map below follow<br>x3<br>e<br>e<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-  | 4<br>5<br>0<br>10<br>15<br>25<br>30<br>40<br>50<br>60<br>9<br>₩ell Loo              | 17.15<br>17.33<br>17.92<br>18.06<br>18.40<br>18.40<br>18.50<br>18.50<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55<br>18.55   | 4<br>5<br>5<br>10<br>3<br>15<br>20<br>5<br>20<br>5<br>20<br>5<br>30<br>5<br>40<br>5<br>60<br>8<br>60   | 17: 17<br>16 15: 15<br>15  |
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 | Alter Contractor's Licence No.   | 13.63       Duration of pumping   | min<br>min<br>di of pumping ()<br>r<br>(thinkGPM)<br>mp depth (f)<br>mp rate<br>3<br>minGPM)<br>map below follow<br>wify 89<br>e<br>- 7<br>- 7<br>- 7<br>- 7<br>- 7<br>- 7<br>- 7<br>- 7   | 4<br>5<br>0<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>Well Loo       | 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 | Comm     Munici     So, 91     To     So, 91     So,   | Abandoned, other, specify Contractor's Licence No.   | 13.63         Duration of pumping   | min<br>di of pumping ⊕n<br>-7<br>(Imir/GPM)<br>mp depth (€nt)<br>[8<br>mp rate<br>-3<br>-3<br>-3<br>-3<br>-3<br>-3<br>-3<br>-3<br>-3<br>-3   | 4<br>5<br>0<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>9<br>Vell Loo  | 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| Cable R<br>Cable  | decompositional     decompositional     Reverse)     assion     pool     Con     Open Hole     (Calvaniz     Con     Open Hole     (Calvaniz     Con     Con     Open Hole     (Calvaniz     Con     Con     (Plastic, Gal      s     tat Depth     //th)     Gass     f at Depth     //th     Gas     f     f at Depth     //th     Gas     f  | Material Steel     Material     |  | ublic<br>tomestic<br>thestock<br>trigation<br>dustrial<br>ther, specify<br>isting<br>Dep<br>From<br>+.45<br>30.00<br>reen<br>Dop<br>From<br>32.91<br>Untested<br>Untested<br>Untested<br>Untested<br>I Technicia<br>s E-mail Ad<br>Technician (<br>Un Lit   | Comm     Munici  | Abandoned, other, specify Bother Coulity Bother Could be abandoned, other, specify Bother Specif | 13.63         Duration of pumping   | min<br>nd of pumping ⊕n<br>7<br>(Imir/GPM)<br>mp depth (€n)<br>[8<br>mp rate<br>3<br>mr/GPM)<br>Map of M<br>map below follow<br>at Package Delivin<br>(C   2     2   2   2   2   2   2   2   2   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| From  | To   | and six of a   | (Material an   | nd Type)   | Mark   | (f)(R)<br>10  | Clear and sand   | free  | Time<br>(min)   | Water Love   | el Time<br>(min)  | Wa  |
| 0   | 6.09   |  | Bento  | onite  |  | .17   | If pumping discontinu  | ied, give reason  | Level   | 12.6   |   |   |
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| Meth<br>Cable Too<br>Rotary (C<br>Rotary (R   | nod of Const<br>ol<br>conventional)<br>teverse)  | Diamond  |  | ublic<br>omestic<br>vestock  | Well Us Comme Municip  | se<br>rcial   Not used<br>al   Dewatering<br>le   Monitoring  | 42.6<br>Pumping rate (mg)<br>22.73<br>Duration of pumping<br>6 hrs + 0   | GPM)  | 3 4 5   | 14.94<br>14.44<br>14.78<br>15.05   | 3 4 5   | 1   |
| Meth Cable Too Rectary (C Rotary (R Boring Air percus   | nod of Const<br>ol<br>conventional)<br>leverse)<br>ssion   | Diamond<br>Diamond<br>Jetting<br>Driving<br>Digging  |  | ublic<br>omestic<br>vestock<br>igation<br>dustrial   | Well Us Comme Municip Ø Test Hoi Cooling   | rcial Not used<br>al Dewatering<br>le Monitoring<br>& Air Conditioning  | Pumping rate (mit)<br>Pumping rate (mit)<br>Duration of pumping<br><u>6</u> hrs + <u>0</u><br>Final water level end  | GPM)<br>min<br>of pumping (201  | 3<br>4<br>5<br>10   | 14.02<br>14.44<br>14.78<br>15.05<br>15.09  | 3<br>4<br>5<br>10   |   |
| Meth<br>Cable Too<br>Rotary (C<br>Rotary (R<br>Boring<br>Air percus<br>Other, spo   | od of Const<br>ol<br>conventional)<br>teverse)<br>ssion<br>ecity   | Diamond<br>Jetting<br>Driving<br>Digging   | Pu<br>  Do<br>  Liv<br>  Im<br>  Im<br>  Im  | iblic<br>omestic<br>vestock<br>igation<br>dustrial<br>her, specify   | Well Us Comme Municip Ø Test Ho Cooling  | se<br>rcial   Not used<br>al   Dewatering<br>le   Monitoring<br>& Air Conditioning  | Pumping rate (mg)<br>20.73<br>Duration of pumping<br>6 hrs + 0<br>Final water level and<br>16.10<br>If flowing give rate (M  | GPM)<br>min<br>of pumping (107<br>nin/GPM)  | 3<br>4<br>5<br>10<br>15   | 14,00<br>14,44<br>14,78<br>15.05<br>15.09<br>15.83   | 3<br>4<br>5<br>10<br>15   |   |
| Meth<br>Cable Too<br>& Rotary (C<br>Boring<br>Air percus<br>Other, spe<br>Inside  | and of Const<br>of<br>conventional)<br>teverse)<br>estion<br>ectiv<br>Const<br>Open Hole Ol  | Diamond<br>Jetting<br>Driving<br>Digging   | Pu<br>Do<br>Liv<br>Int<br>Co<br>ecord - Cas<br>Wall  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>her, specify<br>sing<br>Dept   | Well Us Comme Municip Statest Ho Cooling Cooling   | se rcial   Not used al   Dewatering le   Monitoring & Air Conditioning  Status of Well Water Supply   | 42.6<br>Pumping rate (mg)/<br>20.73<br>Duration of pumping<br>6_hrs+0<br>Final water level and<br>16.18<br>If flowing give rate (in<br>Recommended pum   | min<br>of pumping (107<br>nin/GPM)<br>o depth (10711)   | 2<br>3<br>4<br>5<br>10<br>15<br>20  | 14.94<br>14.44<br>14.78<br>15.05<br>15.09<br>15.83<br>16.18  | 3<br>4<br>5<br>10<br>15<br>20   |   |
| Meth<br>Cable Too<br>K Rotary (C<br>Rotary (R<br>Boring<br>Air percus<br>Other, spectra<br>Inside<br>Diameter<br>Other, spectra<br>Diameter   | Ind of Const<br>of Conventional)<br>teverse)<br>ssion<br>ecity<br>Const<br>Open Hole OI<br>(Galvanizod, F<br>Concrete, Plan  | truction<br>Diamond<br>Jetting<br>Driving<br>Digging<br>truction Ro<br>R Material<br>Fibreglass,<br>stic, Steel)   | Pu<br>Do<br>Liv<br>Inic<br>ecord - Cas<br>Wal<br>Thickness   | iblic<br>mestic<br>restock<br>igation<br>dustrial<br>ther, specify<br>sing<br>Dept<br>From   | Well Us Comme Municip () Test Ho Cooling () () () () () () () () () () () () ()  | se rcial   Not used al   Dewatering be   Monitoring & Air Conditioning  Status of Well  Water Supply Replacement Well Ø Test Hole   | H2.6<br>Pumping rate (mgW<br>3.9.73<br>Duration of pumping<br>6. hrs + 0<br>16.10<br>If flowing give rate (in<br>Recommended pum<br>20   | min<br>of pumping (10)<br>nin/GPM)<br>p depth (10)Til   | 3<br>4<br>5<br>10<br>15<br>20<br>25   | 14.02<br>14.44<br>14.78<br>15.05<br>15.09<br>15.83<br>16.18<br>16.18   | 3<br>4<br>5<br>10<br>15<br>20<br>25   |   |
| Meth<br>Cable Tox<br>Rotary (C<br>Rotary (R<br>Air percus<br>Other, spo<br>Inside<br>Diameter<br>Colin<br>J5-24   | od of Const<br>ol<br>conventional)<br>teverse)<br>ssion<br>ecity<br>Const<br>Open Hole Ol<br>(Galvarized, F<br>Concrete, Pia<br>Steel  | truction<br>Diamond<br>Jetting<br>Driving<br>Digging<br>truction Ri<br>R Material<br>Breglass,<br>stic, Stoel)   | econd - Cas<br>Wall<br>Thiomess  | blic<br>xmestic<br>vestock<br>gation<br>dustrial<br>her, specify<br>sing<br>Prom<br>+, SO  | Well Us Comme Comme Municip Test Ho Cooling To To To   | Se  rcial   Not used al Dewatering le Monitoring 8. Air Conditioning  Status of Well Water Supply Replacement Well Ø. Recharge Well Dewatere Well   | H216<br>Pumping rate (mgW<br>23.73<br>Duration of pumping<br><u>6</u> hrs + 0<br>Final water level and<br>16.18<br>If flowing give rate (in<br>Recommended pump<br>Recommended pump<br>Recommended pump  | min<br>of pumping (201<br>nin/GPM)<br>p depth (2011)<br>p rate  | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30   | 14,00<br>14,14<br>14,18<br>15.05<br>15.09<br>15.83<br>16,18<br>16,18   | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30   |   |
| Cable Toc<br>Cable Toc<br>Rotary (C<br>Boring<br>Boring<br>Cate percent<br>Cate percent<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer<br>Cometer    | od of Const<br>of<br>conventional)<br>teverse)<br>ssion<br>ecity<br>Open Hole OI<br>(Galvanized, F<br>Concrete, Plas<br>5 teel<br>5 teel   | Truction   |  | bbic<br>mestic<br>restock<br>igation<br>her, specify<br>Sing<br>Popt<br>From<br>+, SO<br>70:71   | Weill Us           Comme           Municip           ØT Test Ho           Cooling           n (57t)           To           71.60           71.60   | Se  rcial   Not used al   Dewatering le   Monitoring & Air Conditioning  Status of Well  Replacement Well  Recharge Well  Dewatering Well  Cbservation and/or   | 42.6<br>Pumping rate (mig)/<br>20.73<br>Duration of pumping<br>6.18<br>Final water level and<br>16.10<br>If flowing give rate (in<br>Recommended pum<br>20<br>Recommended pum<br>20<br>Recommended pum<br>Well production (thin)   | min<br>of pumping (2017)<br>nin/GPM)<br>o depth (2017)<br>o rate<br>222,73<br>/GPM)   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40  | 14,02<br>14,14<br>14,78<br>15.05<br>15.09<br>15.83<br>16.18<br>16.18<br>16.18  | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40   |   |
| Cable To:<br>Cable To:<br>Cable To:<br>Rotary (C<br>Boring<br>Data peras<br>Other, sys-<br>Traide<br>Disneter<br>Other, sys-<br>To:<br>Data cable<br>Disneter<br>Other, sys-<br>To:<br>Data cable To:<br>Data to:<br>Dat  | and of Const<br>of<br>conventional)<br>teverse)<br>ssion<br>ecity<br>Const<br>Open Hole OI<br>(Galvanizod, F<br>Concrete, Pia<br>Steel<br>Steel  | ruction<br>Diamond<br>Jeting<br>Driving<br>Digging<br>ruction R<br>R Material<br>Foreglass,<br>stic, Stoel)<br>L<br>L<br>4 P4cker  | ecord - Car<br>Wall<br>Wall<br>Wall<br>Wall<br>Wall<br>Wall<br>Wall<br>Wa  | blic<br>xmestic<br>restock<br>igation<br>Austrial<br>her, specify<br>Sing<br>Dept<br>From<br>+.50<br>70-71   | Well Us           Comme           Municip           ØT Test Ho           Cooling           Dr. GOTI)           To           71.62  | se rdial   Not used al   Dewatering be   Monitoring 8 Air Conditioning   Status of Well   Status of Status   Status of Well   Status of Status   Status of Status   Status of Status  | 42.6<br>Pumping rate (min)/<br>23.73<br>Duration of pumping<br>6. hrs + 0<br>Final water level and<br>16.18<br>If flowing give rate (in<br>Recommended pum<br>20<br>Recommended pum<br>20<br>20<br>Recommended pum<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20   | min<br>of pumping 100<br>nin/GPM)<br>o depth (10011)<br>o rate<br>22.73<br>//GPM)   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50  | 14,02<br>14,14<br>14,78<br>15.05<br>15.07<br>15.83<br>16.18<br>16.18<br>16.18<br>16.18   | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50   |   |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Air percus<br>Other, sys-<br>Control, sys-<br>Methe<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Diamate<br>Di<br>Diamate<br>Diamate<br>Diamate<br>Diamate | and of Const<br>of conventional)<br>teverse)<br>ssion<br>colly<br>Const<br>Open Hole Of<br>(Galvanizod, Pic<br>Concrete, Pic<br>Steel<br>Steel   | ruction<br>Diamond<br>Jetting<br>Driving<br>Digging<br>ruction R<br>R Material<br>Bronglass,<br>stic, Stoel)<br>J<br>J<br>Packer   |  | blic<br>smestic<br>restock<br>gation<br>dustrial<br>her, specify<br>From<br>+. 50<br>70.71   | Well Us           Comme           Municip           Ø Test Ho           Cooling           To           71.62   | se rcial   Not used al   Dewatering be   Monitoring be   Monitoring be   Monitoring be   Monitoring be   Monitoring be   Mater Supply constraint and/or Monitoring Hole conservation and/or Monitoring Hole conservation and/or Monitoring Hole heredsage Well conservation and/or Monitoring Hole heredsage Well conservation and/or Monitoring Hole heredsage Well heredsage  | 42.6<br>Pumping rate (min)/<br>20.73<br>Duration of pumping<br>6_hrs+0<br>Final water level and<br>16.18<br>If flowing give rate (in<br>Recommended pum<br>20<br>Recommended pum<br>(min) GPM<br>Well production (imin<br>Disinfected?<br>§ Yes □ No   | GPM)<br>min<br>of pumping (D)<br>nin/GPM)<br>p depth (D)(1)<br>p rate<br>22,73<br>/GPM)   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60  | 14,02<br>14,14<br>14,78<br>15.05<br>15.09<br>15.83<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18                                     | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60   | 11<br>13<br>14<br>14<br>14  |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Air percas<br>Other, sys-<br>Dime, sys-   | and of Const<br>al<br>conventional)<br>teverse)<br>ssion<br>const<br>Open Hole OI<br>(Gelvanized, Fiz<br>Concrete, Piz<br>Steel  | truction Diamond Diamond Diating Doinging Doigging Fruction R Material Fibroglass L L L L L L L L L L L L L L L L L L  | Pu<br>Do<br>Do<br>Dr<br>Mail<br>Becord - Cas<br>Wall<br>Thidraess<br>S(R)<br>3 4717<br>3 4717<br>3 4717  | blic<br>mestic<br>restock<br>gation<br>Austrial<br>her, specify<br>From<br>+. 50<br>70.71  | Well Us Comme Comme Municip GT test ho Cooling To To Ti.62 Ti.62   | se  rcial   Not used al   Dewatering b Air Conditioning  Status of Well  Replacement Well  Replacement Well  Dewatering Well  Dewatering Well  Dewatering Well  Aiteration  (Construction)  Abandoned, Poor  Weter Outliker   | 42:6       Pumping rate (m)//       20.73       Duration of pumping       6.ns + 0       Final water level and       16.18       If flowing give rate (in       Recommended pum       20       Recommended pum       00       Recommended pum       00       Beinflocted?       Ø.Yes       No   | min<br>of pumping (D)<br>nin/GPM)<br>o depth (D)(1)<br>o rate<br>22,73<br>/GPM)   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>Well Lice   | 14,02<br>14,14<br>14,78<br>15,05<br>15,07<br>15,83<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18                            | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60   |   |
| Meth<br>Cable Toc<br>& Rotary (C<br>Boring<br>Ar percas<br>Other, spo<br>Dismeter<br>Dismeter<br>Const<br>15.24<br>/0.(6  | ood of Const<br>arriventional)<br>teverse)<br>ssion<br>colfy<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Cons  | truction   | Pu<br>Decord - Cas<br>Wall<br>Thickness<br>(Sm)<br>- 477<br>- 477<br>- 477   | blic<br>mestic<br>gation<br>dustrial<br>her, specify<br>From<br>t.50<br>70-71  | Well Us           □ Comme           Municip           Ø Test Ho           □ Cooling           To           71.60           1.60           1.60           1.60           1.60           1.60           1.60   | se  rcial   Not used  al   Dewatering  ke   Monitoring  8 Air Conditioning  Status of Well  Water Supply Replacement Well  Coservation and/or Monitoring Hole Alteration (Construction) Abandoned, Insufficient Supply Abandoned, other, specify other,   | 42:6         Pumping rate (mig)/         Jouration of pumping  | min<br>of pumping (2014)<br>niv(GPM)<br>o depth (2011)<br>o rate<br>222,73<br>(GPM)<br>Map of It<br>ap below follow<br>Alu  | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>Well Loc  | 14,02<br>14,44<br>14,78<br>15,85<br>15,87<br>15,83<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18                            | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60   |   |
| Meth<br>Cable Toc<br>Rotary (R<br>Boring<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darneter<br>Darnete   | and of Const<br>of<br>conventional)<br>teverse)<br>ssion<br>ecity<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Con | truction Diamond Diamond Diamond Diamond Diamond Diamond Diagong Digging truction R R Material Bregiss, steel truction R the packet truction R tal tad, Steel Digging  | Pu<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do   | Ablic<br>mrestic<br>vestock<br>gation<br>dustrial<br>her, specify<br>sing<br>Dept<br>From<br>+.50<br>70.71<br>reen<br>Dept<br>From<br>70.71  | Well Us<br>□ Comme<br>□ Municip<br>Ø Test Ho<br>□ Cooling<br>1 To<br>71.62<br>71.62<br>1 1.62<br>1 1.62  | se  rcial   Not used al Dewatering le Monitoring 8 Air Conditioning  Status of Well  Water Supply  Replacement Well  Conservation and/or Monitoring Hole  Dewatering Well  Dewatering Well  Dewatering Well  Dewatering Well  Atteration (Construction)  Abandoned, Poor Nater Quality  Abandoned, other, specify   | 42.6         Pumping rate (mig)/         3.7.3         Duration of pumping         6         hrs + 0         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Please provide a m         21         Please provide a m   | min<br>of pumping (D)<br>nin/GPM)<br>o depth (D)(1)<br>o rate<br>   | 4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80  | 14,02<br>14,44<br>14,78<br>15.05<br>15.05<br>15.05<br>15.05<br>15.05<br>15.05<br>15.05<br>16.18<br>16.18<br>16.18<br>16.18<br>16.10<br>16.10 | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>60   |   |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Air percas<br>Other, sys-<br>Teckle<br>Diameter<br>Diameter<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contrision<br>Contri<br>Contrision<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contribution<br>Contri<br>Contribution<br>Contribution<br>Contri<br>Contri   | and of Const<br>or an entional)<br>teverse)<br>ssion<br>celly<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const   | Truction Diamond Diamond Diamond Diamond Diamond Diagong Digging Truction R Material Sic, Stool)   | Pu<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do   | blic<br>mestic<br>kestock<br>igation<br>dustrial<br>strig<br>From<br>+.50<br>70-71<br>70-71<br>Peen<br>From<br>11_160  | Well Us           □ Comme           □ Municip           ØT Test Ho           □ Cooling           To           71.62           71.62           1.62           72.84   | se rcial   Not used al   Dewatering is   Monitoring is Air Conditioning   Status of Well   Replacement Well   Replacement Well   Replacement Well   Dewatering Well   Dewatering Well   Dewatering Well   Dewatering Well   Dewatering Well   Dahandoned, from   Abandoned, Poor   Water Quality   Abandoned, other, specify   Dother, specify   Dother, specify   Dother, specify   Dother, specify   Dother, specify   Not used   | 42.6         Pumping rate (min)/         20.73         Duration of pumping         6_hrs+0         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Recommended pumping         Well production (imming Desinflocted?)         18.19         Please provide a minimized pumping   | min<br>of pumping (D)<br>nin/GPM)<br>p depth (D)(1)<br>p rate<br>22.73<br>/GPM)<br>22.73<br>/GPM)   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>Well Loo<br>vy S <sup>∞</sup>   | 14,02<br>14,14<br>14,78<br>15.05<br>15.07<br>15.83<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18                                     | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60   |   |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Air percas<br>D'Other, syn<br>Jone, syn<br>JS-24<br>(0.(b<br>Demoter<br>Demoter<br>Demoter<br>Demoter<br>Demoter<br>Demoter<br>Demoter<br>Demoter<br>Demoter  | and of Const<br>a conventional)<br>teverse)<br>ssion<br>const<br>Open Hole OI<br>(Galvarized, Fi<br>Constel, Plan<br>Steel<br>Const<br>Mater<br>(Plastic, Galvari<br>Steelon   | truction Diamond Diamond Diamond Diamond Diamond Diamond Diamond Diamond Realing Diamond Realing Reali | Pu<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do   | blic<br>mestic<br>gation<br>Austrial<br>her, specify<br>From<br>+. 50<br>70:71<br>From<br>Peen<br>Dept<br>From<br>71,162   | Well Us<br>Comme<br>Municip<br>GT test ho<br>Cooling<br>To<br>To<br>T1.62<br>T1.62<br>T1.62<br>T1.62<br>T2.84  | se rcial   Not used al   Dewatering be   Monitoring be   Monitoring be A Ar Conditioning be A Ar Conditioning be   Noter Supply conditioning be   Needacement Well be   Recharge Well conservation and/or Monitoring Hole conservation and/or Monitori  | 42:6         Pumping rate (m)//         20.73         Duration of pumping         6.ns+0         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Recommended pumping         Well production (imming GPM)         Disinflocted?         XI.Yes         No  | rin<br>of pumping (D)<br>nin/GPM)<br>o depth (D)(1)<br>p rate<br>222,73<br>/GPM)<br>Map of (<br>ap below follow<br>Au<br>Fred   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>00<br>Well Loo  | 14,02<br>14,14<br>14,78<br>15.05<br>15.07<br>15.83<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18                            | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | 1<br>1<br>1<br>1<br>1<br>1<br>1<br>1  |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Ar perca<br>D'theke<br>Diameter<br>Otheside<br>Diameter<br>(0.16<br>Outside<br>Diameter<br>(5)in)<br>15.24<br>Valuer found<br>10.16<br>Water found<br>10.22<br>Water found  | od of Const<br>arriventional)<br>teverse)<br>ssion<br>colfy<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const  | truction Diamond Disting Dirving Driving Driving Digging Truction R Material Freglass, stic, Stool)  |  | blic<br>mestic<br>gation<br>Austrial<br>her, specify<br>From<br>t. 50<br>70-71<br>From<br>71_60-2<br>RUntested   | Well Us<br>Comme<br>Municip<br>(97 Test Ho<br>Cooling<br>71.62<br>71.62<br>71.62<br>71.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.6     | se<br>rcial   Not used<br>al   Dewatering<br>be   Monitoring<br>8 Air Conditioning<br>• Status of Well<br>Water Supply<br>Replacement Well<br>Ø Test Hole<br>Recharge Well<br>Dewatering Well<br>Dewatering Well<br>Dewatering Well<br>Deservation and/or<br>Monitoring Hole<br>Abandoned, Poor<br>Water Cuality<br>Abandoned, other,<br>specify<br>Hole Diameter:<br>th Ø/fi) Diametor<br>To @Ø  | 42:6         Pumping rate (mig)/         30.73         Duration of pumping         6.ns+0         Final water level end         16.18         If flowing give rate (in         20         Recommended pumping         20         Recommended pumping         20         Recommended pumping         Well production (minim         Disinflocted?         XI.Yes       No         Please provide a m  | GPM)<br>min<br>of pumping (D)<br>niv(GPM)<br>o depth (D)(1)<br>o rate<br><u>222,73</u><br>(GPM)<br><u>Map of (</u><br>ap below follow<br><u>4</u><br>Fiell  | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>Well L'oc<br>ving Inst  | 14,02<br>14,14<br>14,78<br>15.05<br>15.07<br>15.83<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18                                     | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>7<br>7<br>8<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1   | //////////////////////////////////////  |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Ar perca<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diamete   | Interest Constant Con   | truction  Jeting Jeting Driving Driving Driving Driving Driving truction R Material Regass, stic, Stool)   | ecord - Sci<br>Sol No.<br>8<br>ails<br>9<br>Fresh  | blic<br>mrestic<br>gation<br>dustrial<br>her, specify<br>From<br>1.50<br>70-71<br>Poept<br>From<br>11_60<br>Untested   | Well Us<br>Comme<br>Municip<br>Coding<br>To<br>Coding<br>To<br>71.62<br>71.62<br>71.62<br>71.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1.62<br>1 | se<br>rcial   Not used<br>al Dewatering<br>le Monitoring<br>& Air Conditioning<br>  Status of Well<br>  Water Supply<br>  Replacement Well<br>  Dewatering Well<br>  Diservation and/or<br>Monitoring Hole<br>  Abandoned, Poor<br>  Dobardoned, Poor<br>  Diameter<br>  To<br>  Diameter<br>  D | 42.6         Pumping rate (mig)/         3.7.3         Duration of pumping         6. hrs + 0         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Recommended pumping         Well production (imming GPM)         Well production (imming Press)         Vell production (imming Press)         No         Please provide a minimic degraphic degraph | min<br>of pumping (D)<br>invGPM)<br>o depth (D)(1)<br>o rate<br>22.73<br>VGPM)<br>Map of V<br>ap below follow<br>Au   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>Well Loo<br>vy SC   | 14,02<br>14,44<br>14,78<br>15.05<br>15.09<br>15.83<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18                                     | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>7<br>7<br>7<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1   | / / / / / / / / / / / / / / / / / / /   |
| Meth<br>Cable Toc<br>Rotary (R<br>Boring<br>Air percas<br>Damater<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Mater found<br>2.23<br>Water found<br>Water found<br>Water found<br>Water found  | and of Const<br>arrentional)<br>teverse)<br>ssion<br>ceity<br>Const<br>Const<br>Open Hole OI<br>(Galwarizod, Fiz<br>Conste, Piz<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Ste   | Truction Diamond Diamond Diamond Diamond Diamond Diamond Diamond Diamond Remaination Rema  | Pu<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do   | blic<br>mestic<br>gation<br>austrial<br>her, specify<br>From<br>+.50<br>70-71<br>reen<br>Dept<br>From<br>70-71<br>Refut<br>From<br>11_60<br>Refut<br>Statester<br>Untester   | Well Us           □ Comme           □ Municip           ØT Test Ho           □ Cooling           0           71.62           71.62           71.62           71.62           72.84           □ Dep           From           0           6.04   | se<br>rcial   Not used<br>al Dewatering<br>le Monitoring<br>& Air Conditioning<br>Status of Well<br>Water Supply<br>Replacement Well<br>Dewatering Well<br>Dotservation and/or<br>Monitoring Hole<br>Abandoned, Poor<br>Abandoned, Poor<br>Dotser, specify<br>Hole Diameter:<br>th @Mi)<br>Construction<br>Diameter<br>To @Dim<br>G.SC4<br>ZD, 84 / 14.68   | 42.6         Pumping rate (min)/         3.73         Duration of pumping         6.18         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Recommended pumping         21         22         23         Please provide a me         24         24         25         26         27         28         29         20         20  | GPM)<br>min<br>of pumping (D)<br>invGPM)<br>p depth (D)(1)<br>p rate<br>22.73<br>VGPM)<br>Map of M<br>ap below follow<br>Alu<br>Fiel  | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60<br>0<br>25<br>30<br>40<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>60<br>6  | 14,02<br>14,44<br>14,78<br>15.05<br>15.05<br>15.83<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18                                     | 3<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>20<br>25<br>30<br>40<br>50<br>60<br>60  | 14<br>13<br>14<br>14<br>14<br>14<br>14<br>14<br>14<br>14<br>14<br>14<br>14<br>14<br>14      |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Air parcas<br>Other, sparcas<br>Dother, sp  | and of Const<br>a conventional)<br>teverse)<br>ssion<br>coily<br>Const<br>Open Hole Of<br>(Gulvanicod, Fi<br>Concere, Pia<br>Steel<br>Steel<br>Const<br>Mater<br>(Plassic, Galvan<br>Mater<br>(Plassic, Galvan<br>I at Depth Kin<br>ft)Gas   | Truction Diamond Diamond Diamond Diamond Diamond Diamond Truction R R Material Forglass, Steel Forglass, Steel Conter, spe d of Water Other, spe d of Water; Other, spe  | Pu<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do<br>Do   | blic<br>mestic<br>gation<br>dustrial<br>her, specify<br>From<br>+.50<br>70-71<br>To-71<br>Peen<br>Dept<br>From<br>11.60<br>Untestec<br>Untestec  | Well Us           □ Comme           □ Municip           ØT Test Ho           □ Cooling           To           71.62           71.62           71.62           71.62           72.84           □ Dep<br>From           0           G.001  | se<br>rotal   Not used<br>al   Dewatering<br>& Air Conditioning<br>& Air Conditioning<br>& Air Conditioning<br>  Status of Well<br>  Replacement Well<br>  Replacement Well<br>  Replacement Well<br>  Dewatering Well<br>  Dewatering Well<br>  Dewatering Well<br>  Dewatering Well<br>  Dewatering Well<br>  Deberation and/or<br>Monitoring Hole<br>  Abandoned, Poor<br>  Water Quality<br>  Danotoned, Poor<br>  Water Quality<br>  Danotoned, Poor<br>  Water Quality<br>  Danotoned, Poor<br>  Water Quality<br>  Danotoned, Poor<br>  Water Quality<br>  Dother, specify<br>  Other, specify<br>  Other, specify<br>  Other, specify<br>  Status of Yell<br>  Dimenter<br>  Status of Yell<br>   | 42.6         Pumping rate (m)//         20.73         Duration of pumping         6_hrs+0         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Recommended pumping         Weil production (imm)         Disinflucted?         XI.Yes         No         Please provide a m         1         20          1          20   | GPM)<br>min<br>of pumping (D)<br>niv(GPM)<br>p depth (D)(1)<br>p rate<br>22.73<br>VGPM)<br>Map of M<br>ap below follow<br>Au<br>Fiel<br>Sm→   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>25<br>50<br>60<br>60<br>60<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80  | 14,02<br>14,14<br>14,78<br>15.05<br>15.07<br>15.83<br>16.18<br>16.18<br>16.18<br>16.10<br>16.10  | 3<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60  |   |
| Meth<br>□ Cable Toc<br>♥ Rotary (C<br>□ Rotary (C<br>□ Rotary (C<br>□ Cable Toc<br>♥ Rotary (C<br>□ Cable Toc<br>♥ Rotary (C<br>□ Cable Toc<br>♥ To   |  | Truction Diamond Diamond Diamond Diamond Diamond Diamond Diamond Truction R Material Foreglass Stack, Steel)   |  | blic<br>mestic<br>gation<br>Austrial<br>her, specify   | Well Us<br>Comme<br>Municip<br>GT test ho<br>Cooling<br>To<br>To<br>T1.62<br>T1.62<br>T1.62<br>T1.62<br>T1.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.62<br>T0.6   | se<br>rcial   Not used<br>al Dewatering<br>& Alr Conditioning<br>& Alr Conditioning<br>Status of Well<br>  Water Supply<br>  Replacement Well<br>  Water Supply<br>  Replacement Well<br>  Dewatering Well<br>  Dematchering<br>  Dematchering<br>  Difference in the interval<br>  Difference in the inte  | 42:6         Pumping rate (m)         20.73         Duration of pumping         6.18         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Recommended pumping         Weil production (imin         Disinfloctad?         XI:Yes         No         Please provide a m         1  | GPM)<br>min<br>of pumping (D)<br>min/GPM)<br>p depth (D)(1)<br>p rate<br>222.73<br>VGPM)<br>Fiel<br>Fiel<br>Sn + (1)<br>25  | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>00<br>Well Loo<br>vy S  | 14,02<br>14,14<br>14,78<br>15.05<br>15.07<br>15.83<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18                                     | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>7<br>7<br>8<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1   |   |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Ar perca<br>D'theke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Otheke<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>D  |  | Truction R Diamond Disting Diamond Disting Dirving Di  |  | blic<br>mestic<br>gation<br>Austrial<br>her, specify<br>From<br>t. 50<br>70-71<br>70-71<br>From<br>71-60<br>RUntestec  | Well Us<br>Comme<br>Municip<br>GT test ho<br>Cooling<br>71.62<br>71.62<br>71.62<br>71.62<br>71.62<br>10<br>70<br>71.62<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10   | se<br>rcial   Not used<br>al   Dewatering<br>b Air Conditioning<br>8 Air Conditioning<br>8 Air Conditioning<br>(Notification<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notification)<br>(Notificatio  | 42:6         Pumping rate (m)         20.73         Duration of pumping         6.18         Final water level and         16.18         If flowing give rate (in         20         Recommended pum         20         Recommended pum         20         Recommended pum         20         Please provide a m         10         10         10         10         10         11         12         13         14         15         16         16         17         18         19         10         10         11         12         13         14         14         14         14         15         16         17         18         19         10         10         11         12         14         16  | GPM)  min of pumping (D)  nin/GPM)  o depth (D)  n  ap below follow  Gray  Free  Son  Son  Son  | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8   | 14,02<br>14,14<br>14,78<br>15.05<br>15.07<br>15.83<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18                                     | 3         4           5         10           15         20           225         30           40         50           50         60   |   |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Ar perca<br>Other, sp<br>Inside<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>Diameter<br>D  |  | Truction  Jetting  Driving Driving Driving Driving Driving Driving Truction R Material Regass, stic, Stool)  | ecord - Car<br>Wall<br>Briddeness<br>Wall<br>Briddeness<br>Sof No.<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>3,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,477<br>4,4774,477<br>4,477<br>4,477<br>4,4774,477<br>4,477<br>4,477<br>4,477<br>4,4774,477<br>4,477<br>4,4774,477<br>4,477<br>4,477<br>4,4774,477<br>4, | blic<br>mestic<br>gation<br>Austrial<br>her, specify<br>From<br>t.SO<br>70:71<br>70:71<br>Peen<br>70:71<br>Nopt<br>From<br>71:60<br>QUntested  | Weil Us           □ Comme           □ Municip           ØT rest Ho           □ Cooling           □ To           71.60           71.60           71.60           71.60           71.60           71.60           71.60           71.60           70.84           □ Dep           From           □ O           0           0           0           0           0           0           0           0           0           0           0           0           0           0           0           0           0   | se<br>rcial   Not used<br>al Dewatering<br>be Monitoring<br>8 Air Conditioning<br>8 Air Conditioning<br>9 Air Conditioning<br>9 Water Supply<br>Replacement Well<br>9 Water Supply<br>9 Replacement Well<br>9 Dewatering Well<br>9 Dewatering<br>9 Dewatering Well<br>9 Diameter<br>9 Diameter<br>9 Diameter<br>9 Diametering Well<br>9 Diametering Well<br>9 Diametering Well<br>9 Diametering Well<br>9 Diametering Well<br>9 Diametering Well<br>9 D  | 42.6         Pumping rate (min)/         Joration of pumping         6.18.10         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Please provide a multiple         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         <   | GPM)<br>min<br>of pumping ton<br>invGPM)<br>o depth (00m)<br>o depth (00m)<br>o rate<br>22.73<br>VGPM)<br>Smathered<br>Field<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Smathered<br>Sma | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>Neil Loo<br>vy 8<br>4   | 14,02<br>14,44<br>14,78<br>15.05<br>15.05<br>15.05<br>15.83<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18                            | 3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>40<br>50<br>60<br>60<br>11<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1   |   |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Conside<br>Darneter<br>Diarneter<br>Diarneter<br>Diarneter<br>Diarneter<br>(C)<br>15-24<br>10-(6<br>Diarneter<br>Conside<br>Diarneter<br>(C)<br>(C)<br>(C)<br>(C)<br>(C)<br>(C)<br>(C)<br>(C)   | I at Depth Kin<br>ft) Gas<br>at Depth Kin<br>ft) Gas<br>at Depth Kin<br>ft) Gas<br>at Depth Kin<br>ft) Gas<br>at Depth Kin<br>ft) Gas<br>ft at Depth Kin<br>ft at   | Truction  Jeting Jeting Driving Driving Driving Driving Driving Truction R Material Freglass, stic, Steel)  Freglass, stic, Steel)  Freglass, stic, Steel  Freglass,   | ecord - Ca<br>Wall<br>Thiohese<br>Soft<br>   | blic<br>mestic<br>gation<br>tastrial<br>her, specify<br>From<br>+.50<br>70-71<br>From<br>11.60<br>RUIntested<br>Untested<br>Untested<br>Untested<br>Technicial<br>Ac   | Well Us           □ Comme           □ Municip           ØT Test Ho           □ Cooling           □ To           71.62           71.62           71.62           71.62           71.62           71.62           1           0           72.84           1           0           6           0           6           0           6           0  | se<br>rotal   Not used<br>al   Dewatering<br>is Air Conditioning<br>& Air Conditioning<br>  Status of Well<br>  Replacement Well<br>  Replacement Well<br>  Replacement Well<br>  Replacement Well<br>  Dewatering Well<br>  Dewa  | 42.6         Pumping rate (min)/         30.73         Duration of pumping         6.18 + 0         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Please provide a multiple         1         20         20         20         20         20         20         20         20         20         20         20         20         <   | GPM)<br>min<br>of pumping ØP<br>nivGPM)<br>p depth ØP(1)<br>p rate<br>22.73<br>VGPM)<br>Son → ↓<br>Son → ↓  | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>60<br>60<br>60<br>60<br>60<br>60<br>8<br>8  | 14,02<br>14,44<br>14,78<br>15.05<br>15.09<br>15.83<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18                                     | 3         4           5         10           15         20           25         30           40         50           60         60           the bac         1           1         1           1         1           1         1  |   |
| Meth<br>Cable Toc<br>Rotary (R<br>Boring<br>Air percas<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter<br>Dameter  | and of Const<br>a conventional)<br>teverse)<br>ssion<br>coily<br>Const<br>Open Hole Of<br>(Gukvancod, Fi<br>Concere, Pia<br>Steel<br>Steel<br>Const<br>Mater<br>(Plassic, Galvan<br>Mater<br>(Plassic, Galvan<br>(Plassic,  | Truction Diamond Diamond Diamond Diamond Diamond Diamond Diamond Diamond Remained Remained Remained Remained Diamond Remained Remained Remained Remained Diamond Remained Rem  | Pu     Do  | blic<br>mestic<br>gation<br>sustrial<br>her, specify<br>From<br>+.50<br>70-71<br>To-71<br>Peen<br>Dept<br>From<br>11.60<br>Untested<br>Untested<br>Untested<br>Technicia<br>AC   | Well Us           □ Comme           □ Municip           ØT Test Ho           □ Cooling           To           71.62           71.62           71.62           71.62           71.62           71.62           71.62           71.62           71.62           71.62           71.62           1           To           From           1           0           6.01           0           6.01           0  | se<br>rotal   Not used<br>al   Dewatering<br>& Air Conditioning<br>& Air Conditioning<br>& Air Conditioning<br>  Status of Well<br>  Replacement Well<br>  Replacement Well<br>  Replacement Well<br>  Dewatering Well<br>  Dotservation and/or<br>Monitoring Hole<br>  Abandoned, Poor<br>  Water Quality<br>  Dother, specify<br>  Dother, specify<br>  Dother, specify<br>  Dother, specify<br>  Dother, specify<br>  Differ Specify<br>  Di  | 42.6         Pumping rate (m)//         20.73         Duration of pumping         6_hrs+0         Final water level and         //6.18         If flowing give rate (in         Recommended pumping         20         Recommended pumping         Well production (imming GPM)         Please provide a minimized pumping         1   | GPM) min of pumping €0 nivGPM) p depth €0n) p rate 22.73 VGPM)  Map of N ap below follow Alu Fiel   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>0<br>25<br>30<br>40<br>0<br>60<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>8   | 14,02<br>14,14<br>14,78<br>15.05<br>15.09<br>15.83<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18<br>16,18                                     | 3           4           5           10           15           20           25           30           40           50           60           60           1           1           1           1           1           1  | 1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Air percar<br>D'Other, spec-<br>D'Other, spec-  | Interest Constant Con   | Truction Diamond Diamond Diamond Diamond Diamond Diamond Diamond Dring Driving Diamond Fruction R Material Fruction R Material Fruction R Material Code d of Water Other, spe d of Water Other, spe d of Water Contractor Interactor I  | Pu     De  | blic<br>mestic<br>gation<br>dustrial<br>her, specify   | Well Us           Comme           Municip           ØT rest ho           Too           71.62           71.62           71.62           71.62           71.62           71.62           71.62           71.62           1           Dep           From           0           6.01           Wa           Wa           Wa           Mathematical Stress           Last Name,   | se<br>rocial   Not used<br>al Dewatering<br>& Air Conditioning<br>& Air Conditioning<br>& Air Conditioning<br>Status of Well<br>  Water Supply<br>  Replacement Well<br>  Water Supply<br>  Replacement Well<br>  Dewatering Hole<br>  Abandoned, Poor<br>Water Quality<br>  Abandoned, Poor<br>  Water Quality<br>  Dother, specify<br>  | 42.6         Pumping rate (m)//         20.73         Duration of pumping         6_hrs+0         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Recommended pumping         21         22         23         24         25         26         27         28         29         29         29         20         20         20         21         22         23         24         2   | GPM)<br>min<br>of pumping @<br>niv(GPM)<br>p depth @nt)<br>p rate<br>22.73<br>VGPM)<br>Fiel<br>Fiel<br>Sn→ ↓<br>35m<br>Package Deliv<br>31.911 @F   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>40<br>50<br>60<br>40<br>50<br>60<br>40<br>50<br>60<br>40<br>50<br>60<br>40<br>50<br>60<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>50<br>60<br>50<br>60<br>50<br>50<br>60<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>5 | 14,02<br>14,14<br>14,78<br>15.05<br>15.07<br>15.83<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18                            | 3           4           5           10           15           20           25           30           40           50           60           60           60           1           1           1           1           1           1           1           1           1           1           1           1           1           1 |   |
| Meth<br>Cable Toc<br>Rotary (C<br>Boring<br>Cable Toc<br>Rotary (C<br>Boring<br>Cable Toc<br>Rotary (C<br>Cable Toc<br>Rotary (C<br>Cable Toc<br>Cable Toc  | Interest Constant<br>a conventional)<br>teverse)<br>ssion<br>Constant<br>Open Hole OL<br>(Galvariado L<br>Constant<br>Open Hole OL<br>(Galvariado L<br>Constant<br>Constant<br>Steel -<br>Steel -<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constant<br>Constan   | Truction R Diamond Disting Diamond Disting Driving Driving Driving Driving Driving Driving Driving Driving Digging Truction R ruction R  | Pu     Do  | blic<br>mestic<br>gation<br>Austrial<br>Austrial<br>Austrial<br>From<br>+. 50<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70:71<br>70 | Weil Us           Comme           Municip           Øf Test Ho           Cooling           To           71.62           71.62           71.62           71.62           71.62           To           71.62           10000           10  | se<br>ricial   Not used<br>al   Dewatering<br>b Air Conditioning<br>Status of Well<br>  Water Supply<br>  Replacement Well<br>  Water Supply<br>  Replacement Well<br>  Dewatering Well  | 42:6         Pumping rate (m)         20:73         Duration of pumping         6. hrs + 0         Final water level and         16.18         If flowing give rate (in         Recommended pumping         20         Recommended pumping         21         22         23         24         24         25         26         27         28         29         29         20         20         21         22         23         24         24  | GPM)  min of pumping (D)  nin/GPM)  o depth (D)()  p rate 22,73 /GPM)  Map of V ap below follow Au  Fiel  Package Deliv  Package Deliv  Package Deliv   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>15<br>50<br>60<br>10<br>15<br>50<br>60<br>10<br>15<br>50<br>60<br>10<br>15<br>10<br>10<br>15<br>10<br>10<br>10<br>15<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10  | 14,02<br>14,14<br>14,78<br>15.05<br>15.07<br>15.83<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18<br>16.18          | 3         4           5         10           15         20           225         30           40         50           50         60   |   |

| Contraction of the second  | r's Inform   | nation   | 12.12.5  | The Party of   | 1. A. A. A. A.   | The second second   | A24779  |  | 8.0792   | Pag   | 10   | or                      |
|--|--|--|--|--|--|---|---|--|--|---|--|-------------------------|
| nst Namo   | Northern   | L  | D-11   | Organization   | Lund   | ula I )   | E-mail Address  | 5  | <u> </u>   |   | U Well   | Constructed             |
| ailing Addres  | s (Street N  | umber/Nam  | 10)  | ( ma   | yus  | Municipality  | Province  | Postal Cod   | ia   | Telephon  | ve No. (inc  | (abco sana "            |
| 6337   | 24   | Huty   | D  | CARNED I   | argermatic 1   | Mono  | CN  | LIGINIS  | 510171   | 12565   | 215 19 17  | Town Particip           |
| idress of We   | I Location (   | (Street Num  | ber/Name)  | - <u>1999</u>  | Clares .   | Township  | a contra consected and  | Lot  | 1000   | Concess   | sion   | 14.16.16.16.202         |
| 772  | 3 Hi<br>Municipalil  | wy 8   | 9  | and the second   |  | Adjala<br>City/Town/Village   |   | 3  | Provir   | nce   | Posta  | al Code                 |
| <  | Simcoe   | 2  |  | man  |  | Allista   | N   |  | Ont  | ario  | LIA  | RIVII                   |
| M Coordina<br>NAD   8  | ates Zone  | Easting  | Izidi  |  | DILLIA   | Municipal Plan and Subl   | ot Number   |  | Other  |   |  |                         |
| verburden  | and Bedro  | ock Materia  | als/Aband  | ionment Se   | aling Reco   | ord (see instructions on t  | ne back of this form)   | The Link   | 0.3  | 11.656  | -  | REAL PROPERTY           |
| eneral Colou   | ur   | Most Comm  | non Materia  | 1  | Ot   | her Materials   | Ge  | eneral Descriptio  | n  |   | From   |                         |
| Brown  |  | Tops   | oil  |  |  |   |   |  | 100  |   | 2  | -5<br>74Z               |
| Grown  | -  | cloy   |  |  | d  | l an al   |   |  |  |   | 2.43   | 498                     |
| Grea   |  | siff   |  | •  |  | t_, gradel  |   |  |  | 1   | 49.98  | 3 56.38                 |
| Brown  |  | clay   | 1  |  |  |   |   |  |  |   | 56.38  | 57.60                   |
| Grey   |  | clay   |  |  | sil-   | - grave   |   |  |  |   | 57.60  | 79.55                   |
| Brown  |  | sand   | 4  |  |  | U   |   |  |  |   | 79.5   | 90.22                   |
| 1113   | -  |  | 1  |  |  |   |   | the second   | No.  |   |  |                         |
| 1220   | Carlina and  | 1351.54  | Annula   | r Space  | 2424244  | TURINGTON   | al a caratal  | Results of V   | Nell Yie   | ld Testin   | 9  | 8.8.5 See               |
| Depth Set at   |  |  | Type of Se<br>(Material a  | ealant Used<br>and Type)   |  | Volume Placed   | After test of well yiel   | kd, water was:<br>d free   | Dr   | Water Lo  | n F<br>svel Time   | Recovery<br>Water Level |
| 0 6  | 6.4  | F  | Benton   | ite  |  | ,22   | Other, specify  |  | (min)<br>Static  | 010   | (min)  | (T)                     |
| -  | -  |  |  |  | L  |   | It pumping discontin  | rued, give reason  | Level  | 010   | 4  | 21 21                   |
|  |  |  |  |  |  |   |   | and the second   | 1  | 212   | 71.  | 01.04                   |
|  |  | in mineral and   |  |  |  | and the second se   | I Pump intake set at t  | mat)   | 1 2  |   | 1 2  |                         |
|  |  |  |  |  | March Cri  |   | Pump intake set at 30.4   | (1911)<br>(1911)<br>(1911)   | 2  |   | 2  |                         |
| Method   | i of Const   | truction   |  | e The drog to  | Well Us  | <b>50</b>   | Pump intake set at<br>30.4<br>Pumping rate/min  | (С)(1)<br>(С)<br>(С)(С)<br>(С)<br>(С)<br>(С)<br>(С)<br>(С)<br>(С)<br>(С)   | 2  |   | 2 3 4  |                         |
| Method<br>Cable Tool<br>Rotary (Conv   | l of Const<br>ventional)   | truction   |  | ublic<br>omestic   | Well Us  | so<br>rcial   Not used<br>al   Dewatering   | Pump intake set at<br>30.4<br>Pumping rate (min)<br>22.72<br>Duration of pumping  | (GPM)<br>(GPM)<br>3<br>min   | 2 3 4 5  |   | 2<br>3<br>4<br>5   |                         |
| Method<br>Cable Tool<br>Rotary (Com<br>Rotary (Reve<br>Boring  | I of Const<br>ventional)<br>erse)  | truction<br>Diamond<br>Jetting<br>Driving<br>Digging   |  | ublic<br>omestic<br>vestock<br>igation   | Well Us Comme Municip X Test Ho Cooling  | so<br>rcial   Not used<br>al   Dewatering<br>le   Mcuitoring<br>& Air Conditioning  | Pump intake set all<br>30.4<br>Pumping rate(Imm)<br>22.72<br>Duration of pumping<br><u>6</u> hrs + <u>0</u><br>Final water level end  | Mant)<br>(GPM)<br>3<br>min<br>d of pumping (Mar  | 2<br>3<br>4<br>5<br>10   |   | 2<br>3<br>4<br>5<br>10   |                         |
| Method<br>Cable Tool<br>Rotary (Conv<br>Rotary (Reve<br>Boring<br>Air percussio<br>Other, specify  | ventional)<br>arse)  | Truction<br>Diamond<br>Jetting<br>Driving<br>Digging   |  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify  | Well Us Comme Municip X Test Ho Cooling  | rcial   Not used<br>al   Dewatering<br>la   Mouitoring<br>& Air Conditioning  | Pump intake set all<br>30.4<br>Pumping rate(Imin)<br>22.72<br>Duration of pumping<br><u>6</u> hrs + <u>0</u><br>Final water level end<br>21.5<br>If flowing give rate (IV)  | 面称)<br>(GPM)<br>3<br>- min<br>d of pumping (例)<br>(イ<br>(min/GPM)  | 2<br>3<br>4<br>5<br>10<br>10   |   | 2<br>3<br>4<br>5<br>10<br>15   |                         |
| Method<br>Cable Tool<br>Rotary (Corve<br>Boring<br>Air percussio<br>Other, specify   | yentional)<br>arse)<br>y<br>Const  | truction Diamond Jetting Driving Digging   |  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>sing  | Well Us<br>Comme<br>Municip<br>Test Ho<br>Cooling  | so<br>crial   Not used<br>al   Dewatering<br>b   Moultoring<br>& Air Conditioning<br>Status of Well<br>  Wells  | Pump intake set al(<br>Pumping rate(fmg)<br>20.72<br>Duration of pumping<br><u>htts + O</u><br>Final water level end<br>21.5<br>If flowing give rate (ii  | Mat)<br>GPM)<br>3<br>min<br>d of pumping (Mat<br>Y<br>min/GPM)   | 2<br>3<br>4<br>5<br>10<br>15<br>20   |   | 2<br>3<br>4<br>5<br>10<br>15<br>20   |                         |
| Method<br>Cable Tool<br>Rotary (Com<br>Rotary (Reve<br>Boring<br>Air percussio<br>Other, specify<br>Inside<br>iameter<br>(Com<br>definin)  | I of Const<br>ventional)<br>an<br>y<br>Const<br>Open Hole Of<br>Galvarized, F<br>2000000000000000000000000000000000000   | truction Diamond Jetting Diving Digging Unigging Truction Re R Material Foreglass, Sric Stael  | PARTIES CONTRACTOR CON | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>sing<br>Depti<br>From   | Well Us Comme Municip STest Ho Cooling Cooling () () () () () () () () () () () () ()  |   | Pump indexe set at (<br>Pumping rate(fmg)<br>20.72<br>Duration of pumping<br>6 hrs + 0<br>Final water level end<br>21.5<br>If flowing give rate (if<br>Recommended pum<br>30.5  | 128<br>17 GPM)<br>17 GPM)<br>10 f pumping (11)<br>17 (11)<br>17 (11)<br>18 (11)<br>18 (11)<br>18 (11)<br>18 (11)<br>18 (11)<br>18 (11)<br>19 (11 | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25   |   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25   |                         |
| Method<br>Cable Tool<br>Rotary (Com<br>Rotary (Reve<br>Boring<br>Air percussio<br>Other, specify<br>inside<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commeter<br>Commete  | I of Const<br>ventional)<br>arse)<br>y<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const | truction   | PA<br>DA<br>DA<br>DA<br>DA<br>DA<br>DA<br>DA<br>DA<br>DA<br>DA<br>DA<br>DA<br>DA   | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>sing<br>From  | Well Us<br>Comme<br>Municip<br>IS Test Ho<br>Cooling<br>To<br>To   | se<br>rrial   Not used<br>a   Dewatering<br>b   Moultoring<br>& Air Conditioning<br>Status of Well<br>  Water Supply<br>  Roplacement Well<br>  Roplacement Well<br>  Roplacement Well<br>  Roplacement Well  | Pump intake set al<br>30.4<br>Pumping rate(min)<br>20.72<br>Duration of pumping<br><u>6</u> hrs + <u>0</u><br>Final water level end<br>11 flowing give rate (i/<br>Recommended pum<br><u>30.4</u><br>Recommended pum  | main<br>min<br>d of pumping (1994)<br>min/GPM)<br>mp depth (1991)<br>18<br>mp rate   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30   |   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30   |                         |
| Method<br>Cable Tool<br>Rotary (Com<br>Rotary (Com<br>Rotary (Row<br>Boring<br>Air percussio<br>Other, specify<br>Inside<br>Com<br>Com<br>Com<br>Com<br>Com<br>Com<br>Com<br>Com<br>Com<br>Com   | i of Const<br>ventional)<br>aree)<br>m<br>y<br>Const<br>Gatvarized, F<br>Soncrete, Pias<br>Steel   | truction   | PA<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D  | ublic<br>omestic<br>vestock<br>tigation<br>dustrial<br>ther, specify<br>sing<br>From<br>+.50   | ₩ell Us<br>☐ Comme<br>☐ Municip<br>⊠ Test Ho<br>☐ Cooling<br>To<br>⑤{, CCO<br>戶<br>⑤{, CCO<br>戶<br>↓<br>↓<br>↓<br>↓<br>↓<br>↓<br>↓<br>↓<br>↓<br>↓<br>↓<br>↓<br>↓   | se<br>rcial   Not used<br>al   Dewatering<br>b   Maultoring<br>& Air Conditioning<br>Status of Well<br>  Water Supply<br>  Roplacement Well<br>  Rocharge Well<br>  Dewatering Well<br>  Deservation and/or   | Pump indexe set all<br>30.4<br>Pumping rated from<br>20.72<br>Duration of pumping<br><u>6 hts + 0</u><br>Final water level end<br>21.5<br>If flowing give rate (i/<br>Recommended pum<br>(mm)GPM)<br>20.7<br>Well production (/mi   | main<br>min<br>d of pumping (1)<br>d of pumping (1)<br>The depth (1)<br>mp depth (1)<br>18<br>19<br>19<br>19<br>19<br>19<br>19<br>19<br>19<br>19<br>19   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40   |   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40   |                         |
| Method<br>Cable Tool<br>Rotary (Came<br>Boring<br>Air parcussio<br>Other, specific<br>Air parcussio<br>Other, specific<br>Air parcussio<br>Other, specific<br>Air parcussio<br>Company<br>Air parcussio<br>Air parcussio<br>Air parcussio<br>Air Air Air Air Air Air Air Air Air Air   | I of Const<br>wertional)<br>my<br>Const<br>Doen Hole Of<br>Galvarized, F<br>Scheel<br>Steel +  | truction   | B<br>B<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>her, specify<br>Sing<br>From<br>+,50<br>83,08  | Well Us<br>Comme<br>Municip<br>X Test Ho<br>Cooling<br>To<br>Sq. ccc<br>Sq. ccc  |   | Pump intake set al<br>30.4<br>Pumping rate(Imp)<br>20.72<br>Duration of pumping<br>6 hrs + 0<br>Final water level end<br>21.5<br>If flowing give rate (i/<br>Recommended pum<br>30.4<br>Recommended pum<br>30.4  | main<br>Market State<br>Market Sta   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50   |   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50   |                         |
| Method<br>Cable Tool<br>Rotary (Carve<br>Boring<br>Ar percussio<br>Other, specify<br>Inside<br>Comment<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Scie  | steel +  | truction   | 00000 - Ca<br>Wat<br>™dom<br>  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>From<br>+.50<br>88.08   | Well Us<br>Comme<br>Municip<br>Test Ho<br>Cooling<br>To<br>Sq. ccc<br>Sq. ccc  | se<br>rrial   Not used<br>al   Dewatering<br>be   Mailtoning<br>Status of Well<br>  Water Supply<br>Replacement Well<br>  Deserting Well<br>  Deserting Well<br>  Desertation Monitoring Hole<br>  Alteration<br>(Construction)<br>  Abandoned,<br>  Entertion  | Pump intake set at (<br>30.4<br>Pumping rate(<br>20.72<br>Duration of pumping<br>6 hrs + 0<br>21.5<br>if flowing give rate (i<br>Recommended pum<br>(m) GPM<br>20.4<br>Recommended pum<br>(m) Disinfected?<br>§ Yes □ No  | man<br>PGPU1<br>3<br>min<br>d of pumping (199<br>Y<br>Y<br>minVGPM)<br>mp depth (1971)<br>18<br>mp rate<br>73<br>inVGPM)   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60   |   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>54<br>60   |                         |
| Method<br>Cable Tool<br>Rotary (Cam<br>Rotary (Reve<br>Boring<br>Art parcussio<br>Other, specify<br>Inside<br>Other, specify<br>Inside<br>Collection<br>S.24   | I of Const<br>vertional)<br>arse)<br>y<br><u>Const</u><br>Const<br>Steel<br>+<br>Const   | Truction Diamond Jeting Driving Driving Digging Truction Re R Material Rrogass, stic, Steel) K Becker  | PR<br>DU<br>UU<br>III<br>III<br>III<br>III<br>IIII<br>IIII<br>IIIII<br>IIIII<br>IIII   | ublic<br>omestic<br>vestock<br>tigation<br>ther, specify<br>From<br>+.50<br>& & C  | Well Us<br>Comme<br>Municip<br>S Test Ho<br>Cooling<br>To<br>S Test Yo<br>S Test Ho<br>Cooling   | so<br>rolal   Not used<br>al   Dewatering<br>b   Maultoring<br>& Air Conditioning<br>Status of Well<br>  Water Supply<br>  Roplacement Well<br>  Roplacement Well<br>  Dewatering Well<br>  Dewatering Well<br>  Deservation and/or<br>  Alternition<br>(Construction)<br>  Abandoned, Poor<br>Water Cuelby   | Pump intake set all<br>30.4<br>Pumping rate(fmg)<br>23.72<br>Duration of pumping<br><u>6</u> hts + 0<br>Final water level end<br>21.5<br>If flowing give rate (i/<br>Recommended pum<br>(mg) GPM)<br>23.4<br>Recommended pum<br>(mg) GPM)<br>23.4<br>Recommended pum<br>(mg) GPM)<br>23.4<br>Pinal Set (intervention)<br>(mg) Set (intervention)  | map below follow   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60   | J.5<br>ation  | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>74 60  | 2.24<br>2.24            |
| Method<br>Cable Tool<br>Rotary (Com<br>Rotary (Rave<br>Boring<br>Mr parcussio<br>Other, specify<br>Inside<br>(Cable)<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Comparison<br>Compar   | i of Const<br>vertional)<br>arse)<br>m<br>y<br>Const<br>Sheel<br>heel +<br>Const<br>attent<br>teel +   | truction Diamond Jeting Onlying Driving Diging Truction Re R Material Rengass, sic, Steel) K Backer muction Re ad ized, Stoel)   | PA<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>From<br>From<br>Depti<br>From   | Wall Us           □ Comme           □ Municip           ⊠ Test Ho           □ Cooling           □ To           ⑤ ¶, CC           ⑧ ¶, CC           ⑧ ¶, CC           ⑨ ¶, To           ⑤ ¶, CC           ⑨ ¶, To           ⑤ ¶, CC           ⑨ ¶, To           ⑤ ¶, CC           ⑨ ¶, To           □ To  |   | Pump indexe set all<br>30.4<br>Pumping rate(fmg)<br>20.72<br>Duration of pumping<br><u>6</u> hrs + 0<br>Final water level end<br>21.5<br>If flowing give rate (i/<br>Recommended pum<br>(mg)GPM)<br>20.4<br>Recommended pum<br>(mg)GPM)<br>20.4<br>Recommended pum<br>(mg)GPM)<br>20.4<br>Plasse provide a m  | min<br>d of pumping (f)<br>y<br>min<br>d of pumping (f)<br>y<br>min(GPM)<br>mp depth (f)<br>t<br>8<br>73<br>in(GPM)<br>Map of V<br>map below follow  | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60   | JI.5<br>atton<br>uctions o<br>89                              | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>50<br>50   | ×                       |
| Method<br>Cable Tool<br>Rotary (Reve<br>Boring<br>Traido<br>Other, specify<br>Inside<br>Differ<br>Differ<br>Differ<br>Color<br>S. 24<br>J. (6<br>S<br>S. 24<br>J. (6<br>S<br>S<br>S. 24<br>J. (6<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S<br>S  | I of Const<br>ventional)<br>arse)<br>y<br>Const<br>y<br>Const<br>Steel<br>+<br>Const<br>Steel<br>+<br>Const<br>Steel<br>Const<br>Steel<br>Steel  | truction Disping Uniting Driving Driving Driving Driving Driving Sic, Steel KBacker Function Re fail fazed, Steel  | P<br>P<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D   | bbic<br>omestic<br>vestock<br>gation<br>dustrial<br>ther, specify<br>From<br>+.50<br>83.00<br>From<br>From<br>Depti<br>From<br>B3.00                                     | Well Us           Comme           Municip           Municip           Test Ho           Cooling           B1, cool   | Status of Well  Status of Well  Status of Well  Water Supply  Replacement Well  Dewatering Well  Dewatering Well  Dewatering Well  Observation and/or  Monitoring Hole  Alteration  (Construction)  Abandoned, Insufficient Supply  Abandoned, Poor  Water Quality  Dandoned, other,  specify  Dither specify  Dither specify   | Pump intake set all<br>30.4<br>Pumping rate(mp)<br>27.72<br>Duration of pumping<br>6 hrs + 0<br>21.5<br>if flowing give rate (i/<br>Recommended pum<br>6.1.5<br>if flowing give rate (i/<br>Recommended pum<br>6.1.5<br>if flowing give rate (i/<br>Recommended pum<br>6.1.5<br>1.5<br>1.5<br>1.5<br>1.5<br>1.5<br>1.5<br>1.5   | man below follow   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>0<br>0<br>15<br>50<br>10<br>15<br>50<br>10<br>15<br>50<br>10<br>15<br>50<br>10<br>15<br>50<br>10<br>15<br>50<br>10<br>15<br>50<br>10<br>15<br>50<br>10<br>15<br>50<br>10<br>15<br>50<br>10<br>15<br>15<br>10<br>15<br>15<br>10<br>15<br>15<br>10<br>10<br>15<br>15<br>10<br>10<br>15<br>15<br>10<br>10<br>15<br>15<br>10<br>10<br>15<br>15<br>10<br>10<br>15<br>10<br>10<br>15<br>10<br>10<br>15<br>10<br>10<br>15<br>10<br>10<br>15<br>10<br>10<br>15<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10 | V<br>21,5<br>attors o<br>&9                                   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>60<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50                               | 2.24<br>k               |
| Method<br>Cable Tool<br>Rotary (Cam<br>Rotary (Reve<br>Boring<br>Inside<br>Other, specify<br>Inside<br>Collection<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Science<br>Scie  | I of Const<br>vertional)<br>arse)<br>y<br>Const<br>Steel +<br>Const<br>aste, Galvan<br>Staon   | Truction Diamond Jeting Driving Driving Digging Truction Re R Material Frenglass, sic, Steel) K Becker Fraction Re fail fized, Steel)  | PP<br>DD<br>DU<br>U<br>U<br>U<br>U<br>U<br>U<br>U<br>U<br>U<br>U<br>U<br>U<br>U<br>U<br>U<br>U   | ublic<br>omestic<br>vestock<br>(gation<br>ther, specify<br>sing)<br>Depti<br>From<br>±.50<br>&\$3.06<br>From<br>Depti<br>From<br>B&1.00                                  | Well Us           □ Comme           □ Municipy           ⊠ Test Ho           □ Cooling           ∅           ™           ™           ™           ™           ™           ™           ™           ™           ™           ™           ™           ™           ™           ™           Ø   | so<br>rotal   Not used<br>al   Dewatering<br>b   Mailtoring<br>& Air Conditioning<br>Status of Well<br>  Water Supply<br>  Roplacement Well<br>  Roplacement Well<br>  Rocharge Well<br>  Deservation and/or<br>Monitoring Hole<br>  Alternition<br>(Construction)<br>  Abandoned, Poor<br>Water Qualty<br>  Abandoned, other,<br>specify<br>  Other, specify   | Pump intake set all<br>30.4<br>Pumping rate(fmg)<br>23.72<br>Duration of pumping<br><u>6</u> hts + 0<br>Final water level end<br>21.5<br>If flowing give rate (i/<br>Recommended pum<br>(mm) GPM)<br>23.4<br>Recommended pum<br>(mm) GPM)<br>23.4<br>Recommended pum<br>Piease provide a m<br>1 1   | min<br>d of pumping (1)<br>min<br>d of pumping (1)<br>min/GPM)<br>mp rate<br>73<br>mGPM)<br>Map of V   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>50<br>60<br>50<br>60<br>50<br>60   | V<br>21,5<br>ation:<br>89                                     | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>74 60  | 2.24<br>2.24            |
| Method<br>Cable Tool<br>Rotary (Cam<br>Rotary (Rave<br>Boring<br>Art parcussio<br>Other, specify<br>maids<br>(Cable Tool<br>(Cable Tool<br>(Cabl  | I of Const<br>vertional)<br>arse)<br>y<br>Const<br>Steel<br>teel +<br>Const<br>astic, Gatvan<br>Steel<br>Steel   | truction Diamond Jeting Driving Driving Driving Driving Truction Re K Backer K Backer  | PR<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>frer, specify<br>From<br>1:50<br>88.08<br>reeen<br>Depti<br>From   | Well Us           □ Comme           Municip           ⊠ Test Ho           ⊡ Cooling           ™     <  |   | Pump intake set all<br>30.4<br>Pumping rate(fmg)<br>20.72<br>Duration of pumping<br><u>6</u> hrs + 0<br>Final water level end<br>21.5<br>If flowing give rate (i/<br>Recommended pum<br>(mi)GPM)<br>Disinfected?<br>Xell production (/mi)<br>Disinfected?<br>No<br>Piease provide a m<br>1<br>1   | min<br>d of pumping (Mi<br>d of pu   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | J<br>J<br>J<br>J<br>J<br>J<br>J<br>S<br>J<br>S<br>S<br>S<br>S | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50   | 2.24<br>x               |
| Method<br>Cable Tool<br>Rotary (Com<br>Rotary (Rave<br>Boring<br>Air parcussio<br>Other, spocify<br>missio<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Simeter<br>Com<br>Sim<br>Com<br>Sim<br>Sim<br>Com<br>Sim<br>Sim<br>Com<br>Sim<br>Sim<br>Com<br>Sim<br>Com<br>Sim<br>Com | I of Const<br>ventional)<br>arse)<br>y<br>Const<br>Steel<br>teel +<br>Const<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel<br>Steel  | Truction   | Corrd - Sci<br>Sol No.<br>6<br>ilis<br>Fresh<br>ify  | Ablic<br>omestic<br>vestock<br>(gation<br>dustrial<br>ther, specify<br>From<br>+.50<br>83.08<br>From<br>+.50<br>83.08<br>From<br>83.00<br>From<br>83.00<br>From<br>83.00 | Wall Us           □ Comme           □ Municip           ⊠ Test Ho           □ Cooling           □ To           ⑧ 1.00           ⑧ 1.00           ⑧ 1.00           ⑨ 1.00  |   | Pump intake set all<br>30.44<br>Pumping rate(mp)<br>20.72<br>Duration of pumping<br>6 hrs + 0<br>21.5<br>if flowing give rate (i/<br>Recommended pum<br>50.4<br>Recommended pum<br>(mm)GCPM<br>20.7<br>Recommended pum<br>(mm)GCPM<br>20.7<br>Recommended pum<br>(mm)GCPM<br>20.7<br>Recommended pum<br>(mm)GCPM<br>20.7<br>Recommended pum<br>(mm)GCPM<br>20.7<br>Recommended pum<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>20.7<br>(mm)GCPM<br>2 | man<br>min<br>d of pumping (1997<br>y<br>y<br>minVGPM)<br>modepth (1978)<br>18<br>73<br>map below follow<br>↓<br>15m<br>↓  | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>0<br>0<br>8<br>8<br>H Liac   | V<br>21,5<br>attion 8<br>89                                   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>60<br>50   | 2.24                    |
| Method<br>Cable Tool<br>Rotary (Reve<br>Boring<br>Art percussio<br>Other, specify<br>Inside<br>Collection<br>Science<br>Science<br>Collection<br>Science<br>Collection<br>Science<br>Collection<br>Science<br>Collection<br>Science<br>Collection<br>Science<br>Collection<br>Science<br>Collection<br>Collection<br>Science<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collection<br>Collecti 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Const<br>vertional)<br>arse)<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>C | truction Diamond Jeting Jeting Driving Diging Truction Re R Material Received R Material Received R Store) K Beckee Ruction Re Ructi | P<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D<br>D   | Ablic<br>omestic<br>vestock<br>(gation<br>ther, specify<br>sing)<br>From<br>4.50<br>88.08<br>reeen<br>Depti<br>From<br>89.00   | Well Us           Comme           Municipy           Municipy           Test Ho           Cooling           STest Ho           Cooling           Status  | Status of Well  Status of Well  Status of Well  Water Supply  Replacement Well  Replacement Well  Replacement Well  Replacement Well  Replacement Well  Atternition  Atternit | Pump intake set all<br>30.4<br>Pumping rate(fmg)<br>20.72<br>Duration of pumping<br><u>6</u> hts + 0<br>Final water level end<br>21.5<br>if flowing give rate (i/<br>Recommended pum<br><u>8</u> Yes □ No<br>Please provide a m<br>1<br>1<br>1<br>2<br>2<br>4<br>1<br>5<br>1<br>1<br>2<br>1<br>2<br>1<br>2<br>1<br>2<br>1<br>2<br>1<br>2<br>1<br>2<br>1<br>2<br>1<br>2<br>1<br>2<br>1<br>2<br>2<br>2<br>2<br>4<br>1<br>5<br>Mo<br>1<br>2<br>2<br>2<br>2<br>2<br>2<br>2<br>2<br>2<br>2<br>2<br>2<br>2  | min     for the second s   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | v<br>JI.5<br>89   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>40<br>50<br>74 60  | ×                       |
| Method<br>Cable Tool<br>Rotary (Corn<br>Rotary (Reve<br>Boring<br>Ar percussio<br>Other, specify<br>Inside<br>Other, specify<br>Other, specify<br>Inside<br>Other, specify<br>Inside<br>Inside<br>Inside<br>Other, specify<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside   | I of Const<br>vertional)<br>arse)<br>y<br>Const<br>y<br>Const<br>Steel +<br>Const<br>steel +<br>Const<br>steel +   | Truction Diamond Jeting Driving Driving Driving Driving Driving R Material Frendass, stic, Steel) KBckee Frendass, stic, Steel) KBckee Guided State: Other, spec d of Water: Other, spec d of Water:   | PR           D           Fresh           dify           D           Fresh  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>ther, specify<br>sing:<br>Depti<br>From<br>±.50<br>&\$.08<br>From<br>Depti<br>From<br>\$9,00<br>Voltested          | Well Us           □ Comme           Municip           ⊠ Test Ho           □ Cooling           ∅Ti)           To           ⑧1.00           ⑧1.00           ⑧1.00           ⑧1.00           ⑧1.00           ⑧1.00           ⑧1.00           ⑧1.00           ⑧1.00           ⑧1.00           ⑧1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00           ●1.00  | So     Image: Solution of the second se                          | Pump index set all<br>30.44<br>Pumping rate(fmg)<br>23.72<br>Duration of pumping<br><u>burntion of pumping</u><br><u>chrs + O</u><br>Final water level end<br>21.5<br>If flowing give rate (ii<br>Recommended pum<br>30.4<br>Recommended pum<br>30.4<br>30.4<br>30.4<br>30.4<br>Recommended pum<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4   | $\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} $   | 2<br>3<br>4<br>5<br>0<br>10<br>15<br>20<br>25<br>30<br>40<br>60<br>60<br>60  | J J J J J J J J J J J J J J J J J J J                         | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>74<br>60   | 2.24                    |
| Method<br>Cable Tool<br>Rotary (Cam<br>Rotary (Rave<br>Boring<br>Ar percussio<br>Other, specify<br>inmeter<br>(Din) C<br>S, O4<br>9.(6<br>S)<br>(6<br>S)<br>(6<br>S)<br>(6<br>S)<br>(6<br>S)<br>(7)<br>(7)<br>(7)<br>(7)<br>(7)<br>(7)<br>(7)<br>(7)<br>(7)<br>(7  | I of Const<br>vertional)<br>arse)<br>m<br><u>y</u><br>Const<br>Steel +<br>Steel +<br>Steel +<br>Steel +<br>Depth Kin<br>Gas Depth Kin<br>Gas Depth Kin   | Truction Diamond Jeting Driving Driving Digsing Truction Re R Material Rendars, sic, Steel) K Backer Ruction Re ad ized, Steel) K Backer Giter, spec d of Water: Other, spec d of Water: Other, spec   |  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>from<br>From<br>B88.08<br>From<br>B88.00<br>From<br>B89.00<br>Vuntested  | Wall Us           □ Comme           Municip           ⊠ Test Ho           □ Cooling           □ To           ⑤ 1. cO           ⑧ 1. cO           ⑧ 1. cO           ⑧ 1. cO           ⑧ 1. cO           ⑨ 1. cO           ◎ 1. cO           ○ 1. cO           ○ 1. cO           ○ 1. cO   |   | Pump indexe set all<br>30.4<br>Pumping rate(fmg)<br>  | $\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} $   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60   | JI.3<br>ation 8<br>wetions o<br>89                            | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>50<br>50<br>50   | - A                     |
| Method<br>Cable Tool<br>Rotary (Com<br>Rotary (Rave<br>Boring<br>Air parcussio<br>Other, specify<br>Inside<br>Com<br>Simeter (C<br>Com<br>Com<br>Com<br>Com<br>Com<br>Com<br>Com<br>Com<br>Com<br>Co   | I of Const<br>ventional)<br>arse)<br>m<br>y<br>Const<br>Steel<br>teel +<br>Const<br>Steel<br>teel +<br>Materia<br>astic, Galvan<br>Steel<br>Kin<br>Gas Depth Kin<br>Gas Depth Kin<br>Gas Const<br>Kin<br>Gas Const<br>Const<br>Steel<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>Const<br>C             | Truction Diamond Jeting Jeting Driving Driving Driving Driving Driving Remainsia Françass, stic, Steel) KBeckee  ruction Re fail ized, Steel) KBeckee  Remainsia Mater Deta d of Water: Other, spec d of Water: Other, spec Contractor nitractor   | P           D  |  | Wall Us           Comme           Municip           Municip           To           S1 Test Ho           Cooling           To           S2 Test Ho           Cooling           To           S2 Cooling           To           S2 Cooling           S1 Cooling           To           S2 Cooling           S1 Cooling           S2 Cooling           S2 Cooling           S2 Cooling           To           S2 Cooling           S2 Cooling <td></td> <td>Pump indexe set all<br/>30.44<br/>Pumping rate(<math>100</math><br/>22.72<br/>Duration of pumping<br/><u>6 hits + 0</u><br/>Final water level end<br/>21.5<br/>if flowing give rate (<math>100</math><br/>Recommended pum<br/>30.4<br/>Recommended pum<br/>30.4<br/>30.4<br/>Recommended pum<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4<br/>30.4</td> <td><math display="block">\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} </math></td> <td>2<br/>3<br/>4<br/>5<br/>10<br/>10<br/>15<br/>20<br/>25<br/>30<br/>40<br/>50<br/>60<br/>60<br/>60</td> <td>v<br/>21,5<br/>ation<br/>89</td> <td>2<br/>3<br/>4<br/>5<br/>10<br/>15<br/>20<br/>25<br/>30<br/>40<br/>50<br/>50<br/>74<br/>60</td> <td>2.24</td> |   | Pump indexe set all<br>30.44<br>Pumping rate( $100$<br>22.72<br>Duration of pumping<br><u>6 hits + 0</u><br>Final water level end<br>21.5<br>if flowing give rate ( $100$<br>Recommended pum<br>30.4<br>Recommended pum<br>30.4<br>30.4<br>Recommended pum<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4<br>30.4   | $\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} $   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60   | v<br>21,5<br>ation<br>89                                      | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>74<br>60   | 2.24                    |
| Method<br>Cable Tool<br>Rotary (Carrow<br>Rotary (Reve<br>Boring<br>Other, specifi<br>Inside<br>Other, specifi<br>Inside<br>Inside<br>Other, specifi<br>Inside<br>Other, specifi<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Inside<br>Ins  | I of Const<br>vertional)<br>arse)<br>Const<br>Steel +<br>Const<br>Steel +<br>Const<br>Steel +<br>Const<br>Steel (<br>Materia<br>asis, Galvan<br>Steel (<br>Const<br>Steel (<br>Const<br>Const<br>Const<br>Steel (<br>Const<br>Steel  | Truction Diamond Jetting Dorwing Dorwing Dorwing Dorwing Dorwing Truction Re A Material Responses Stic, Steel) K Bucker Ruterial Steel Ruter Deta do f Water: Other, spec do f Water: Other, spec Contractor ruter Contractor ruter Steel Ruter Deta Steel Ruter Det  | PR           D   | ublic omestic vestock igation iter, specify sing Depti From 4.50 88.08 reen Depti From 89.00 Untested Untested Technician /.c.   | Well Us           Comme           Municip           Municip           S Test Ho           Cooling           B1           To           S1           S2           S4           S2           S4           S2           S4   |   | Pump indexe set all<br>30.44<br>Pumping rate(fmg)<br>23.72<br>Duration of pumping<br><u>6</u> htts + 0<br>Final water level and<br>21.5<br>If flowing give rate (ii<br>Recommended pum<br>Bisinfected?<br>Xiel production (Imi<br>Disinfected?<br>Xiel production (Imi<br>Disinfected?  | map below follow   | 2<br>3<br>4<br>5<br>10<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60   | JI.55   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>40<br>50<br>74 60  | ×                       |
| Method<br>Cable Tool<br>Rotary (Com<br>Rotary (Rave<br>Boring<br>Thiside<br>Cher, specify<br>Thiside<br>Cher, specify<br>Thiside<br>Cher, specify<br>Thiside<br>Cher, specify<br>Thiside<br>Cher, specify<br>Cher, speci   | I of Const<br>vertional)<br>my<br>Const<br>Den Hole Of<br>Salvarized, Pas<br>Steel +<br>Const<br>Steel +<br>Const<br>Steel +<br>Const<br>Steel (<br>Steel (<br>Const<br>Steel (<br>Steel (   | Truction Diamond Jeting Driving Driving Driving Driving Driving R Material Frequess, Sic, Steel) K Bucket K Bu  |  | ublic omestic vestock igation ductrial ther, specify From +.50 83.08 Freen Depti From 89.00 Untested Untested Technician /   | Well Us           □ Comme           Municip           ⊠ Test Ho           □ Cooling           ☑ Test Ho           ☑ Test Ho           ☑ Test Ho           ☑ Gott)           To           ☑ ① Test Ho           ☑ Gott)           To           ☑ ① Test Ho           ☑ ④1.00           ④1.00           ④1.00           ④1.00           ④1.00           ④1.00           ④1.00           ●1.00  |   | Pump intake set all<br>30.4/<br>Pumping rate(fmg)<br>20.72<br>Duration of pumping<br><u>6</u> hts + 0<br>Final water level end<br>21.5<br>If flowing give rate (i/<br>Recommended pum<br>(mi)GPM)<br>20.4<br>Well production (fmi)<br>Disinfected?<br>8 Yes   No<br>Piease provide a m<br>1<br>1<br>2<br>2<br>4<br>5<br>4<br>5<br>1<br>1<br>2<br>2<br>4<br>5<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>5<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1  | $\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} $   | 2<br>3<br>4<br>5<br>0<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60  | JI.5<br>Viliation So<br>Seq                                   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>50<br>50<br>50   | 2.24                    |
| Method<br>Cable Tool<br>Rotary (Com<br>Rotary (Com<br>Rotary (Rave<br>Boring<br>Ar parcussio<br>Other, specify<br>ameter<br>(Diff)<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C<br>C   | I of Const<br>vertional)<br>arse)<br>m<br>Const<br>Const<br>Steel<br>teel +<br>Const<br>Steel<br>teel +<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Const<br>Steel<br>Con | Truction Diamond Diamond Diging Driving Driving Driving Driving Driving R Material Rendiass, sic, Steel) K Backet Ruterial Rendiass, sic, Steel K Backet Ruterial Rendiass, sic, Steel Ruterial Rendiass Ruterial  |  | ublic<br>omestic<br>vestock<br>igation<br>dustrial<br>from<br>1.50<br>88.08<br>reen<br>Dept<br>From<br>88.00<br>Vuntested<br>Untested<br>Untested                        | Well Us           □ Comme           □ Municip           ⊠ Test Ho           □ Cooling           ☑ To           ☑ O   |   | Pump index set at(<br>30.4)         Pumpin rate(fmg)  | min<br>GPU)<br>S<br>GPU)<br>S<br>min<br>d of pumping (M<br>Y<br>minGPM)<br>np depth (M)<br>15 m<br>↓<br>15 m<br>↓<br>15 m<br>↓<br>15 m   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>60<br>60<br>60   | JI.3<br>ation<br>89   | 2<br>3<br>4<br>5<br>10<br>15<br>20<br>25<br>30<br>40<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>40<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50 | 2.24<br>2.24            |

•

# APPENDIX D

Groundwater Sampling Results



Project Number: 1101-4125

Project Location: 7723 Highway 89, Alliston Sample Date: July 30th, 2021

Sampled by: CM

Prepared by: CM

Checked by: CG/KR

|                  | Λ          | NONITORI | NG WELL | WATER QU | ALITY RES | ULTS JULY | 2021     |          |       |
|------------------|------------|----------|---------|----------|-----------|-----------|----------|----------|-------|
| Parameter        | Unit       | G/S      | RDL     |          |           | Well      |          |          | Notes |
|                  |            |          |         | MW1      | MW2       | MW3       | MW4      | MW5      |       |
| E.Coli           | CFU/100 mL | 0        | 2       | ND       | ND        | ND        | ND       | ND       | MAC   |
| Total Coliforms  | CFU/100 mL | 0        | 100     | 3100     | 700       | 800       | 1500     | 2800     | MAC   |
| Flouride         | mg/L       | 1.5      | 0.05    | <0.05    | 0.2       | <0.05     | <0.05    | <0.05    | MAC   |
| Chloride         | mg/L       | 250      | 0.10    | 20       | 23.9      | 236       | 1100     | 48.7     | AO    |
| Nitrate          | mg/L       | 10       | 0.05    | 5.93     | 8.57      | <0.05     | 0.9      | 0.74     | MAC   |
| Nitrite          | mg/L       | 1        | 0.05    | 0.25     | 0.33      | <0.05     | <0.11    | 0.38     | MAC   |
| Bromide          | mg/L       |          | 0.05    | < 0.05   | < 0.05    | <0.05     | <0.11    | <0.05    |       |
| Sulphate         | mg/L       | 500      | 0.10    | 14       | 53.2      | 30.5      | 42.6     | 56.3     | AO    |
| Phosphate        | mg/L       |          | 0.10    | <0.10    | <0.10     | <0.10     | <0.26    | <0.10    |       |
| lotal Aluminum   | mg/L       | 0.1      | 0.010   | 1.410    | 0.022     | 0.045     | 0.027    | 0.01     | OG    |
| Total Antimony   | mg/L       | 0.006    | 0.003   | < 0.003  | < 0.003   | < 0.003   | < 0.003  | <0.003   | MAC   |
| Total Arsenic    | mg/L       | 0.025    | 0.003   | < 0.003  | < 0.003   | < 0.003   | < 0.003  | < 0.003  | MAC   |
| Total Barium     | mg/L       | 1        | 0.002   | 0.060    | 0.136     | 0.226     | 0.407    | 0.140    | MAC   |
| Total Beryllium  | mg/L       |          | 0.0005  | <0.0005  | <0.0005   | <0.0005   | < 0.0005 | <0.0005  |       |
| Total Bismuth    | mg/L       |          | 0.002   | <0.002   | < 0.002   | < 0.002   | < 0.002  | <0.002   |       |
| Total Boron      | mg/L       | 5        | 0.010   | 0.012    | 0.087     | 0.084     | 0.100    | 0.063    | MAC   |
| Total Cadmium    | mg/L       | 0.005    | 0.0001  | < 0.0001 | <0.0001   | <0.0001   | <0.0001  | <0.0001  | MAC   |
| lotal Chromium   | mg/L       | 0.05     | 0.003   | 0.003    | < 0.003   | < 0.003   | < 0.003  | < 0.003  | MAC   |
| Total Cobalt     | mg/L       |          | 0.0005  | 0.0007   | <0.0005   | <0.0005   | 0.0008   | < 0.0005 |       |
| Total Copper     | mg/L       | 1        | 0.001   | 0.005    | 0.004     | 0.003     | 0.004    | 0.004    | AO    |
| Total Iron       | mg/L       | 0.3      | 0.010   | 1.54     | 0.013     | 0.053     | 0.030    | 0.01     | AO    |
| Total Lead       | mg/L       | 0.01     | 0.001   | < 0.001  | <0.001    | < 0.001   | < 0.001  | < 0.001  | MAC   |
| Total Manganese  | mg/L       | 0.05     | 0.002   | 0.063    | 0.059     | 0.043     | 0.082    | 0.054    | AO    |
| Total Mercury    | mg/L       | 0.001    | 0.0001  | 0.0001   | <0.0001   | <0.0001   | <0.0001  | <0.0001  | MAC   |
| Total Molybdenum | mg/L       |          | 0.002   | < 0.002  | 0.006     | 0.002     | 0.004    | 0.002    |       |
| lotal Nickel     | mg/L       |          | 0.003   | 0.004    | < 0.003   | < 0.003   | < 0.003  | < 0.003  |       |
| Total Phosphorus | mg/L       |          | 0.10    | <0.10    | <0.10     | <0.10     | <0.10    | <0.10    |       |
| Total Selenium   | mg/L       | 0.05     | 0.002   | < 0.002  | < 0.002   | < 0.002   | < 0.002  | < 0.002  | MAC   |
| Total Silicon    | mg/L       |          | 0.08    | 12.10    | 7.89      | 6.11      | 8.40     | 8.27     |       |
| Total Silver     | mg/L       |          | 0.0001  | < 0.0001 | <0.0001   | <0.0001   | < 0.0001 | < 0.0001 |       |
| Total Strontium  | mg/L       |          | 0.005   | 0.246    | 0.520     | 0.869     | 1.520    | 0.58     |       |
| fotal Thallium   | mg/L       |          | 0.0003  | < 0.0003 | < 0.0003  | < 0.0003  | < 0.0003 | < 0.0003 |       |
| ſotal Tin        | mg/L       |          | 0.002   | <0.002   | <0.002    | <0.002    | <0.002   | < 0.002  |       |
| Total Titanium   | mg/L       |          | 0.002   | 0.085    | <0.002    | 0.003     | 0.004    | 0.003    |       |
| Total Uranium    | mg/L       | 0.02     | 0.0005  | 0.001    | 0.0035    | 0.0026    | 0.0016   | 0.0033   | MAC   |
| Total Vanadium   | mg/L       |          | 0.002   | 0.003    | <0.002    | <0.002    | <0.002   | <0.002   |       |
| Total Zinc       | ma/L       | 5.0      | 0.005   | 0.012    | < 0.005   | < 0.005   | < 0.005  | 0.005    | AO    |
| Total Zirconium  | ma/l       |          | 0.004   | <0.004   | < 0.004   | < 0.004   | <0.004   | < 0.004  |       |

\* - detection limit of 100 CFU/100 mL

\*\* Aesthetic objective for drinking water is 200 mg/L. Where concentrations are found to exceed 20 mg/L, the local medical health officer must be notified.

AO - Aesthetic Objective

MAC - Maximum Allowable Concentration

OG - Operational Guideline

exceeds standard at standard



Project Number: 1101-4125

Project Location: 7723 Highway 89, Alliston

Sampled by: CM

Sample Date: September 7th, 2021

Prepared by: CM

Checked by: CG/KR

|                  |            | TEST WELL | . WATER G | QUALITY RE | SULTS SEP | TEMBER 2 | 021      |          |       |
|------------------|------------|-----------|-----------|------------|-----------|----------|----------|----------|-------|
| Parameter        | Unit       | G/S       | RDL       |            |           | Well     |          |          | Notes |
|                  |            |           |           | TW1        | TW2       | TW3      | TW4      | TW5      |       |
| E.Coli           | CFU/100 mL | 0         | 1         | ND         | 13        | ND       | ND       | ND       | MAC   |
| Total Coliforms  | CFU/100 mL | 0         | 1         | 2          | 41        | 1500*    | 2        | 22       | MAC   |
| Flouride         | mg/L       | 1.5       | 0.05      | 0.38       | <0.05     | 0.27     | <0.05    | 0.17     | MAC   |
| Chloride         | mg/L       | 250       | 0.10      | 15.9       | 19.2      | 42.2     | 19.1     | 14.2     | AO    |
| Nitrate          | mg/L       | 10        | 0.05      | <0.05      | < 0.05    | <0.05    | <0.05    | <0.05    | MAC   |
| Nitrite          | mg/L       | 1         | 0.05      | <0.05      | < 0.05    | <0.05    | <0.05    | <0.05    | MAC   |
| Bromide          | mg/L       |           | 0.05      | <0.05      | 0.22      | 0.48     | <0.05    | <0.05    |       |
| Sulphate         | mg/L       | 500       | 0.10      | 1.72       | 0.31      | 3.39     | 0.32     | 3.74     | AO    |
| Phosphate        | mg/L       |           | 0.10      | <0.10      | <0.10     | <0.10    | <0.10    | <0.10    |       |
| Total Calcium    | mg/L       | 500       | 0.16      | 33.00      | 12.80     | 9.09     | 39.40    | 176.00   | AO    |
| Total Magnesium  | mg/L       | 500       | 0.17      | 19.30      | 16.70     | 5.95     | 19.90    | 25.00    | AO    |
| Total Potassium  | mg/L       |           | 0.58      | 1.88       | 1.67      | 1.59     | 1.66     | 2.72     |       |
| Total Sodium     | mg/L       | 20**      | 0.22      | 62.30      | 31.50     | 92.70    | 19.70    | 24.50    | MAC   |
| Total Aluminum   | mg/L       | 0.1       | 0.010     | 0.013      | 0.014     | 0.017    | 0.059    | 2.46     | OG    |
| Total Antimony   | mg/L       | 0.006     | 0.003     | < 0.003    | < 0.003   | < 0.003  | < 0.003  | < 0.003  | MAC   |
| Total Arsenic    | mg/L       | 0.025     | 0.003     | < 0.003    | < 0.003   | < 0.003  | < 0.003  | < 0.003  | MAC   |
| Total Barium     | mg/L       | 1         | 0.002     | 0.064      | 0.059     | 0.059    | 0.051    | 0.103    | MAC   |
| Total Beryllium  | mg/L       |           | 0.0005    | < 0.0005   | < 0.0005  | < 0.0005 | < 0.0005 | < 0.0005 |       |
| Total Bismuth    | mg/L       |           | 0.002     | < 0.002    | < 0.002   | <0.002   | <0.002   | < 0.002  |       |
| Total Boron      | mg/L       | 5         | 0.010     | 0.169      | 0.114     | 0.172    | 0.098    | 0.111    | MAC   |
| Total Cadmium    | mg/L       | 0.005     | 0.0001    | < 0.0001   | < 0.0001  | <0.0001  | <0.0001  | < 0.0001 | MAC   |
| Total Chromium   | mg/L       | 0.05      | 0.003     | < 0.003    | < 0.003   | < 0.003  | < 0.003  | 0.004    | MAC   |
| Total Cobalt     | mg/L       |           | 0.0005    | < 0.0005   | <0.0005   | <0.0005  | < 0.0005 | 0.0013   |       |
| Total Copper     | mg/L       | 1         | 0.001     | 0.003      | 0.003     | 0.001    | 0.003    | 0.010    | AO    |
| Total Iron       | mg/L       | 0.3       | 0.010     | 2.36       | 0.121     | 0.112    | 0.452    | 3.76     | AO    |
| Total Lead       | mg/L       | 0.01      | 0.001     | < 0.001    | <0.001    | < 0.001  | <0.001   | 0.002    | MAC   |
| Total Manganese  | mg/L       | 0.05      | 0.002     | 0.223      | 0.065     | 0.020    | 0.205    | 0.374    | AO    |
| Total Mercury    | mg/L       | 0.001     | 0.0001    | < 0.0001   | <0.0001   | <0.0001  | <0.0001  | < 0.0001 | MAC   |
| Total Molybdenum | mg/L       |           | 0.002     | 0.020      | 0.002     | 0.031    | 0.004    | 0.005    |       |
| Total Nickel     | mg/L       |           | 0.003     | < 0.003    | < 0.003   | < 0.003  | < 0.003  | < 0.003  |       |
| Total Phosphorus | mg/L       |           | 0.10      | <0.10      | <0.10     | <0.10    | 0.22     | 0.92     |       |
| Total Selenium   | mg/L       | 0.05      | 0.002     | <0.002     | <0.002    | <0.002   | < 0.002  | < 0.002  | MAC   |
| Total Silicon    | mg/L       |           | 0.08      | 0.98       | 0.20      | 0.44     | 2.63     | 7.57     |       |
| Total Silver     | mg/L       |           | 0.0001    | < 0.0001   | <0.0001   | <0.0001  | <0.0001  | < 0.0001 |       |
| Total Strontium  | mg/L       |           | 0.005     | 0.507      | 0.583     | 0.184    | 0.759    | 1.10     |       |
| Total Thallium   | mg/L       |           | 0.0003    | < 0.0003   | < 0.0003  | < 0.0003 | < 0.0003 | < 0.0003 |       |
| Total Tin        | mg/L       |           | 0.002     | <0.002     | <0.002    | <0.002   | <0.002   | <0.002   |       |
| Total Titanium   | mg/L       |           | 0.002     | <0.002     | <0.002    | <0.002   | <0.002   | 0.087    |       |
| Total Uranium    | mg/L       | 0.02      | 0.0005    | <0.0005    | <0.0005   | 0.0007   | <0.0005  | <0.0005  | MAC   |
| Total Vanadium   | mg/L       |           | 0.002     | <0.002     | <0.002    | <0.002   | <0.002   | 0.004    |       |
| Total Zinc       | mg/L       | 5.0       | 0.005     | <0.005     | <0.005    | <0.005   | <0.005   | 0.010    | AO    |
| Total Zirconium  | mg/L       |           | 0.004     | <0.004     | < 0.004   | < 0.004  | < 0.004  | < 0.004  |       |

\* - detection limit of 100 CFU/100 mL

\*\* Aesthetic objective for drinking water is 200 mg/L. Where concentrations are found to exceed 20 mg/L, the local

medical health officer must be notified.

AO - Aesthetic Objective

MAC - Maximum Allowable Concentration OG - Operational Guideline

exceeds standard at standard



Project Number: 1101-4125

Project Location: 7723 Highway 89, Alliston

Sampled by: CM

Sample Date: October 8th, 2021

Prepared by: CM

Checked by: CG/KR

|                 |            | TEST WEL | L WATER ( | QUALITY R | ESULTS OC | CTOBER 20 | 021   |       |       |
|-----------------|------------|----------|-----------|-----------|-----------|-----------|-------|-------|-------|
| Parameter       | Unit       | G/S      | RDL       |           |           | Well      |       |       | Notes |
|                 |            |          |           | TW1       | TW2       | TW3       | TW4   | TW5   |       |
| E.Coli          | CFU/100 mL | 0        | 1         | ND        | ND        | ND        | ND    | ND    | MAC   |
| Total Coliforms | CFU/100 mL | 0        | 1         | 21        | 1         | 5700*     | ND    | ND    | MAC   |
| Nitrate         | mg/L       | 10       | 0.05      | <0.05     | <0.05     | <0.05     | <0.05 | <0.05 | MAC   |
| Nitrite         | mg/L       | 1        | 0.05      | <0.05     | <0.05     | <0.05     | <0.05 | <0.05 | MAC   |

\* - detection limit of 100 CFU/100 mL

AO - Aesthetic Objective

MAC - Maximum Allowable Concentration

OG - Operational Guideline

exceeds standard at standard



Project Number: 1101-4125

Project Location: 7723 Highway 89, Alliston

Sampled by: CM

Sample Date: October 8th, 2021

Prepared by: CM

Checked by: CG/KR

|                 | MOI        | NITORING | WELL WA |       | ITY RESUL | TS OCTOB | ER 2021 |       |
|-----------------|------------|----------|---------|-------|-----------|----------|---------|-------|
| Parameter       | Unit       | G/S      | RDL     |       |           | Well     |         | Notes |
|                 |            |          |         | MW1   | MW2       |          |         |       |
| E.Coli          | CFU/100 mL | 0        | 1       | ND    | ND        |          |         | MAC   |
| Total Coliforms | CFU/100 mL | 0        | 1       | 55    | 18        |          |         | MAC   |
| Nitrate         | mg/L       | 10       | 0.05    | 8.57  | 9.26      |          |         | MAC   |
| Nitrite         | mg/L       | 1        | 0.05    | <0.05 | 0.26      |          |         | MAC   |

AO - Aesthetic Objective

MAC - Maximum Allowable Concentration

OG - Operational Guideline

exceeds standard at standard

# APPENDIX E

Pumping Test Results

6891 SR7W, Mt Forest, Ont. N0G 2L0

519-501-4750 MOE Lic. 7719

#### Well Test Data

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| Data Ad  | IL NO. | 2365970 | 1 Well   | Tag No.   | A 309:  | 223     |          |           |          |                  |
|----------|--------|---------|----------|-----------|---------|---------|----------|-----------|----------|------------------|
| Well # T | Statio | 1021    | Client ( | crozier d | Associa | tes - 2 | be Pilla | - Pilla   | Investm  | ents             |
| Tëst .   | Static | Pumping | Rate     | Intke At  | Amnt/   | Casing  | Amnt/S   | Screen    | Ttl Dpth | Datum            |
| WEIL "I  | 630    | 5       | IGPM     | JJ.86m    |         |         | Open     | Hole      | To Grade | Lop of<br>Casing |
| Elapsd   | Wate   | r Level | Draw     | Down      | Reco    | overy   |          | Rem       | narks    |                  |
| Time     | weters | Feet    | weters   | Feet      | Meters  | Feet    | F        | Rock star | rts@     |                  |
| 0        |        |         | 1.0      |           |         |         |          |           |          |                  |
| 1        |        |         | 2.50     |           | 6.64    |         |          |           |          |                  |
| 2        |        |         | 6.56     |           | 6.62    |         |          |           |          |                  |
| 3        |        |         | 6.57     |           | 6.61    |         |          |           |          |                  |
| 4        |        |         | 6.58     |           | 6.61    |         |          |           |          |                  |
| 5        |        |         | 6.58     |           | 6.61    |         | 1        |           |          |                  |
| 6        |        |         | 6.58     |           | 6.61    |         |          |           |          |                  |
| 7        |        |         | 6.58     |           | 6.61    |         |          |           |          |                  |
| 8        |        |         | 6.58     |           | 6.61    |         |          |           |          | P                |
| 9        |        |         | 6.58     |           | 6.61    |         |          |           |          |                  |
| 10       |        |         | 6.58     |           | 6,6     |         |          |           |          |                  |
| 12       |        |         | 10.59    |           | 6.61    |         |          |           |          |                  |
| 14       |        |         | 6.59     |           | 6.60    |         |          |           |          |                  |
| 15       |        |         | 6.59     |           | 6.60    |         |          |           |          |                  |
| 16       |        |         | 6.59     |           | 6.60    |         |          |           |          |                  |
| 18       |        |         | 6,59     |           | 6.60    |         |          |           |          |                  |
| 20       |        |         | 6.59     |           | 6.60    |         |          |           |          |                  |
| 25       |        |         | 9.60     |           | 6,60    |         |          |           |          |                  |
| 30       |        |         | 216      |           | 6.60    |         |          |           |          |                  |
| 35       |        |         | 6.62     |           | 6.59    |         |          |           |          |                  |
| 40       |        |         | 6.62     |           | 6.59    |         |          |           |          |                  |
| 45       |        |         | 6.62     |           | 6.99    |         |          |           |          |                  |
| 50       |        |         | 6.63     |           | 6.58    |         |          |           |          |                  |
| 55       |        |         | 6.63     |           | 6,58    |         |          |           |          |                  |
| 60       | 2      |         | 6.63     |           | 6.58    |         |          |           |          |                  |
| 90       |        |         | 6.68     |           |         |         |          |           |          |                  |
| 2/120    |        |         | 6,70     |           |         |         |          |           |          |                  |
| Drawdowi | n @ 60 | Minutes |          |           |         |         |          |           |          |                  |
| Recovery | @ 60   | Minutes |          |           |         |         |          |           |          |                  |
| Comments | 5      |         |          |           |         |         |          | Page      | 1/2      |                  |

6891 SR7W, Mt Forest, Ont. N0G 2L0

519-501-4750 MOE Lic. 7719

| well #        | Static | Pumping  | Rate   | Intke At       | Amnt/           | Casing         | Amnt/s        | Screen        | Ttl Dpth | Datum            |
|---------------|--------|----------|--------|----------------|-----------------|----------------|---------------|---------------|----------|------------------|
| WELL 1        | 6.30   | 5        | IGPM   | pile men       |                 |                | Open          | Hole          | To Grade | Top of<br>Casing |
| Elapsd        | Wate   | er Level | Draw   | Down           | Reco            | overy          |               | Ren           | narks    |                  |
| Time          | Meters | Feet     | Meters | Feet           | Meters          | Feet           | F             | Rock sta      | rts@     | •                |
| 150           | 6-A    |          | 6.71   |                |                 |                | 1000          |               |          |                  |
| 180           | 677    |          | 6.72   |                | 460             |                |               |               |          |                  |
| 210           | 6.B    |          | 6.73   |                |                 |                |               |               |          |                  |
| \$240         |        |          | 6.75   |                |                 |                |               | 1.2.5         |          |                  |
| 4270          |        |          | 6.78   |                | ·               | and the        | Sector Street |               |          |                  |
| <b>B</b>  300 |        |          | 6.81   |                |                 |                |               |               |          |                  |
| 6 330         |        |          | 6.82   |                |                 |                |               |               |          | 0                |
| * # 3600      |        |          | 6.85   |                |                 |                |               |               |          |                  |
| \$390         | 1      |          |        |                |                 |                |               |               |          |                  |
| 0420          |        |          |        |                |                 |                |               |               | 1        |                  |
| 19450         |        |          |        |                | 4               |                |               | diser (       |          |                  |
| 18480         |        |          |        |                |                 |                |               |               |          | 1                |
| \$5:0         |        |          |        |                |                 |                |               |               |          |                  |
| \$540         |        |          |        |                | 100             |                | -             |               |          |                  |
| 16            |        |          |        | 0.000          |                 |                | 1             |               |          |                  |
| 18            |        |          |        |                | 1000            |                |               |               |          | -                |
| 20            |        |          |        |                |                 | and the second |               |               |          |                  |
| 25            |        |          |        | 0              |                 | 1.11           | 1             | A State State |          |                  |
| 30            |        |          |        |                |                 | 1.90           |               |               |          |                  |
| 35            |        |          |        |                |                 |                |               |               |          |                  |
| 40            |        |          |        | all the second | Constant of the |                |               |               |          |                  |
| 45            |        |          |        |                |                 |                | 1             | 6             |          |                  |
| 50            |        |          |        |                | 1               |                |               |               |          |                  |
| 55            |        |          |        |                | 1               | 1              | +             |               |          |                  |
| 60            |        |          |        |                |                 |                | +             |               |          |                  |
|               |        |          |        | 1              |                 |                |               | 0.            |          |                  |
|               |        |          |        |                | -               |                |               |               |          |                  |
| Drawdown      | @ 60   | Minutes  |        |                |                 |                |               |               |          |                  |
| Recovery      | @ 60   | Minutes  |        |                |                 |                |               |               |          |                  |

6891 SR7W, Mt Forest, Ont. N0G 2L0

519-501-4750 MOE Lic. 7719

| OE Au          | dit No. Z       | -36597        | / Well         | Tag No.      | A3352          | 52           |         |                 |                |        |
|----------------|-----------------|---------------|----------------|--------------|----------------|--------------|---------|-----------------|----------------|--------|
| Date Ju        | ly 12,0         | 2021          | Client         | Crozier      | + Assoc        | iates.       | - Joe F | illa - 1        | tila hve       | sments |
| Vell #         | Static F        | Pumping       | Rate           | Intke At     | Amnt/C         | asing        | Amnt/S  | Screen          | Ttl Dpth       | Datum  |
| 2              | 10.97m          | 5             | IGPM           | 45.11m       |                |              | Open    | Hole            | To Grade       | Casing |
| Elapsd<br>Time | Water<br>Meters | Level<br>Feet | Draw<br>Meters | Down<br>Feet | Reco<br>Meters | very<br>Feet | F       | Ren<br>Rock sta | narks<br>rts @ | •      |
| 0              |                 | C. May        |                |              |                |              |         |                 |                |        |
| 1              | 12.64           | 116 187       |                |              | 38.00          |              |         |                 |                |        |
| 2              | 13.50           | No. of        |                |              | 37.12          |              |         |                 |                |        |
| 3              | 14.20           | S. MB         |                |              | 36.24          |              |         |                 |                |        |
| 4              | 14.63           | 1. 57         |                |              | 35.38          |              |         |                 |                |        |
| 5              | 15.63           | 8.198         |                |              | 34.59          |              |         |                 |                |        |
| 6              | 16.21           | 199 6.00      |                |              | 33,77          |              |         |                 |                |        |
| 7              | 16.82           |               | -              |              | 33,10          |              |         |                 |                |        |
| 8              | 17.37           | 100           |                |              | 32.40          |              |         |                 |                | 7      |
| 9              | 17.89           | all see       |                |              | 31.69          |              |         |                 |                |        |
| 10             | 148.40          |               |                |              | 30.99          |              |         |                 |                |        |
| 12             | 19.35           | •             |                |              | 21.74          |              |         |                 |                |        |
| 14             | 19.93           |               | 1.17           |              | 28.59          |              |         |                 |                |        |
| 15             | 21,06           |               |                |              | 27.85          |              |         |                 |                |        |
| 16             | 21.82           |               |                |              | 27.43          | · · · · ·    |         |                 |                |        |
| 18             | 22.52           |               |                |              | 26.45          |              |         |                 |                |        |
| 20             | 23.01           |               |                |              | 25.23          |              |         |                 |                |        |
| 25             | 24.07           |               |                |              | 23.43          |              |         |                 |                |        |
| 30             | 25.38           |               |                |              | 21.73          |              |         |                 |                |        |
| 35             | 26.57           |               |                |              |                |              |         |                 |                |        |
| 40             | 27.49           |               |                |              | 19.01          |              |         |                 |                |        |
| 45             | 28.46           |               |                |              |                |              |         |                 |                |        |
| 50             | 29.26           |               |                |              | 17.28          |              |         |                 |                |        |
| 55             | 10.00           |               |                |              |                |              |         |                 |                |        |
| 60             | 30.48           |               |                |              | 15.81          |              |         |                 |                |        |
|                | 50.10           |               |                |              |                |              |         |                 |                |        |
|                |                 |               |                |              |                |              |         |                 |                |        |
| Drawdov        | wn @ 60         | Minutes       |                |              |                |              |         |                 |                |        |
| Recover        | y @ 60          | Minutes       |                | 1            |                | 1            |         |                 |                |        |
| Comme          | its             |               |                |              |                |              |         | Page            | 1/Z            |        |

6891 SR7W, Mt Forest, Ont. N0G 2L0

519-501-4750 MOE Lic. 7719

| MOE Au   | dit No.  | 236597        | 7) Well          | Tag No.  | A 335          | 252   | 1 0                      | ti o    | Il a Inda   | Luents |  |
|----------|----------|---------------|------------------|----------|----------------|---|--------------------------|---------|-------------|--------|--|
| Date j   | uly 12   | 16001         | Client           | Crozier  | + Ass          | ociates   | - Je li                  | Ila - V | Ttl Doth    | Datum  |  |
| Well #   | Static   | Pumping       | Rate             | Intke At | Amnt/          | Casing  | Amnus                    | bcreen  | To Grade    | Top of |  |
| 2        |          |               | IGPM             |          | 1              |   | Open                     | Hole    |             | Casing |  |
| Elapsd   | Wate     | er Level      | Draw             | Down     | Reco           | overy   | Remarks<br>Rock starts @ |         |             |        |  |
| Time     | Meters   | Feet          | Meters           | Feet     | Meters         | Feet  |                          |         |             |        |  |
| ¢        | 90 m:n   | 33.04m        |                  |          |                | Marine Contraction  |                          |         |             |        |  |
| 1        | 120      | 34.47         |                  |          |                |   |                          |         |             | 115    |  |
| 2        | 150      | 35.41         |                  |          | 200            | And the second se |                          |         |             |        |  |
| 3        | 180      | 36,08         | -                |          |                |   |                          |         | 180.<br>190 | 100    |  |
| 4        | 210      | 36.57         |                  |          |                |   |                          | and the |             |        |  |
| 5        | 210      | 36.94         |                  |          |                |   |                          |         |             |        |  |
| 6        | 270      | 37.52         |                  |          |                |   |                          |         |             |        |  |
| 1        | 300      | 38.95         |                  |          | and the second |   |                          |         |             |        |  |
| 8        | 330      | 38.95         |                  |          |                |   |                          |         |             |        |  |
| 9        | 360      | 38.95         |                  |          |                |   |                          |         |             |        |  |
| 10       |          | · · · · · · · |                  |          |                |   |                          |         |             |        |  |
| 12       |          |               | ALL STREET       |          |                | 1.  |                          |         | -           |        |  |
| 14       | 1.       |               |                  |          |                |   |                          |         |             |        |  |
| 15       | 1.000    | 100           | and the second   |          |                |   |                          |         |             |        |  |
| 16       |          | -             |                  |          |                |   | Stand Street             | Marine. |             |        |  |
| 18       |          | 12. 3         |                  |          |                |   |                          | <u></u> | As a second |        |  |
| 20       |          | 1             |                  |          |                |   | 1.00                     | 2       |             |        |  |
| 25       |          | 1933409       |                  |          |                |   |                          |         |             |        |  |
| 30       |          |               | 10-10            |          |                | and the second  |                          |         |             |        |  |
| 35       |          |               | -                |          |                |   |                          |         |             |        |  |
| 40       | 1        |               | -                |          |                |   |                          |         |             |        |  |
| 45       |          |               | 1949 (1998)<br>1 |          |                |   |                          |         |             |        |  |
| 50       | 140      |               | 1.200            |          |                |   |                          |         |             |        |  |
| 55       |          | 1002          |                  |          |                |   |                          |         | <u> </u>    |        |  |
| 60       |          | 1.1.1         | 1                | -        |                |   |                          |         |             |        |  |
|          |          | - There -     | -                |          |                |   |                          |         |             |        |  |
|          | <u> </u> |               |                  |          |                |   |                          |         |             |        |  |
| Drawdow  | vn @ 60  | Minutes       |                  |          |                |   |                          |         |             |        |  |
| Recovery | / @ 60   | winutes       |                  |          |                |   |                          |         | ,           |        |  |
| Commen   | 15       | 1.6           |                  |          | 1.1            |   |                          | Page    | Z/2         |        |  |

6891 SR7W, Mt Forest, Ont. N0G 2L0

519-501-4750 MOE Lic. 7719

| MOE Au  | dit No. | 2365965     | Well        | Tag No.     | A299-       | 193          |         | 2.0      | Plla laur | streats |
|---------|---------|-------------|-------------|-------------|-------------|--------------|---------|----------|-----------|---------|
| Date A  | 1917,   | 202         | Client      | Crozier     | - Assoc     | - Associates |         | creen    | Ttl Dpth  | Datum   |
| Well #  | Static  | Pumping     | Rate        | Intke At    | Amnt/C      | Jasing       | Annos   | 010011   | To Grade  | Top of  |
| 3       | 15:54m  | 3           | IGPM        | IGPM 30.48m |             |              |         | Hole     | arke      | Casing  |
| Elapsd  | Wate    | er Level    | I Draw Down |             | Reco        | very         | Remarks |          |           |         |
| Time    | Meters  | Feet        | Meters      | Feet        | Meters Feet |              |         | OCK Star | w e       |         |
| 0       | 9       | - Distantes |             |             |             |              |         |          |           |         |
| 1       | 16.41   | 10.47       |             |             | 18.56       |              |         |          |           |         |
| 2       | 16.71   | 10.78       |             |             | 18.12       |              |         |          |           |         |
| 3       | 16.96   | 10.70       |             |             | 17.76       |              |         |          |           |         |
| 4       | M.15    | . Aller     |             |             | 17.42       |              |         |          |           |         |
| 5       | 17.33   | 10.5        |             |             | 17.16       |              |         |          |           |         |
| 6       | 17.48   | 1.00        |             |             | 16.94       |              |         |          |           |         |
| 7       | 17.6    | 19.00       |             |             | 16.74       |              |         |          |           |         |
| 8       | 17.72   | 12.00       |             |             | 16.58       |              |         |          |           |         |
| 9       | 17.83   | 1.0.01      |             |             | 16.40       |              |         |          |           |         |
| 10      | 17.92   |             |             |             | 16.27       |              |         |          |           |         |
| 12      | 18.07   |             |             |             | 16.03       |              |         |          |           |         |
| 14      | 18.00   |             |             |             | 15.87       |              |         |          |           |         |
| 15      | 18.08   |             |             |             | 15.79       |              |         |          |           |         |
| 16      | 18.0    | 1           |             |             | 15.73       |              |         |          |           |         |
| 18      | 18.18   |             |             |             | 15.64       |              |         |          |           |         |
| 20      | 18.25   | -           |             |             | 15.55       |              |         |          |           |         |
| 25      | 18.40   |             |             |             | 15.54       |              |         |          |           |         |
| 30      | 18.49   |             |             |             |             |              |         |          |           |         |
| 35      |         |             |             |             |             |              |         |          |           |         |
| 40      | 18.56   |             |             |             |             |              |         |          |           |         |
| 45      |         |             |             |             |             |              |         |          |           |         |
| 50      | 18.58   | 3           |             |             |             |              |         |          |           |         |
| 55      |         |             |             |             |             |              |         |          |           |         |
| 60      | 18.64   |             |             |             |             |              |         |          |           |         |
|         |         |             |             |             |             |              |         |          |           |         |
| Desuit  |         | Minutos     |             |             |             |              |         |          |           |         |
| Recover |         | ) Minutes   | 1           |             | 1           |              |         |          |           |         |
| Commen  | its     | , minutos   |             |             | <u></u>     | <u></u>      |         | Page     | 1/2       |         |
|         |         |             |             |             |             |              |         | inge     |           |         |

#### 6891 SR7W, Mt Forest, Ont. N0G 2L0

519-501-4750 MOE Lic. 7719

| MOE Au  | dit No. |  | Well           | Tag No.   | A29979                                   | 3            |                                       |           |              |  |
|---------|---------|--|----------------|---|--|--------------|---------------------------------------|-----------|--------------|--|
| Date    |         |  | Client         |   |  |              |                                       |           | Ind D. dt    | Detum  |
| Nell #  | Static  | Pumping  | Rate           | Intke At  | Amnt/Casing                              |              | Amnt/S                                | Screen    | To Grade     | Top of   |
|         |         |  | IGPM           |   |  |              | Open                                  | Hole      | 10 0.000     | Casing   |
| Elapsd  | Wate    | er Level   | Draw           | Down  | Reco                                     | overy        |                                       | Ren       | narks        |  |
| Time    | Meters  | Feet   | Meters         | Feet  | Meters Feet                              |              | Rock starts @ '                       |           |              |  |
| ø       | 90 min  | 18.64m   |                |   |  | 2000         |                                       |           |              |  |
| 1       | 120     | 18.67  |                |   |  |              | 1                                     |           |              |  |
| 2       | 150     | 18.74  |                |   |  |              | 1                                     |           |              | Marine -   |
| 3       | 180     | 18.79  |                |   | 1  |              | 1 and anno                            |           |              |  |
| 4       | 210     | 18.86  |                | (209) - C.S.  |  |              | Sec. Sec.                             | 1         |              |  |
| 5       | 240     | 18.91  |                |   |  |              | 1                                     |           | - din s      | - Martine -  |
| 6       | 270     | 18.97  |                |   |  |              |                                       | Sec. 1    |              |  |
| 1       | 300     | 19.00  |                | Contraction of  |  |              |                                       |           |              |  |
| 8       | 330     | 19.04  |                |   |  |              |                                       |           |              |  |
| 9       | 360     | 19.01  | 1999           | No. of the second se |  |              |                                       |           | A Carlot     |  |
| 10      |         |  |                | all and   | and the second                           |              |                                       |           | 111          |  |
| 12      |         |  | 1.1            |   |  | Sec. States  |                                       | 1000      |              |  |
| 14      | ALA     | Stead  |                |   | ALL STAN                                 | Sugar States | Col                                   |           | Al ma        |  |
| 15      |         | The state of the s | and stepped    |   | and the second                           | A            |                                       |           |              |  |
| 16      |         |  | 1              |   | The second                               | -            | Contra La Contra                      |           |              | <u>k </u>  |
| 18      |         |  |                | a market and  | The second second                        |              |                                       |           |              |  |
| 20      | Rect    |  |                |   |  | 199          | a martine                             |           |              |  |
| 25      | 1       |  | 1.45 - 17      | all De  | Sec. 2                                   |              | (                                     |           | Section 2    |  |
| 30      |         |  |                | 1 martin  | Concernance -                            |              | A                                     | Sec.      | A CONTRACTOR | and the second sec |
| 35      |         | ···  | 1000 Barris    | Taki Inda   | a second                                 | 11 61        | · · · · · · · · · · · · · · · · · · · |           |              |  |
| 40      |         |  |                | 1 1   |  | 1 Maple      | 1 24                                  |           |              |  |
| 45      |         |  | and strains    | · San Sill  |  | A Carlos     |                                       |           |              |  |
| 50      |         |  |                |   | 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1 |              | al che                                |           |              |  |
| 55      |         |  | -              |   | a state of the                           | 1            |                                       |           |              |  |
| 60      |         |  | C. Section and | Managari -  |  |              | ille -                                |           |              |  |
|         |         |  | 1. C. L. L.    |   |  |              |                                       | - Wasseld |              |  |
|         | 1       |  |                |   |  |              | C Theorem                             |           |              |  |
| Drawdow | /n @ 60 | Minutes  | 1              |   |  |              |                                       |           |              |  |
| Recover | @ 60    | Minutes  |                |   |  | 1            |                                       |           |              |  |
| Commen  | ts      |  |                |   |  |              |                                       | Pa        | ge $2/i$     | 2  |

## 6891 SR7W, Mt Forest, Ont. N0G 2L0

519-501-4750 MOE Lic. 7719

| MOE Au         | dit No.        | 2365964          | Well           | Tag No.        | A29917         | 69           |                          |                |                       |   |
|----------------|----------------|------------------|----------------|----------------|----------------|--------------|--------------------------|----------------|-----------------------|---|
| Date S         | ept 6/         | 21               | Client (       | rozier +       | Associates - 1 |              | pe Pilla                 | ts hc          |                       |   |
| Well #         | Static         | Pumping          | Rate           | Intke At       | Amnt/0         | Amnt/Casing  |                          | Screen         | Ttl Dpth              | Datum   |
| 4              | 12.6m          | 5                | IGPM           | 42.67m         |                |              |                          | Hole           | To Grade              | Casing  |
| Elapsd<br>Time | Wate<br>Meters | er Level<br>Feet | Draw<br>Meters | / Down<br>Feet | Reco<br>Meters | very<br>Feet | Remarks<br>Rock starts @ |                |                       |   |
| 0              | 1              | Carlo Mar        |                |                | 16.18 m        |              |                          |                |                       |   |
| 1              | 13.47          |                  |                |                | 15.36          |              |                          |                |                       |   |
| 2              | 14.02          | 1 11.12          |                |                | 14.69          |              |                          |                |                       |   |
| 3              | 14.44          | 1. A.            |                |                | 14.17          |              |                          |                |                       | and the second  |
| 4              | 14.78          | 1.00             |                |                | 13.80          |              |                          | and the second |                       |   |
| 5              | 15.05          | 1. 14. 11        |                |                | 13.53          |              |                          |                | and the first start   | and an enter  |
| 6              | 15.24          | 1                |                |                | 13.31          |              |                          |                |                       | and the local   |
| 7              | 15.45          |                  |                |                | 13.16          |              |                          |                |                       |   |
| 8              | 15.54          | 1                |                |                | 13.04          |              |                          |                |                       | na seconda da seconda s<br>En esta da seconda da se |
| 9              | 15.60          |                  |                |                | 12.98          |              |                          |                | Second Second         | ter alagin ta in  |
| 10             | 15.69          |                  |                |                | 12.92          |              |                          |                |                       | and the second  |
| 12             | 15.70          |                  |                | T              | 12.86          | 1            | 1                        |                | and the second second | Same and Same   |
| 14             | 15.77          |                  | Maria and      |                | 12.80          |              |                          |                |                       | -   |
| 15             | 15.83          |                  |                |                | 12.77          |              | 1. Summer                |                |                       |   |
| 16             | 15.92          |                  |                | 1              | 12.74          |              | L                        | a labela in    | e                     | and stores  |
| 18             | 16.04          | T                | 1              | 1              | 12.67          |              |                          |                |                       |   |
| 20             | 16.18          |                  |                |                | 12.61          |              |                          |                | ni ali strict menti   |   |
| 25             | 16.18          |                  |                |                |                |              |                          |                |                       |   |
| 30             | 16.18          |                  |                |                |                |              |                          |                |                       |   |
| 35             | -              |                  |                |                |                |              |                          |                |                       | Na santa  |
| 40             | 16.18          |                  |                |                |                |              | 1                        |                |                       | - and the store   |
| 45             |                |                  |                |                |                |              |                          |                |                       |   |
| 50             | 16.18          |                  |                |                |                |              |                          |                |                       | -   |
| 55             | 10.10          |                  |                |                |                |              |                          |                |                       |   |
| 60             | 16.18          |                  |                |                |                |              |                          |                |                       | n constantia  |
| Drawdow        | n @ 60         | Minutes          |                | 1              |                |              |                          |                |                       |   |
| Recovery       | @ 60           | Minutes          |                |                |                |              | 1.1                      |                | Concertor a concerto  |   |
| Comment        | S              |                  |                |                |                |              |                          | Page           | 1/2                   |   |

6891 SR7W, Mt Forest, Ont. N0G 2L0 519-501-4750 MOE Lic. 7719

| MOE Au         | dit No.           | 2365964          | Well           | Tag No.      | A29978                  | 9                            |                          |  | 7 . (    | ,       |
|----------------|-------------------|------------------|----------------|--------------|-------------------------|------------------------------|--------------------------|--|----------|---------|
| Date Se        | Sept. 6/21 Client |                  |                | sozier 4     | tes - Joe               | Pilla - Pilla hvestments hc. |                          |  |          |         |
| Well #         | Static            | Pumping          | Rate           | Intke At     | Amnt/Casing             |                              | Amnt/S                   | creen  | To Grade | Top of  |
| 4              | DUM               | 5                | IGPM           | 42.67m       |                         |                              | Open                     | Hole   | 10 01000 | Casing  |
| Elapsd<br>Time | Wate<br>Meters    | er Level<br>Feet | Draw<br>Meters | Down<br>Feet | Recovery<br>Meters Feet |                              | Remarks<br>Rock starts @ |  |          |         |
| ò              | 90 min            | 16.1Bm           |                |              |                         |                              |                          |  |          |         |
| 1              | 20                | 16.18            |                |              |                         |                              |                          | State of the second  |          |         |
| 2              | 150               | 16.18            |                |              |                         |                              |                          |  |          |         |
| 3              | 190               | 16.18            |                |              |                         |                              |                          |  |          |         |
| 4              | 210               | 16.18            |                |              |                         |                              |                          |  |          |         |
| 5              | 240               | 16.18            |                |              |                         |                              |                          |  |          |         |
| 6              | 270               | 16.18            |                |              |                         |                              |                          |  |          |         |
| 7              | 300               | 16.18            |                |              |                         |                              |                          |  |          |         |
| 8              | 330               | 16-18            |                |              |                         |                              |                          |  |          |         |
| 9              | 360               | 16.18            |                |              |                         |                              |                          |  |          |         |
| 10             |                   |                  | Here.          |              |                         |                              |                          |  |          |         |
| 12             |                   |                  |                | •            |                         |                              |                          |  |          |         |
| 14             |                   | and the second   | and the        |              |                         |                              |                          | de la companya de la |          | <u></u> |
| 15             |                   | 10 M             | 1              | 6            |                         |                              |                          |  |          |         |
| 16             |                   |                  |                |              | P.                      |                              | <u></u>                  |  |          |         |
| 18             |                   |                  |                | 4            |                         |                              |                          |  |          |         |
| 20             |                   |                  |                | Marine and   |                         | 1                            |                          |  |          |         |
| 25             |                   |                  |                |              |                         |                              |                          |  |          |         |
| 30             |                   |                  |                |              |                         |                              |                          |  |          |         |
| 35             |                   | 10.00            |                |              |                         |                              | the second second        |  |          |         |
| 40             |                   |                  |                |              |                         | -                            |                          |  |          |         |
| 45             |                   |                  |                |              | 199                     |                              |                          |  |          |         |
| 50             |                   |                  |                | 10           | a fair                  |                              |                          |  |          |         |
| 55             |                   |                  |                |              |                         |                              |                          |  | <u></u>  |         |
| 60             |                   |                  |                |              |                         |                              |                          |  |          |         |
|                |                   |                  |                |              |                         |                              |                          |  |          |         |
| rawdown        | @ 60              | Minutes          |                |              |                         |                              |                          |  |          |         |
| ecovery        | @ 60              | Minutes          |                |              |                         |                              |                          |  |          |         |
| omments        |                   |                  |                |              |                         |                              | P                        | nap a  | 2/2      |         |

6891 SR7W, Mt Forest, Ont. N0G 2L0

519-501-4750 MOE Lic. 7719

| MOE Au   | dit No.        | 236593  | 6 Well | Tag No.                    | Aa       | 1979        | 10      |                             | www.ensections   | and services   | and the second |  |
|----------|----------------|---------|--------|----------------------------|----------|-------------|---------|-----------------------------|--|--|--|--|
| Date 5.  | ept. 61        | 21      | Client | Crozier + Associates - Joe |          |             |         | 2 filla - Pilla Investments |  |  |  |  |
| Well #   | Static         | Pumping | Rate   | Intke At                   | A        | Amnt/Casing |         | Amnt/S                      | Screen   | Ttl Dpth   | Datum  |  |
| 5        | 21.24          | 5       | IGPM   |                            |          |             | Open    | Hole                        | To Grade   | Casing   |  |  |
| Elapsd   | d Water Level  |         | Draw   | Down                       | Recovery |             |         |                             | Ren  | narks  |  |  |
| Time     | Meters         | Feet    | Meters | Feet                       | Met      | ers         | Feet    | Rock starts @               |  |  |  |  |
| 0        |                |         |        |                            |          |             |         |                             |  | المرجع والمرجع والمرجع   | and the second   |  |
| 1        | 21.54          |         |        |                            | 21.      | 24          |         |                             |  | and the second second  | Calence - Second   |  |
| 2        | 21.54          |         |        |                            |          |             |         | man - man                   | -  |  | and the second second  |  |
| 3        | 21.54          |         |        |                            |          | •           |         |                             | Sector and   | and a second   |  |  |
| 4        | 21.54          |         |        |                            |          |             |         |                             |  | Section and  | and the second   |  |
| 5        | 21.54          |         |        |                            |          |             |         |                             | Second Second  |  | and the second   |  |
| 6        | 1              |         |        |                            |          |             |         |                             | ener vi  | Section of the section of the  | and the second   |  |
| 7        |                |         |        |                            |          |             |         |                             |  |  |  |  |
| 8        | and the second |         |        |                            |          |             |         |                             |  | and the second   | and the second second  |  |
| 9        | 1.100          | 131 840 |        |                            |          |             |         |                             | a lane a   |  |  |  |
| 10       |                |         |        |                            |          |             |         |                             |  | Jeline and the   | agenerite areas  |  |
| 12       |                |         |        |                            |          |             |         |                             |  |  | and the second   |  |
| 14       |                |         |        |                            |          |             |         |                             |  |  | - and the second second  |  |
| 15       |                |         | 1      |                            |          |             |         | a second second             |  | and a second second  | - and the second states  |  |
| 16       |                |         |        |                            |          |             |         | 1                           | Same Street of   | and the second second  | an succession and  |  |
| 18       |                |         |        |                            |          |             |         |                             |  |  | and the second   |  |
| 20       |                |         |        |                            |          |             |         | A                           |  |  | -  |  |
| 25       |                |         |        |                            |          |             |         |                             |  |  |  |  |
| 30       |                |         |        |                            |          |             |         |                             |  |  |  |  |
| 35       |                |         |        |                            |          |             |         |                             |  | and the second |  |  |
| 40       |                | 1       |        |                            |          |             | ]       |                             |  |  | an analysis alogo  |  |
| 45       |                |         |        |                            |          |             |         |                             |  | Styles externation   |  |  |
| 50       |                | 1       |        |                            |          |             |         |                             | and the second sec |  | and an inclusion   |  |
| EE       | V              |         |        | 1                          |          |             |         |                             |  |  |  |  |
| 60       | 21,54          | 1       | 100    |                            | 21,      | 24          | lana an |                             |  |  | and the second |  |
|          |                |         |        |                            |          |             | -       |                             |  |  |  |  |
| )rawdown | @ 60           | Minutes | 1.     |                            |          |             | -       |                             | n filmen ihnenen ih  |  |  |  |
| Recovery | @ 60           | Minutes |        |                            |          |             |         |                             | -  |  |  |  |
| comments |                |         |        |                            |          |             |         |                             | Page   | . 1/2  |  |  |

6891 SR7W, Mt Forest, Ont. N0G 2L0

519-501-4750 MOE Lic. 7719

| MOE Au   | dit No.2 | Z36                 | 5936 | Well     | Tag No.    | A299 790 | )             |           |           |           |        |  |
|----------|----------|---------------------|------|----------|------------|----------|---------------|-----------|-----------|-----------|--------|--|
| Date Se  | pt 6/2   | 1                   |      | Client ( | citozier + | Associat | es - Joe      | Pilla - t | rilla hue | Streets 1 | Datum  |  |
| Well #   | Static   | Pum                 | ping | Rate     | Intke At   | Amnt/    | Amnt/Casing   |           | screen    | To Grade  | Top of |  |
| 5        |          |                     | 5    | IGPM     |            |          |               | Open      | Hole      |           | Casing |  |
| Elapsd   | Wate     | er Le               | vel  | Draw     | / Down     | Recovery |               | Remarks   |           |           | .      |  |
| Time     | Meters   | rs Feet Meters Feet |      |          | Meters     | Feet     | Rock starts @ |           |           |           |        |  |
| •        | min      | 21.5                | 54m  | -        |            |          |               |           |           |           |        |  |
|          | 120      |                     |      |          |            |          |               |           |           |           |        |  |
| 2        | 150      |                     |      |          |            |          |               |           |           |           |        |  |
| 3        | 180      |                     |      |          |            |          |               |           |           |           |        |  |
| . 4      | 210      |                     |      |          |            |          |               |           |           |           |        |  |
| 5        | 240      |                     |      |          |            |          |               |           |           |           |        |  |
| 6        | 270      |                     |      |          |            |          |               |           |           |           |        |  |
|          | 300      |                     |      |          |            |          |               |           |           |           |        |  |
| 8        | 330      | 1                   | /    |          |            |          |               |           |           |           |        |  |
| 9        | 360      | 21.                 | 54m  |          |            |          |               |           |           | 100       |        |  |
| 10       |          |                     |      |          |            |          |               |           | <u></u>   |           |        |  |
| 12       |          |                     | -    |          |            |          |               |           |           |           |        |  |
| 14       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 15       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 16       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 18       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 20       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 25       |          |                     |      |          |            |          |               |           | ·         |           |        |  |
| 30       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 35       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 40       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 45       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 50       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 55       |          |                     |      |          |            |          |               |           |           |           |        |  |
| 60       |          |                     |      |          |            |          |               |           |           |           |        |  |
|          |          |                     |      |          |            |          |               |           |           |           |        |  |
|          |          |                     |      |          |            |          |               |           |           |           |        |  |
| Drawdown | @ 60     | Minu                | tes  |          |            |          |               |           |           |           |        |  |
| Recovery | @ 60     | Minu                | tes  |          |            |          |               |           |           |           |        |  |
| Comments | ;        |                     |      |          |            |          |               |           | Pag       | e 2/2     | 2      |  |

# APPENDIX F

Hydrographs











# APPENDIX G

Pumping Test Results











# ${\sf APPENDIX}\ H$

Certificate of Analyses



#### CLIENT NAME: CROZIER & ASSOCIATES 2800 HIGH POINT DRIVE, SUITE 100 MILTON, ON L9T 6P4 905-875-0026 ATTENTION TO: Caitlyn Macphee PROJECT: Alliston Site (1101-4125) AGAT WORK ORDER: 21T812364 MICROBIOLOGY ANALYSIS REVIEWED BY: Nivine Basily, Inorganics Report Writer WATER ANALYSIS REVIEWED BY: Jacky Zhu, Spectroscopy Technician DATE REPORTED: Oct 08, 2021 PAGES (INCLUDING COVER): 7 VERSION\*: 1

Should you require any information regarding this analysis please contact your client services representative at (905) 712-5100

\*Notes

Disclaimer:

- All work conducted herein has been done using accepted standard protocols, and generally accepted practices and methods. AGAT test methods may
  incorporate modifications from the specified reference methods to improve performance.
- All samples will be disposed of within 30 days after receipt unless a Long Term Storage Agreement is signed and returned. Some specialty analysis may be exempt, please contact your Client Project Manager for details.
- AGAT's liability in connection with any delay, performance or non-performance of these services is only to the Client and does not extend to any other third party. Unless expressly agreed otherwise in writing, AGAT's liability is limited to the actual cost of the specific analysis or analyses included in the services.
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- The test results reported herewith relate only to the samples as received by the laboratory.
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  contained in this document.
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|---|--|
| (APEGA)   |  |
| Western Enviro-Agricultural Laboratory Association (WEALA)                    |  |
| Environmental Services Association of Alberta (ESAA)                          |  |

Page 1 of 7

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AGAT WORK ORDER: 21T812364 PROJECT: Alliston Site (1101-4125) 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.aqatlabs.com

#### CLIENT NAME: CROZIER & ASSOCIATES

SAMPLING SITE: Alliston

DATE RECEIVED: 2021-10-06

ATTENTION TO: Caitlyn Macphee

SAMPLED BY:C. MacPhee

| То                 | tal Colifo | rms & E. C | Coli (Using MI Agar) |              |               |
|--------------------|------------|------------|----------------------|--------------|---------------|
|                    |            |            |                      | DATE REPORTE | D: 2021-10-08 |
| AMOLE DECODIDUTON. | T14/4      | T14/0      | 714/0                | T\A/4        | 714/5         |

|                  | SA        | MPLE DES    | CRIPTION:             | TW1                          | TW2                 |     | TW3                 |     | TW4                 | TW5                 | MW1                 |
|------------------|-----------|-------------|-----------------------|------------------------------|---------------------|-----|---------------------|-----|---------------------|---------------------|---------------------|
|                  |           | SAM         | PLE TYPE:             | Water                        | Water               |     | Water               |     | Water               | Water               | Water               |
|                  |           | DATE        | SAMPLED:              | 2021-10-06<br>14:00          | 2021-10-06<br>14:00 |     | 2021-10-05<br>12:00 |     | 2021-10-05<br>09:00 | 2021-10-05<br>14:00 | 2021-10-06<br>14:00 |
| Parameter        | Unit      | G/S         | RDL                   | 3061969                      | 3061978             | RDL | 3061979             | RDL | 3061980             | 3061981             | 3061982             |
| Escherichia coli | CFU/100mL |             | 1                     | ND                           | ND                  | 1   | ND                  | 1   | ND                  | ND                  | ND                  |
| Total Coliforms  | CFU/100mL |             | 1                     | 21                           | 1                   | 100 | 5700                | 1   | 1                   | ND                  | 55                  |
|                  | SA        | MPLE DES    | CRIPTION:             | MW2                          |                     |     |                     |     |                     |                     |                     |
|                  |           | SAM<br>DATE | PLE TYPE:<br>SAMPLED: | Water<br>2021-10-06<br>14:00 |                     |     |                     |     |                     |                     |                     |
| Parameter        | Unit      | G/S         | RDL                   | 3061983                      |                     |     |                     |     |                     |                     |                     |
| Escherichia coli | CFU/100mL |             | 1                     | ND                           |                     |     |                     |     |                     |                     |                     |
| Total Coliforms  | CFU/100mL |             | 1                     | 18                           |                     |     |                     |     |                     |                     |                     |

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard

**3061969-3061983** If RDL >1 indicates dilutions of the sample.

ND - Not Detected.

Analysis performed at AGAT Toronto (unless marked by \*)





AGAT WORK ORDER: 21T812364 PROJECT: Alliston Site (1101-4125) 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.aqatlabs.com

#### **CLIENT NAME: CROZIER & ASSOCIATES**

SAMPLING SITE: Alliston

ATTENTION TO: Caitlyn Macphee

SAMPLED BY:C. MacPhee

|                           |      |                           |                                    | ()                                  | Nater) Nitra                        | te, Nitrite                         |                                     |                                     |                                     |                                     |  |
|---------------------------|------|---------------------------|------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|--|
| DATE RECEIVED: 2021-10-06 |      |                           |                                    |                                     |                                     |                                     |                                     | I                                   | DATE REPORT                         | ED: 2021-10-08                      |  |
|                           |      | SAMPLE DES<br>SAM<br>DATE | CRIPTION:<br>PLE TYPE:<br>SAMPLED: | TW1<br>Water<br>2021-10-06<br>14:00 | TW2<br>Water<br>2021-10-06<br>14:00 | TW3<br>Water<br>2021-10-05<br>12:00 | TW4<br>Water<br>2021-10-05<br>09:00 | TW5<br>Water<br>2021-10-05<br>14:00 | MW1<br>Water<br>2021-10-06<br>14:00 | MW2<br>Water<br>2021-10-06<br>14:00 |  |
| Parameter                 | Unit | G/S                       | RDL                                | 3061969                             | 3061978                             | 3061979                             | 3061980                             | 3061981                             | 3061982                             | 3061983                             |  |
| Nitrate as N              | mg/L |                           | 0.05                               | <0.05                               | <0.05                               | <0.05                               | <0.05                               | <0.05                               | 8.57                                | 9.26                                |  |
| Nitrite as N              | mg/L |                           | 0.05                               | <0.05                               | <0.05                               | <0.05                               | <0.05                               | <0.05                               | <0.05                               | 0.26                                |  |

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard

Analysis performed at AGAT Toronto (unless marked by \*)

**Certified By:** 



### **Quality Assurance**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

#### PROJECT: Alliston Site (1101-4125)

#### SAMPLING SITE: Alliston

AGAT WORK ORDER: 21T812364

**ATTENTION TO: Caitlyn Macphee** 

SAMPLED BY:C. MacPhee

### **Microbiology Analysis**

| RPT Date: Oct 08, 2021                    |       | DUPLICATE |        |        |       | REFERENCE MATERIAL |          |             | METHOD         | BLANK    | ( SPIKE              | MATRIX SPIKE |          |                      |       |
|---|-------|-----------|--------|--------|-------|--------------------|----------|-------------|----------------|----------|----------------------|--------------|----------|----------------------|-------|
| PARAMETER                                 | Batch | Sample    | Dup #1 | Dup #2 | 2 RPD | Method<br>Blank    | Measured | Acce<br>Lir | ptable<br>nits | Recoverv | Acceptable<br>Limits |              | Recoverv | Acceptable<br>Limits |       |
|   |       | ld        |        |        |       |                    | Value    | Lower       | Upper          |          | Lower                | Upper        | <b>,</b> | Lower                | Upper |
| Total Coliforms & E. Coli (Using MI Agar) |       |           |        |        |       |                    |          |             |                |          |                      |              |          |                      |       |

| Escherichia coli | 3061969 3061969 | ND | ND | NA   | < 1 |
|------------------|-----------------|----|----|------|-----|
| Total Coliforms  | 3061969 3061969 | 21 | 20 | 4.9% | < 1 |

Comments: ND - Not Detected, NA - % RPD Not Applicable.





**AGAT** QUALITY ASSURANCE REPORT (V1)

Page 4 of 7

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### **Quality Assurance**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

#### PROJECT: Alliston Site (1101-4125)

#### AGAT WORK ORDER: 21T812364 ATTENTION TO: Caitlyn Macphee

SAMPLING SITE: Alliston

SAMPLED BY:C. MacPhee

### Water Analysis

| RPT Date: Oct 08, 2021   |         |        | D      | UPLICAT | E    |                 | REFEREN  | ICE MA               | TERIAL | METHOD   | BLANK       |                | MAT      | RIX SPI     | KE             |
|--------------------------|---------|--------|--------|---------|------|-----------------|----------|----------------------|--------|----------|-------------|----------------|----------|-------------|----------------|
| PARAMETER                | Batch   | Sample | Dup #1 | Dup #2  | RPD  | Method<br>Blank | Measured | Acceptable<br>Limits |        | Recoverv | Acce<br>Lir | ptable<br>nits | Recoverv | Acce<br>Lir | ptable<br>nits |
|                          |         | Id     |        |         |      |                 | value    | Lower                | Upper  |          | Lower       | Upper          |          | Lower       | Upper          |
| (Water) Nitrate, Nitrite |         |        |        |         |      |                 |          |                      |        |          |             |                |          |             |                |
| Nitrate as N             | 3061743 |        | 1.47   | 1.52    | 3.3% | < 0.05          | 101%     | 70%                  | 130%   | 108%     | 80%         | 120%           | 107%     | 70%         | 130%           |
| Nitrite as N             | 3061743 |        | <0.05  | <0.05   | NA   | < 0.05          | 108%     | 70%                  | 130%   | 108%     | 80%         | 120%           | 111%     | 70%         | 130%           |

Comments: NA Signifies Not Applicable.

Duplicate NA: results are less than 5X the RDL and RPD will not be calculated.





#### **AGAT** QUALITY ASSURANCE REPORT (V1)

Page 5 of 7

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# **Method Summary**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

#### PROJECT: Alliston Site (1101-4125)

SAMPLING SITE: Alliston

#### AGAT WORK ORDER: 21T812364

**ATTENTION TO: Caitlyn Macphee** 

#### SAMPLED BY:C. MacPhee

| PARAMETER             | AGAT S.O.P   | LITERATURE REFERENCE    | ANALYTICAL TECHNIQUE |
|-----------------------|--------------|-------------------------|----------------------|
| Microbiology Analysis |              |                         |                      |
| Escherichia coli      | MIC-93-7010  | EPA 1604                | Membrane Filtration  |
| Total Coliforms       | MIC-93-7010  | EPA 1604                | Membrane Filtration  |
| Water Analysis        |              |                         |                      |
| Nitrate as N          | INOR-93-6004 | modified from SM 4110 B | ION CHROMATOGRAPH    |
| Nitrite as N          | INOR-93-6004 | SM 4110 B               | ION CHROMATOGRAPH    |

| A G G  |  | La  | bora  | torie  | mi-bi<br>es <sup>p</sup>  | Mi<br>h: 905.71                        | 5<br>ssissau<br>2 5100<br>we                      | 835 (<br>iga, O<br>) Fax:<br>beart  | Coopers<br>ntario l<br>905.71<br>h.agatla                          | Aven<br>_4Z 1<br>_2.51<br>abs.co    | ue<br>Y2<br>22<br>om | Labora<br>Work Orde<br>Cooler Qua  | r #:  |   | Dnly<br>T  | 81  | 2:18  | 36   | 4   |  |
|--|--|---|---|--|---|--|---|---|--|-------------------------------------|----------------------|--|---|---|--|---|---|--|---|--|
| Report Information:         Company:       CF.Crozie         Contact:       Caitlyn         Address:       2800 hic         Milton,       Milton,         Phone:       905.87         Reports to be sent to:       1. Email:         2. Email:       Concepted         Project Information:       Project:         Site Location:       Alliston | u ir this is a<br>yacphi<br>h poi<br>on!<br>6506x7<br>e@ cfcrc<br>Site (1)   | Drinking Water  | tes<br>ve<br>100  | se use Drini                                   | king Water Chain of Custody Form (pot.         gulatory Requirements:         echeck all applicable boxes)         agulation 153/04         bleindicate One         jInd/Com         iIndicate One         jInd/Com         iIndicate One         jInd/Com         iIndicate One         jInd/Com         iIndicate One         jInd/Com         iCoarse         iFine         this submission for a cord of Site Condition?         Yes       X No | R406   <br>ne   <br>58   <br>Cer       | Sew<br>Sew<br>Prov<br>Obje<br>Othe<br>Port<br>Yes | d by h<br>eer Us<br>anitary<br><i>Regio</i><br>. Wat<br>ective:<br>er<br><i>Indica</i> t<br><b>Guid</b> | e Stu<br>n<br>er Qualiti<br>s (PWQC<br>s (PWQC<br>e One<br>f Analy | orm<br>(y<br>))<br>on<br>ysis<br>No |                      | Custody Se<br>Notes:<br>Turnarou<br>Regular 1<br>Rush TAT<br>Day<br>OR<br>*TAT | eal Intac<br>und T<br>TAT<br>(Rush Sur<br>Usiness<br>ys<br>Date R<br>Please<br>T is excl<br>ne Day' | ct:<br><b>Freine</b><br>recharges<br>a<br>provid<br>usive c<br>analy: | (TAT)<br>(TAT)<br>5 t<br>Apply)<br>2 Da<br>ed (Rus<br>e prior<br>of week<br>sis, ple | i Req<br>i Req<br>i Req<br>i o 7 Bu:<br>Busine:<br>ays<br>h Surch<br>notifica<br>kends a<br>sase co | uired<br>siness<br>ss<br>harges<br>ation fo<br>and stat | Vo<br>I:<br>Days<br>Days<br>May Ap<br>or rush<br>tutory F<br>your AG | ext Busin<br>ay<br>pply):<br>TAT<br>nolidays<br>rAT CPM | ess  |
| AGAT Quote #:<br>Please note: If quotation number<br>Invoice Information:<br>Company:<br>Contact:<br>Address:<br>Email:<br>Email:  | PO:<br>is not provided, cilent will<br>B<br>icr + O:<br>Icr + O:<br>Icr + O:<br>Icr + O:<br>Cr + O | be billed full price for<br>ill To Same: Ye<br>SSOCOC   | analysis<br>as No D<br>ates<br>ngwccc   | Sam<br>B<br>GW<br>O<br>P<br>S<br>SD<br>SW      | nple Matrix Legend<br>Biota<br>Ground Water<br>Oil<br>Paint<br>Soil<br>Sediment<br>Surface Water  | Field Filtered - Metals, Hg, CrVI, DOC | k Inorganics                                      | Reg 11<br>- CrVI, CHg, CHWSB  | F1-F4 PHCs 8   |                                     |                      | Disposal Characterization TCLP: 019  | Soils Characterization Package  | EC/SAR  | Coli   | tal Colitoring  |   |  |   | ally Hazardous or High Concentration (Y/N) |
| Sample Identification<br>TW1<br>TW2<br>TW3<br>TW4<br>TW5<br>MW1<br>MW2   | Date<br>Sampled  | Time<br>Sampled<br>200 (**<br>200 (**)))))))))))))))))))))))))))))))))) | # of<br>Containers<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3<br>3 | Sample<br>Matrix<br>GW<br>GW<br>GW<br>GW<br>GW | Comments/<br>Special Instructions   | ZZZZZ                                  | Metal   | Metal   | BTEX   | PAHS                                |                      | Landfill<br>TCP: C<br>Excess   | Excess  | Salt -  | CCCCCCF.   |   |   |  | 5:4   | Potenti                                    |
| Samples Relinquished By (Print Name and Sign): Samples Relinquished By (Print Name and Sign): Samples Relinquished By (Print Name and Sign): Decompart (IV) DB/128-4614-002  | A  | Date<br>Date<br>Date<br>Date  | Time<br>Time<br>Time<br>Time  | :35  | Samples Received By (Print Name and Sign):<br>Samples Received By (Print Name and Sign):<br>Samples Received By (Print Name and Sign):  | )                                      | 2   | Z   | Pink Cor   |                                     | Date<br>Date         | Time<br>Time<br>Time   | CAT L   | White   | Nº: <b>T</b>   | Page  | 1   | _ of<br>15   |   | 121  |



#### CLIENT NAME: CROZIER & ASSOCIATES 2800 HIGH POINT DRIVE, SUITE 100 MILTON, ON L9T 6P4 905-875-0026 ATTENTION TO: Caitlyn Macphee PROJECT: Alliston (1101-4125) AGAT WORK ORDER: 21T798235 MICROBIOLOGY ANALYSIS REVIEWED BY: Nivine Basily, Inorganics Report Writer WATER ANALYSIS REVIEWED BY: Nivine Basily, Inorganics Report Writer DATE REPORTED: Sep 14, 2021 PAGES (INCLUDING COVER): 13 VERSION\*: 1

Should you require any information regarding this analysis please contact your client services representative at (905) 712-5100

\*Notes

Disclaimer:

- All work conducted herein has been done using accepted standard protocols, and generally accepted practices and methods. AGAT test methods may
  incorporate modifications from the specified reference methods to improve performance.
- All samples will be disposed of within 30 days after receipt unless a Long Term Storage Agreement is signed and returned. Some specialty analysis may be exempt, please contact your Client Project Manager for details.
- AGAT's liability in connection with any delay, performance or non-performance of these services is only to the Client and does not extend to any other third party. Unless expressly agreed otherwise in writing, AGAT's liability is limited to the actual cost of the specific analysis or analyses included in the services.
- This Certificate shall not be reproduced except in full, without the written approval of the laboratory.
- The test results reported herewith relate only to the samples as received by the laboratory.
- Application of guidelines is provided "as is" without warranty of any kind, either expressed or implied, including, but not limited to, warranties of
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  contained in this document.
- All reportable information as specified by ISO/IEC 17025:2017 is available from AGAT Laboratories upon request.

**AGAT** Laboratories (V1)

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|---|--|
| (APEGA)   |  |
| Western Enviro-Agricultural Laboratory Association (WEALA)                    |  |

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AGAT WORK ORDER: 21T798235 PROJECT: Alliston (1101-4125) 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.aqatlabs.com

#### CLIENT NAME: CROZIER & ASSOCIATES

#### SAMPLING SITE: Alliston

#### ATTENTION TO: Caitlyn Macphee

SAMPLED BY:C. MacPhee

| DATE RECEIVED: 2021-09-07 |           |          |           |                     |                     |     |                     |     | DATE REPORT         | ED: 2021-09-14      |  |
|---------------------------|-----------|----------|-----------|---------------------|---------------------|-----|---------------------|-----|---------------------|---------------------|--|
|                           | SA        | MPLE DES | CRIPTION: | T1                  | T2                  |     | T3                  |     | T4                  | T5                  |  |
|                           |           | SAM      | PLE TYPE: | Water               | Water               |     | Water               |     | Water               | Water               |  |
|                           |           | DATE     | SAMPLED:  | 2021-09-07<br>15:01 | 2021-09-07<br>15:30 |     | 2021-09-07<br>11:00 |     | 2021-09-07<br>12:00 | 2021-09-07<br>13:00 |  |
| Parameter                 | Unit      | G/S      | RDL       | 2940146             | 2940154             | RDL | 2940155             | RDL | 2940156             | 2940157             |  |
| Escherichia coli          | CFU/100mL |          | 1         | ND                  | 13                  | 1   | ND                  | 1   | ND                  | ND                  |  |
| Total Coliforms           | CFU/100mL |          | 1         | 2                   | 41                  | 100 | 1500                | 1   | 2                   | 22                  |  |

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard

2940146 ND - Not Detected.

2940155 ND - Not Detected.

RDL >1 indicates dilutions of the sample.

2940156-2940157 ND - Not Detected.

Analysis performed at AGAT Toronto (unless marked by \*)



**Certified By:** 



AGAT WORK ORDER: 21T798235 PROJECT: Alliston (1101-4125) 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.aqatlabs.com

#### CLIENT NAME: CROZIER & ASSOCIATES

SAMPLING SITE: Alliston

ATTENTION TO: Caitlyn Macphee

SAMPLED BY:C. MacPhee

| Anion Scan                |                    |                       |                     |                     |                     |                     |                           |  |  |  |  |  |
|---------------------------|--------------------|-----------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|--|--|--|--|--|
| DATE RECEIVED: 2021-09-07 |                    |                       |                     |                     |                     |                     | DATE REPORTED: 2021-09-14 |  |  |  |  |  |
|                           | SAMPLE DESCRIPTION | : T1                  | T2                  | Т3                  | T4                  | Т5                  |                           |  |  |  |  |  |
|                           | SAMPLE TYPE        | : Water               | Water               | Water               | Water               | Water               |                           |  |  |  |  |  |
|                           | DATE SAMPLED       | : 2021-09-07<br>15:01 | 2021-09-07<br>15:30 | 2021-09-07<br>11:00 | 2021-09-07<br>12:00 | 2021-09-07<br>13:00 |                           |  |  |  |  |  |
| Parameter Unit            | G/S RDL            | 2940146               | 2940154             | 2940155             | 2940156             | 2940157             |                           |  |  |  |  |  |
| Fluoride mg/L             | 0.05               | 0.38                  | <0.05               | 0.27                | <0.05               | 0.17                |                           |  |  |  |  |  |
| Chloride mg/L             | 0.10               | 15.9                  | 19.2                | 42.2                | 19.1                | 14.2                |                           |  |  |  |  |  |
| Nitrate as N mg/L         | 0.05               | <0.05                 | <0.05               | < 0.05              | <0.05               | <0.05               |                           |  |  |  |  |  |
| Nitrite as N mg/L         | 0.05               | <0.05                 | <0.05               | < 0.05              | <0.05               | <0.05               |                           |  |  |  |  |  |
| Bromide mg/L              | 0.05               | <0.05                 | 0.22                | 0.48                | <0.05               | <0.05               |                           |  |  |  |  |  |
| Sulphate mg/L             | 0.10               | 1.72                  | 0.31                | 3.39                | 0.32                | 3.74                |                           |  |  |  |  |  |
| Phosphate as P mg/L       | 0.10               | <0.10                 | <0.10               | <0.10               | <0.10               | <0.10               |                           |  |  |  |  |  |

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard

Analysis performed at AGAT Toronto (unless marked by \*)



**Certified By:** 

Basil



AGAT WORK ORDER: 21T798235 PROJECT: Alliston (1101-4125) 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.aqatlabs.com

#### **CLIENT NAME: CROZIER & ASSOCIATES**

SAMPLING SITE: Alliston

#### ATTENTION TO: Caitlyn Macphee

SAMPLED BY:C. MacPhee

| DATE RECEIVED: 2021-09-07 |      |            |            |                     |                     |                     |                     |                     | DATE REPORTED: 2021-09-14 |
|---------------------------|------|------------|------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------------|
|                           |      | SAMPLE DES | CRIPTION:  | T1                  | T2                  | Т3                  | T4                  | Т5                  |                           |
|                           |      | SAM        | IPLE TYPE: | Water               | Water               | Water               | Water               | Water               |                           |
|                           |      | DATE       | SAMPLED:   | 2021-09-07<br>15:01 | 2021-09-07<br>15:30 | 2021-09-07<br>11:00 | 2021-09-07<br>12:00 | 2021-09-07<br>13:00 |                           |
| Parameter                 | Unit | G/S        | RDL        | 2940146             | 2940154             | 2940155             | 2940156             | 2940157             |                           |
| Total Calcium             | mg/L |            | 0.16       | 33.0                | 12.8                | 9.09                | 39.4                | 176                 |                           |
| Total Magnesium           | mg/L |            | 0.17       | 19.3                | 16.7                | 5.95                | 19.9                | 25.0                |                           |
| Total Potassium           | mg/L |            | 0.58       | 1.88                | 1.67                | 1.59                | 1.66                | 2.72                |                           |
| Total Sodium              | mg/L |            | 0.22       | 62.3                | 31.5                | 92.7                | 19.7                | 24.5                |                           |
|                           |      |            |            |                     |                     |                     |                     |                     |                           |

Cations in Water - Total (mg/L)

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard

**2940146-2940157** Dilution required, RDL has been increased accordingly.

Analysis performed at AGAT Toronto (unless marked by \*)





AGAT WORK ORDER: 21T798235 PROJECT: Alliston (1101-4125)

5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.agatlabs.com

#### **CLIENT NAME: CROZIER & ASSOCIATES**

**SAMPLING SITE: Alliston** 

#### **ATTENTION TO: Caitlyn Macphee**

SAMPLED BY:C. MacPhee

|                           | Total Metals in water (mg/L) |   |   |   |                                       |                                      |                                    |                           |  |  |
|---------------------------|------------------------------|---|---|---|---------------------------------------|--------------------------------------|------------------------------------|---------------------------|--|--|
| DATE RECEIVED: 2021-09-07 |                              |   |   |   |                                       |                                      |                                    | DATE REPORTED: 2021-09-14 |  |  |
|                           |                              | SAMPLE DESCRIPT<br>SAMPLE T<br>DATE SAMPI | ION: T1<br>(PE: Wat<br>_ED: 2021-0<br>_15:( | T2<br>er Water<br>19-07 2021-09-0<br>11 15:30 | T3<br>Water<br>07 2021-09-07<br>11-00 | T4<br>Water<br>7 2021-09-07<br>12:00 | T5<br>Water<br>2021-09-07<br>13-00 |                           |  |  |
| Parameter                 | Unit                         | G/S RD                                    | L 2940                                      | 146 2940154                                   | 4 2940155                             | 2940156                              | 2940157                            |                           |  |  |
| Total Aluminum            | mg/L                         | 0.0                                       | 10 0.01                                     | 0.014   | 0.017                                 | 0.059                                | 2.46                               |                           |  |  |
| Total Antimony            | mg/L                         | 0.0                                       | 03 <0.0                                     | 03 <0.003                                     | <0.003                                | <0.003                               | < 0.003                            |                           |  |  |
| Total Arsenic             | mg/L                         | 0.0                                       | 03 <0.0                                     | 03 <0.003                                     | < 0.003                               | <0.003                               | < 0.003                            |                           |  |  |
| Total Barium              | mg/L                         | 0.0                                       | 02 0.06                                     | 64 0.059                                      | 0.059                                 | 0.051                                | 0.103                              |                           |  |  |
| Total Beryllium           | mg/L                         | 0.00                                      | 005 <0.00                                   | 005 <0.0005                                   | < 0.0005                              | < 0.0005                             | <0.0005                            |                           |  |  |
| Total Bismuth             | mg/L                         | 0.0                                       | 02 <0.0                                     | 02 <0.002                                     | <0.002                                | <0.002                               | < 0.002                            |                           |  |  |
| Total Boron               | mg/L                         | 0.0                                       | 10 0.16                                     | 0.114   | 0.172                                 | 0.098                                | 0.111                              |                           |  |  |
| Total Cadmium             | mg/L                         | 0.00                                      | 001 <0.00                                   | 001 <0.0001                                   | <0.0001                               | <0.0001                              | <0.0001                            |                           |  |  |
| Total Chromium            | mg/L                         | 0.0                                       | 03 <0.0                                     | 03 <0.003                                     | < 0.003                               | <0.003                               | 0.004                              |                           |  |  |
| Total Cobalt              | mg/L                         | 0.00                                      | 005 <0.00                                   | 005 <0.0005                                   | < 0.0005                              | < 0.0005                             | 0.0013                             |                           |  |  |
| Total Copper              | mg/L                         | 0.0                                       | 0.00  | 0.003   | 0.001                                 | 0.003                                | 0.010                              |                           |  |  |
| Total Iron                | mg/L                         | 0.0                                       | 10 2.3                                      | 6 0.121                                       | 0.112                                 | 0.452                                | 3.76                               |                           |  |  |
| Total Lead                | mg/L                         | 0.0                                       | 01 <0.0                                     | 01 <0.001                                     | <0.001                                | <0.001                               | 0.002                              |                           |  |  |
| Total Manganese           | mg/L                         | 0.0                                       | 02 0.22                                     | 0.065   | 0.020                                 | 0.205                                | 0.374                              |                           |  |  |
| Total Mercury             | mg/L                         | 0.00                                      | 001 <0.00                                   | 001 <0.0001                                   | <0.0001                               | <0.0001                              | <0.0001                            |                           |  |  |
| Total Molybdenum          | mg/L                         | 0.0                                       | 02 0.02                                     | 0.002   | 0.031                                 | 0.004                                | 0.005                              |                           |  |  |
| Total Nickel              | mg/L                         | 0.0                                       | 03 <0.0                                     | 03 <0.003                                     | < 0.003                               | <0.003                               | < 0.003                            |                           |  |  |
| Total Phosphorus          | mg/L                         | 0.1                                       | 0 <0.1                                      | 10 <0.10                                      | <0.10                                 | 0.22                                 | 0.92                               |                           |  |  |
| Total Selenium            | mg/L                         | 0.0                                       | 02 <0.0                                     | 02 <0.002                                     | <0.002                                | < 0.002                              | < 0.002                            |                           |  |  |
| Total Silicon             | mg/L                         | 0.0                                       | 0.9   | 8 0.20  | 0.44                                  | 2.63                                 | 7.57                               |                           |  |  |
| Total Silver              | mg/L                         | 0.00                                      | 001 <0.00                                   | 001 <0.0001                                   | <0.0001                               | <0.0001                              | <0.0001                            |                           |  |  |
| Total Strontium           | mg/L                         | 0.0                                       | 05 0.50                                     | 0.583   | 0.184                                 | 0.759                                | 1.10                               |                           |  |  |
| Total Thallium            | mg/L                         | 0.00                                      | 003 <0.00                                   | 003 <0.0003                                   | < 0.0003                              | < 0.0003                             | < 0.0003                           |                           |  |  |
| Total Tin                 | mg/L                         | 0.0                                       | 02 <0.0                                     | 02 <0.002                                     | <0.002                                | <0.002                               | < 0.002                            |                           |  |  |
| Total Titanium            | mg/L                         | 0.0                                       | 02 <0.0                                     | 02 <0.002                                     | <0.002                                | <0.002                               | 0.087                              |                           |  |  |
| Total Uranium             | mg/L                         | 0.00                                      | 005 <0.00                                   | 005 <0.0005                                   | 0.0007                                | <0.0005                              | <0.0005                            |                           |  |  |
| Total Vanadium            | mg/L                         | 0.0                                       | 02 <0.0                                     | 02 <0.002                                     | <0.002                                | < 0.002                              | 0.004                              |                           |  |  |
| Total Zinc                | mg/L                         | 0.0                                       | 05 <0.0                                     | 05 <0.005                                     | <0.005                                | <0.005                               | 0.010                              |                           |  |  |
| Total Zirconium           | mg/L                         | 0.0                                       | 04 <0.0                                     | 04 <0.004                                     | < 0.004                               | < 0.004                              | < 0.004                            |                           |  |  |







AGAT WORK ORDER: 21T798235 PROJECT: Alliston (1101-4125)

**CLIENT NAME: CROZIER & ASSOCIATES** 

SAMPLING SITE: Alliston

ATTENTION TO: Caitlyn Macphee

**DATE REPORTED: 2021-09-14** 

SAMPLED BY:C. MacPhee

Total Metals in water (mg/L)

DATE RECEIVED: 2021-09-07

**Comments:** RDL - Reported Detection Limit; G / S - Guideline / Standard Analysis performed at AGAT Toronto (unless marked by \*)



**Certified By:** 

5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.agatlabs.com



### **Quality Assurance**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

#### PROJECT: Alliston (1101-4125)

#### SAMPLING SITE: Alliston

AGAT WORK ORDER: 21T798235 **ATTENTION TO: Caitlyn Macphee** 

SAMPLED BY:C. MacPhee

### **Microbiology Analysis**

| RPT Date: Sep 14, 2021             |          |        | DUPLICATE |        |     |                 | REFERENCE MATERIAL |             |                | METHOD BLANK SPIKE |             |                 | MATRIX SPIKE |             |                |
|------------------------------------|----------|--------|-----------|--------|-----|-----------------|--------------------|-------------|----------------|--------------------|-------------|-----------------|--------------|-------------|----------------|
| PARAMETER                          | Batch    | Sample | Dup #1    | Dup #2 | RPD | Method<br>Blank | Measured           | Acce<br>Lir | ptable<br>nits | Recoverv           | Acce<br>Lir | eptable<br>nits | Recoverv     | Acce<br>Lin | ptable<br>nits |
|                                    |          | ld     |           |        |     |                 | Value              | Lower       | Upper          |                    | Lower       | Upper           |              | Lower       | Upper          |
| Total Coliforms & E. Coli (Using N | II Agar) |        |           |        |     |                 |                    |             |                |                    |             |                 |              |             |                |

| Escherichia coli | 2940146 2940146 | ND | ND | NA | < 1 |
|------------------|-----------------|----|----|----|-----|
| Total Coliforms  | 2940146 2940146 | 2  | 1  | NA | < 1 |

Comments: ND - Not Detected, NA - % RPD Not Applicable.

NA - % RPD Not Reportable based on the number of colonies count acceptable for RPD calculation.





**AGAT** QUALITY ASSURANCE REPORT (V1)

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### **Quality Assurance**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

#### PROJECT: Alliston (1101-4125)

#### SAMPLING SITE: Alliston

#### AGAT WORK ORDER: 21T798235 ATTENTION TO: Caitlyn Macphee SAMPLED BY:C. MacPhee

### Water Analysis

|         |  | _  |   | -  |  | DEFEDEN   |  |   | METHOD   |   | 0.00   |   |   |   |
|---------|--|--|---|--|--|---|--|---|--|---|--|---|---|---|
|         |  | L  | UPLICAT   | E  |  |   |  | TERIAL  | METHOD   | BLANK   | SPIKE  | MATRIA SPIRE  |   |   |
| Batch   | Sample   | Dup #1   | Dup #2  | RPD  | Method<br>Blank  | Measured  | Acce<br>Lir  | ptable<br>nits  | Recovery   | Acce<br>Lin   | ptable<br>nits   | Recovery  | Acceptable<br>Limits  |   |
|         | Ia   |  |   |  |  | value   | Lower  | Upper   |  | Lower   | Upper  | -   | Lower   | Upper   |
|         |  |  |   |  |  |   |  |   |  |   |  |   |   |   |
| 2954187 |  | <0.05  | <0.05   | NA   | < 0.05   | 99%   | 70%  | 130%  | 101%   | 80%   | 120%   | 110%  | 70%   | 130%  |
| 2954187 |  | 135  | 132   | 2.2%   | < 0.10   | 94%   | 70%  | 130%  | 100%   | 80%   | 120%   | 107%  | 70%   | 130%  |
| 2954187 |  | <0.07  | <0.07   | NA   | < 0.05   | 98%   | 70%  | 130%  | 102%   | 80%   | 120%   | 111%  | 70%   | 130%  |
| 2954187 |  | <0.05  | <0.05   | NA   | < 0.05   | 96%   | 70%  | 130%  | 95%  | 80%   | 120%   | 108%  | 70%   | 130%  |
| 2954187 |  | 0.89   | 0.77  | 14.5%  | < 0.05   | 104%  | 70%  | 130%  | 105%   | 80%   | 120%   | 108%  | 70%   | 130%  |
| 2954187 |  | 322  | 323   | 0.3%   | < 0.10   | 101%  | 70%  | 130%  | 101%   | 80%   | 120%   | NA  | 70%   | 130%  |
| 2954187 |  | <0.13  | <0.13   | NA   | < 0.10   | 105%  | 70%  | 130%  | 103%   | 80%   | 120%   | 100%  | 70%   | 130%  |
|         | Batch<br>2954187<br>2954187<br>2954187<br>2954187<br>2954187<br>2954187<br>2954187 | Batch         Sample<br>Id           2954187         2954187           2954187         2954187           2954187         2954187           2954187         2954187           2954187         2954187           2954187         2954187 | Batch         Sample<br>Id         Dup #1           2954187         <0.05 | Batch         Sample<br>Id         Dup #1         Dup #2           2954187         <0.05 | Batch         Sample<br>Id         Dup #1         Dup #2         RPD           2954187         <0.05 | DUPLICATE         Method Blank           Batch         Sample Id         Dup #1         Dup #2         RPD         Method Blank           2954187         <0.05 | DUPLICATE         Method         REFEREN           Batch         Sample<br>Id         Dup #1         Dup #2         RPD         Method         Measured<br>Value           2954187         <0.05 | DUPLICATE         Method         REFERENCE MA           Batch         Sample<br>Id         Dup #1         Dup #2         RPD         Method         Measured<br>Value         Acce<br>Lir           2954187         <0.05 | DUPLICATE         REFERENCE MATERIAL           Batch         Sample<br>Id         Dup #1         Dup #2         RPD         Method<br>Blank         REFERENCE MATERIAL           2954187         <0.05 | DUPLICATE         Method<br>Blank         REFERENCE MATERIAL<br>Measured<br>Value         METHOD           Batch         Sample<br>Id         Dup #1         Dup #2         RPD         Method<br>Blank         Method<br>Blank         Measured<br>Value         Acceptable<br>Limits         Recovery           2954187         <0.05 | DUPLICATE         Method<br>Blank         REFERENCE MATERIAL         METHOD BLANK         Acceptable<br>Limits         Method Blank           Batch         Sample<br>Id         Dup #1         Dup #2         RPD         Method<br>Blank         Method<br>Measured<br>Value         Acceptable<br>Limits         Recovery         Acce<br>Lin           2954187         <0.05 | Batch         Sample<br>Id         Dup #1         Dup #2         RPD         Method<br>Blank         REFERENCE MATERIAL<br>Value         METHOD BLANK SPIKE         Acceptable<br>Limits         Acceptable Limits         Accentable | Batch         Sample<br>Id         Dup #1         Dup #2         RPD         Method<br>Blank         REFERENCE MATERIAL<br>Value         METHOD BLANK SPIKE         MAT           2954187         <0.05 | DUPLICATE         Reference Material         Method Blank         Recovery         Acceptable Limits         Matrix SPI         Matrix SPI         Matrix SPI           Batch         Sample Id         Dup #1         Dup #2         RPD         Method Blank         Method Blank         Acceptable Limits         Acceptable Limits         Acceptable Limits         Acceptable Limits         Recovery         Acceptable Limits         Acceptable Limits         Acceptable Limits         Recovery         Acceptable Limits         Recovery         Acceptable Limits         Acceptable Limits         Recovery         Acceptable Limits |

Comments: NA signifies Not Applicable.

Duplicate NA: results are under 5X the RDL and will not be calculated.

Matrix spike NA: Spike level < native concentration. Matrix spike acceptance limits do not apply and are not calculated.

#### Total Metals in water (mg/L)

| Total Aluminum   | 2936001 | <0.010  | <0.010   | NA | < 0.010  | 98%  | 70% | 130% | 105% | 80% | 120% | 108% | 70% | 130% |
|------------------|---------|---------|----------|----|----------|------|-----|------|------|-----|------|------|-----|------|
| Total Antimony   | 2936001 | <0.003  | <0.003   | NA | < 0.003  | 100% | 70% | 130% | 98%  | 80% | 120% | 100% | 70% | 130% |
| Total Arsenic    | 2936001 | <0.003  | <0.003   | NA | < 0.003  | 92%  | 70% | 130% | 105% | 80% | 120% | 105% | 70% | 130% |
| Total Barium     | 2936001 | < 0.002 | <0.002   | NA | < 0.002  | 98%  | 70% | 130% | 99%  | 80% | 120% | 100% | 70% | 130% |
| Total Beryllium  | 2936001 | <0.0005 | <0.0005  | NA | < 0.0005 | 94%  | 70% | 130% | 103% | 80% | 120% | 105% | 70% | 130% |
| Total Bismuth    | 2936001 | <0.002  | <0.002   | NA | < 0.002  | 93%  | 70% | 130% | 108% | 80% | 120% | 110% | 70% | 130% |
| Total Boron      | 2936001 | <0.010  | <0.010   | NA | < 0.010  | 96%  | 70% | 130% | 104% | 80% | 120% | 105% | 70% | 130% |
| Total Cadmium    | 2936001 | <0.0001 | <0.0001  | NA | < 0.0001 | 100% | 70% | 130% | 100% | 80% | 120% | 98%  | 70% | 130% |
| Total Chromium   | 2936001 | < 0.003 | < 0.003  | NA | < 0.003  | 97%  | 70% | 130% | 99%  | 80% | 120% | 105% | 70% | 130% |
| Total Cobalt     | 2936001 | <0.0005 | <0.0005  | NA | < 0.0005 | 99%  | 70% | 130% | 101% | 80% | 120% | 107% | 70% | 130% |
| Total Copper     | 2936001 | <0.001  | <0.001   | NA | < 0.001  | 97%  | 70% | 130% | 100% | 80% | 120% | 106% | 70% | 130% |
| Total Iron       | 2936001 | <0.010  | <0.010   | NA | < 0.010  | 103% | 70% | 130% | 107% | 80% | 120% | 108% | 70% | 130% |
| Total Lead       | 2936001 | <0.001  | <0.001   | NA | < 0.001  | 101% | 70% | 130% | 102% | 80% | 120% | 105% | 70% | 130% |
| Total Manganese  | 2936001 | <0.002  | <0.002   | NA | < 0.002  | 100% | 70% | 130% | 102% | 80% | 120% | 103% | 70% | 130% |
| Total Mercury    | 2936001 | <0.0001 | <0.0001  | NA | < 0.0001 | 105% | 70% | 130% | 98%  | 80% | 120% | 100% | 70% | 130% |
| Total Molybdenum | 2936001 | <0.002  | <0.002   | NA | < 0.002  | 101% | 70% | 130% | 102% | 80% | 120% | 110% | 70% | 130% |
| Total Nickel     | 2936001 | < 0.003 | < 0.003  | NA | < 0.003  | 98%  | 70% | 130% | 103% | 80% | 120% | 106% | 70% | 130% |
| Total Phosphorus | 2936001 | <0.10   | <0.10    | NA | < 0.10   | 103% | 70% | 130% | 96%  | 80% | 120% | 115% | 70% | 130% |
| Total Selenium   | 2936001 | <0.002  | <0.002   | NA | < 0.002  | 99%  | 70% | 130% | 112% | 80% | 120% | 105% | 70% | 130% |
| Total Silicon    | 2936001 | <0.08   | <0.08    | NA | < 0.08   | 91%  | 70% | 130% | 97%  | 80% | 120% | 107% | 70% | 130% |
| Total Silver     | 2936001 | <0.0001 | <0.0001  | NA | < 0.0001 | 100% | 70% | 130% | 103% | 80% | 120% | 109% | 70% | 130% |
| Total Strontium  | 2936001 | <0.005  | <0.005   | NA | < 0.005  | 99%  | 70% | 130% | 103% | 80% | 120% | 106% | 70% | 130% |
| Total Thallium   | 2936001 | <0.0003 | < 0.0003 | NA | < 0.0003 | 93%  | 70% | 130% | 107% | 80% | 120% | 107% | 70% | 130% |
| Total Tin        | 2936001 | <0.002  | <0.002   | NA | < 0.002  | 94%  | 70% | 130% | 100% | 80% | 120% | 100% | 70% | 130% |
| Total Titanium   | 2936001 | <0.002  | <0.002   | NA | < 0.002  | 105% | 70% | 130% | 88%  | 80% | 120% | 97%  | 70% | 130% |
| Total Uranium    | 2936001 | <0.0005 | <0.0005  | NA | < 0.0005 | 103% | 70% | 130% | 104% | 80% | 120% | 106% | 70% | 130% |

#### AGAT QUALITY ASSURANCE REPORT (V1)

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### **Quality Assurance**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

#### PROJECT: Alliston (1101-4125)

#### SAMPLING SITE: Alliston

#### AGAT WORK ORDER: 21T798235 ATTENTION TO: Caitlyn Macphee SAMPLED BY:C. MacPhee

### Water Analysis (Continued)

| RPT Date: Sep 14, 2021 |         |        | C      | UPLICAT | E   |                 | REFERENCE MATERIAL |             |                | METHOD BLANK SPIKE |             |                | MATRIX SPIKE |             |                |
|------------------------|---------|--------|--------|---------|-----|-----------------|--------------------|-------------|----------------|--------------------|-------------|----------------|--------------|-------------|----------------|
| PARAMETER              | Batch   | Sample | Dup #1 | Dup #2  | RPD | Method<br>Blank | Measured           | Acce<br>Lir | ptable<br>nits | Recovery           | Acce<br>Lir | ptable<br>nits | Recovery     | Acce<br>Lir | ptable<br>nits |
|                        |         | Ia     |        |         |     |                 | value              | Lower       | Upper          | -                  | Lower       | Upper          |              | Lower       | Upper          |
| Total Vanadium         | 2936001 |        | <0.002 | <0.002  | NA  | < 0.002         | 98%                | 70%         | 130%           | 99%                | 80%         | 120%           | 104%         | 70%         | 130%           |
| Total Zinc             | 2936001 |        | <0.005 | <0.005  | NA  | < 0.005         | 97%                | 70%         | 130%           | 100%               | 80%         | 120%           | 109%         | 70%         | 130%           |
| Total Zirconium        | 2936001 |        | <0.004 | <0.004  | NA  | < 0.004         | 95%                | 70%         | 130%           | 100%               | 80%         | 120%           | 106%         | 70%         | 130%           |

Comments: NA signifies Not Applicable.

Duplicate NA: results are under 5X the RDL and will not be calculated.

#### Cations in Water - Total (mg/L)

| Total Calcium   | 2936001 | <0.10 | <0.10 | NA | < 0.10 | 97%  | 70% | 130% | 96%  | 80% | 120% | 95%  | 70% | 130% |
|-----------------|---------|-------|-------|----|--------|------|-----|------|------|-----|------|------|-----|------|
| Total Magnesium | 2936001 | <0.10 | <0.10 | NA | < 0.10 | 101% | 70% | 130% | 100% | 80% | 120% | 98%  | 70% | 130% |
| Total Potassium | 2936001 | <0.50 | <0.50 | NA | < 0.50 | 100% | 70% | 130% | 100% | 80% | 120% | 100% | 70% | 130% |
| Total Sodium    | 2936001 | <0.10 | <0.10 | NA | < 0.10 | 96%  | 70% | 130% | 95%  | 80% | 120% | 99%  | 70% | 130% |

Comments: NA signifies Not Applicable.

Duplicate NA: results are under 5X the RDL and will not be calculated.





#### AGAT QUALITY ASSURANCE REPORT (V1)

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# **Method Summary**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

AGAT WORK ORDER: 21T798235

**ATTENTION TO: Caitlyn Macphee** 

#### SAMPLING SITE: Alliston

PROJECT: Alliston (1101-4125)

SAMPLED BY:C. MacPhee

| PARAMETER             | AGAT S.O.P  | LITERATURE REFERENCE | ANALYTICAL TECHNIQUE |  |  |  |  |  |  |  |
|-----------------------|-------------|----------------------|----------------------|--|--|--|--|--|--|--|
| Microbiology Analysis | ·           |                      |                      |  |  |  |  |  |  |  |
| Escherichia coli      | MIC-93-7010 | EPA 1604             | Membrane Filtration  |  |  |  |  |  |  |  |
| Total Coliforms       | MIC-93-7010 | EPA 1604             | Membrane Filtration  |  |  |  |  |  |  |  |



# **Method Summary**

#### CLIENT NAME: CROZIER & ASSOCIATES

#### PROJECT: Alliston (1101-4125)

### AGAT WORK ORDER: 21T798235 ATTENTION TO: Caitlyn Macphee

| SAMPLING SITE: Alliston |              | SAMPLED BY:C. MacPhee                            |                      |  |  |  |  |  |  |
|-------------------------|--------------|--|----------------------|--|--|--|--|--|--|
| PARAMETER               | AGAT S.O.P   | LITERATURE REFERENCE                             | ANALYTICAL TECHNIQUE |  |  |  |  |  |  |
| Water Analysis          |              | 1  |                      |  |  |  |  |  |  |
| Fluoride                | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |  |  |  |  |  |  |
| Chloride                | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |  |  |  |  |  |  |
| Nitrate as N            | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |  |  |  |  |  |  |
| Nitrite as N            | INOR-93-6004 | SM 4110 B  | ION CHROMATOGRAPH    |  |  |  |  |  |  |
| Bromide                 | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |  |  |  |  |  |  |
| Sulphate                | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |  |  |  |  |  |  |
| Phosphate as P          | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |  |  |  |  |  |  |
| Total Calcium           | MET-93-6105  | modified from EPA 6010D                          | ICP/OES              |  |  |  |  |  |  |
| Total Magnesium         | MET-93-6105  | modified from EPA 6010D                          | ICP/OES              |  |  |  |  |  |  |
| Total Potassium         | MET-93-6105  | modified from EPA 6010D                          | ICP/OES              |  |  |  |  |  |  |
| Total Sodium            | MET-93-6105  | modified from EPA 6010D                          | ICP/OES              |  |  |  |  |  |  |
| Total Aluminum          | MET-93-6103  | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |  |  |  |  |  |  |
| Total Antimony          | MET-93-6103  | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |  |  |  |  |  |  |
| Total Arsenic           | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Barium            | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Beryllium         | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Bismuth           | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Boron             | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Cadmium           | MET -93-6103 | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Chromium          | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Cobalt            | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Copper            | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Iron              | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Lead              | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Manganese         | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Mercury           | MET-93-6100  | modified from EPA 245.2 and SM 31<br>B           | <sup>12</sup> CVAAS  |  |  |  |  |  |  |
| Total Molybdenum        | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Nickel            | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Phosphorus        | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Selenium          | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Silicon           | MET-93-6103  | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |  |  |  |  |  |  |
| Total Silver            | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |



# **Method Summary**

### CLIENT NAME: CROZIER & ASSOCIATES

### PROJECT: Alliston (1101-4125)

### AGAT WORK ORDER: 21T798235 ATTENTION TO: Caitlyn Macphee

| SAMPLING SITE: Alliston |              | SAMPLED BY:C. MacPhee                            |                      |  |  |  |  |  |  |
|-------------------------|--------------|--|----------------------|--|--|--|--|--|--|
| PARAMETER               | AGAT S.O.P   | LITERATURE REFERENCE                             | ANALYTICAL TECHNIQUE |  |  |  |  |  |  |
| Total Strontium         | INOR-93-6003 | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Thallium          | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Tin               | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Titanium          | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Uranium           | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Vanadium          | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Zinc              | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Zirconium         | MET-93-6103  | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |  |  |  |  |  |  |

| AGAT Labor   | ratories  | 5835 Coopers Ave<br>Mississauga, Ontario L4Z<br>Ph: 905.712.5100 Fax: 905.712.5<br>webearth.agatlabs.   | enue     Laboratory Use Only       2 1Y2     Work Order #: 217798235       Scoon     Cooler Quantity:       Cooler Quantity:     1 arge   |
|--|---|---|---|
| Chain of Custody Record         If this is a Drinking Water sample         Report Information:         Company:       CF Cro3ier & associate         Contact:       Caithun MacPhae         Address:       Suite 100, 2800 highp         Phone:       Fax:         Reports to be sent to:       Fax:         1. Email:       Coerchic & Cfcro3ier.         2. Email:       Coerchic & Cfcro3ier.         Project Information:         Project:       Alliston (101-4125)         Site Location:       Alliston   | constraints       Regulatory Requirem         (Picase check all applicable bases)       Regulation 153/04         Constraints       Regulation 153/04         Table       Indicate One         Dind/Com       Res/Park         Agriculture       R         Soil Texture (check one)       C         Fine       Is this submission for         Record of Site Condition       Yes  | Ady Form (potable water consumed by humans)   | Arrival Temperatures:<br>Custody Seal Intact:<br>Custody Seal Intact:<br>Custody Seal Intact:<br>Custody Seal Intact:<br>Custody Seal Intact:<br>Custody Seal Intact:<br>Custody Seal Intact:<br>Press Days<br>Custody Seal Intact:<br>Custody Seal Intact:<br>Press Days<br>Custody Seal Intact:<br>Press Days<br>Custody Seal Intact:<br>Custody Seal Intact:<br>Press Days<br>Custody Seal Intact:<br>Press Days<br>Press Provide Prior notification for rush TAT<br>*TAT is exclusive of weekends and statutory holidays<br>For 'Same Day' analysis, please contact your AGAT CPM   |
| AGAT ID #:   | No C<br>Sample Matrix Legend<br>B Biota<br>GW Ground Water<br>O Oil<br>P Paint<br>S Soil<br>Soil<br>Sw Surface Water  | Rei 123<br>& Inorganics<br>& Inorganics<br>CrVI, DOC<br>A& Inorganics<br>- CrVI, DHg, DHWSB<br>CrVI, DHg, DHWSB<br>CrVI, DHS, CrVI, DOC<br>CrVI, DC<br>CrVI, CV<br>CrVI, DC<br>CrVI, CV<br>CrVI, CV<br>CV<br>CrVI, CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV<br>CV | CBS Aroclor<br>Disposal Characterization TCDP:<br>Disposal Characterization TCDP:<br>Meal Dvocs Dates Data PCD PCB8 B934<br>Soils SPLP Rainwater Leach<br>Soils Characterization Package<br>MS Metals, BTEX, F1-F4<br>Soils Characterization Package<br>MS Metals, BTEX, F1-F4<br>Or D 1<br>F O 1 C 0 1 F F C M<br>F O 1 C 0 1 F F C M<br>F O 1 C 0 1 F C M<br>F O 1 C 0 F F O 1 F C M<br>F O 1 C 0 F F O 1 |
| Sample Identification     Date<br>Sampled     Time<br>Sampled     H contain<br>Contain       T1     09/07     31     AM<br>Contain     Contain       T2     1     330     AM<br>Contain     Contain       T3     11     AM<br>Contain     Contain       T4     12     AM<br>Contain     Contain       T5     V     AM<br>Contain     Contain       AM     AM<br>Contain     AM<br>Contain       AM     AM<br>Contain     AM<br>Contain       T3     T4     Contain       T5     V     AM<br>Contain       AM     AM<br>Contain     AM       AM     AM     AM       AM     AM       AM     AM | Sample Comments<br>Matrix Special Instruct<br>Secial | And   | Total PC       Total PC       VOC       Landfill       Total PC       Total PC       PH. ICP       Ph. ICP    Ph. ICP   P   |
| Samples Relinquished By (Print Name and Sign):     Date     Date       Samples Relinquished By (Print Name and Sign):     Date   Date Decement ID: Div-78-1511.020   | Time Samples Received By (Print Name  | e and Sign):<br>e and Sign):<br>e and Sign):<br>Pink Copy - C   | Date         Time         121 SEP         7         6         6         6         6         7         1         2         4         1         7         1         2         4         1         7         0         2         0         1         1         1         2         4         1         7         0         2         0         <   |

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#### CLIENT NAME: CROZIER & ASSOCIATES 2800 HIGH POINT DRIVE, SUITE 100 MILTON, ON L9T 6P4 905-875-0026 ATTENTION TO: Caitlyn Macphee PROJECT: Alliston(1101-4125) AGAT WORK ORDER: 21T781957 MICROBIOLOGY ANALYSIS REVIEWED BY: Nivine Basily, Inorganics Report Writer WATER ANALYSIS REVIEWED BY: Nivine Basily, Inorganics Report Writer DATE REPORTED BY: Yris Verastegui, Report Reviewer DATE REPORTED: Aug 06, 2021 PAGES (INCLUDING COVER): 12 VERSION\*: 1

Should you require any information regarding this analysis please contact your client services representative at (905) 712-5100

\*Notes

Disclaimer:

- All work conducted herein has been done using accepted standard protocols, and generally accepted practices and methods. AGAT test methods may
  incorporate modifications from the specified reference methods to improve performance.
- All samples will be disposed of within 30 days after receipt unless a Long Term Storage Agreement is signed and returned. Some specialty analysis may be exempt, please contact your Client Project Manager for details.
- AGAT's liability in connection with any delay, performance or non-performance of these services is only to the Client and does not extend to any other third party. Unless expressly agreed otherwise in writing, AGAT's liability is limited to the actual cost of the specific analysis or analyses included in the services.
- This Certificate shall not be reproduced except in full, without the written approval of the laboratory.
- The test results reported herewith relate only to the samples as received by the laboratory.
- Application of guidelines is provided "as is" without warranty of any kind, either expressed or implied, including, but not limited to, warranties of
  merchantability, fitness for a particular purpose, or non-infringement. AGAT assumes no responsibility for any errors or omissions in the guidelines
  contained in this document.
- All reportable information as specified by ISO/IEC 17025:2017 is available from AGAT Laboratories upon request.

**AGAT** Laboratories (V1)

| lember of: As | ssociation of Professional Engineers and Geoscientists of Alberta |
|---------------|---|
| (A            | PEGA)   |
| Ŵ             | estern Enviro-Agricultural Laboratory Association (WEALA)         |

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Page 1 of 12



AGAT WORK ORDER: 21T781957 PROJECT: Alliston(1101-4125)

**CLIENT NAME: CROZIER & ASSOCIATES** 

SAMPLING SITE:

### ATTENTION TO: Caitlyn Macphee

SAMPLED BY:

| Total Coliforms | & E. | Coli (Using | MI Agar) |
|-----------------|------|-------------|----------|
|                 |      |             |          |

| DATE RECEIVED: 2021-07-30 |           |           |           |            |            |            |            |            | DATE REPORTED: 2021-08-06 |
|---------------------------|-----------|-----------|-----------|------------|------------|------------|------------|------------|---------------------------|
|                           | S         | AMPLE DES | CRIPTION: | MW1        | MW2        | MW3        | MW4        | MW5        |                           |
|                           |           | SAM       | PLE TYPE: | Water      | Water      | Water      | Water      | Water      |                           |
|                           |           | DATE      | SAMPLED:  | 2021-07-30 | 2021-07-30 | 2021-07-30 | 2021-07-30 | 2021-07-30 |                           |
|                           |           |           |           | 09:00      | 09:30      | 10:00      | 11:30      | 12:00      |                           |
| Parameter                 | Unit      | G/S       | RDL       | 2801012    | 2801148    | 2801149    | 2801150    | 2801151    |                           |
| Escherichia coli          | CFU/100mL |           | 2         | ND         | ND         | ND         | ND         | ND         |                           |
| Total Coliforms           | CFU/100mL |           | 100       | 3100       | 700        | 800        | 1500       | 2800       |                           |
|                           |           |           |           |            |            |            |            |            |                           |

**Comments:** RDL - Reported Detection Limit; G / S - Guideline / Standard

2801012-2801151 ND - Not Detected.

If RDL >1 indicates dilutions of the sample.

Analysis performed at AGAT Toronto (unless marked by \*)



5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.agatlabs.com



AGAT WORK ORDER: 21T781957 PROJECT: Alliston(1101-4125)

#### **CLIENT NAME: CROZIER & ASSOCIATES**

SAMPLING SITE:

5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.agatlabs.com

#### **ATTENTION TO: Caitlyn Macphee**

SAMPLED BY:

|   |      |            |           |                     | /                   | Jan  |                     |      |                     |      |                     |  |
|---|------|------------|-----------|---------------------|---------------------|------|---------------------|------|---------------------|------|---------------------|--|
| DATE RECEIVED: 2021-07-30 DATE REPORTED: 2021-08-06 |      |            |           |                     |                     |      |                     |      |                     |      |                     |  |
|   |      | SAMPLE DES | CRIPTION: | MW1                 | MW2                 |      | MW3                 |      | MW4                 |      | MW5                 |  |
|   |      | SAM        | PLE TYPE: | Water               | Water               |      | Water               |      | Water               |      | Water               |  |
|   |      | DATE       | SAMPLED:  | 2021-07-30<br>09:00 | 2021-07-30<br>09:30 |      | 2021-07-30<br>10:00 |      | 2021-07-30<br>11:30 |      | 2021-07-30<br>12:00 |  |
| Parameter   | Unit | G/S        | RDL       | 2801012             | 2801148             | RDL  | 2801149             | RDL  | 2801150             | RDL  | 2801151             |  |
| Fluoride  | mg/L |            | 0.05      | <0.05               | 0.20                | 0.05 | <0.05               | 0.05 | <0.05               | 0.05 | <0.05               |  |
| Chloride  | mg/L |            | 0.10      | 20.0                | 23.9                | 0.12 | 236                 | 0.49 | 1100                | 0.10 | 48.7                |  |
| Nitrate as N  | mg/L |            | 0.05      | 5.93                | 8.57                | 0.05 | <0.05               | 0.14 | 0.90                | 0.05 | 0.74                |  |
| Nitrite as N  | mg/L |            | 0.05      | 0.25                | 0.33                | 0.05 | <0.05               | 0.11 | <0.11               | 0.05 | 0.38                |  |
| Bromide   | mg/L |            | 0.05      | <0.05               | <0.05               | 0.05 | <0.05               | 0.11 | <0.11               | 0.05 | <0.05               |  |
| Sulphate  | mg/L |            | 0.10      | 14.0                | 53.2                | 0.10 | 30.5                | 0.38 | 42.6                | 0.10 | 56.3                |  |
| Phosphate as P                                      | mg/L |            | 0.10      | <0.10               | <0.10               | 0.10 | <0.10               | 0.26 | <0.26               | 0.10 | <0.10               |  |

Anion Scan

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard

2801149-2801150 Dilution required, RDL has been increased accordingly.

Analysis performed at AGAT Toronto (unless marked by \*)

**Certified By:** 

Inis Verastegui



AGAT WORK ORDER: 21T781957 PROJECT: Alliston(1101-4125)

Total Motals in water (mg/L)

5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.aqatlabs.com

#### **CLIENT NAME: CROZIER & ASSOCIATES**

SAMPLING SITE:

#### ATTENTION TO: Caitlyn Macphee

SAMPLED BY:

|                           |      |             |                        | 1014                         |                              |                              | -)                           |                              |                           |
|---------------------------|------|-------------|------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|---------------------------|
| DATE RECEIVED: 2021-07-30 |      |             |                        |                              |                              |                              |                              |                              | DATE REPORTED: 2021-08-06 |
|                           |      | SAMPLE DES  | CRIPTION:              | MW1                          | MW2                          | MW3                          | MW4                          | MW5                          |                           |
|                           |      | SAM<br>DATE | IPLE TYPE:<br>SAMPLED: | Water<br>2021-07-30<br>09:00 | Water<br>2021-07-30<br>09:30 | Water<br>2021-07-30<br>10:00 | Water<br>2021-07-30<br>11:30 | Water<br>2021-07-30<br>12:00 |                           |
| Parameter                 | Unit | G/S         | RDL                    | 2801012                      | 2801148                      | 2801149                      | 2801150                      | 2801151                      |                           |
| Total Aluminum            | mg/L |             | 0.010                  | 1.41                         | 0.022                        | 0.045                        | 0.027                        | 0.014                        |                           |
| Total Antimony            | mg/L |             | 0.003                  | < 0.003                      | < 0.003                      | < 0.003                      | < 0.003                      | < 0.003                      |                           |
| Total Arsenic             | mg/L |             | 0.003                  | < 0.003                      | < 0.003                      | < 0.003                      | < 0.003                      | < 0.003                      |                           |
| Total Barium              | mg/L |             | 0.002                  | 0.060                        | 0.136                        | 0.226                        | 0.407                        | 0.140                        |                           |
| Total Beryllium           | mg/L |             | 0.0005                 | <0.0005                      | <0.0005                      | <0.0005                      | <0.0005                      | <0.0005                      |                           |
| Total Bismuth             | mg/L |             | 0.002                  | <0.002                       | <0.002                       | <0.002                       | <0.002                       | <0.002                       |                           |
| Total Boron               | mg/L |             | 0.010                  | 0.012                        | 0.087                        | 0.084                        | 0.100                        | 0.063                        |                           |
| Total Cadmium             | mg/L |             | 0.0001                 | <0.0001                      | <0.0001                      | <0.0001                      | <0.0001                      | <0.0001                      |                           |
| Total Chromium            | mg/L |             | 0.003                  | 0.003                        | < 0.003                      | < 0.003                      | < 0.003                      | < 0.003                      |                           |
| Total Cobalt              | mg/L |             | 0.0005                 | 0.0007                       | <0.0005                      | <0.0005                      | 0.0008                       | <0.0005                      |                           |
| Total Copper              | mg/L |             | 0.001                  | 0.005                        | 0.004                        | 0.003                        | 0.004                        | 0.004                        |                           |
| Total Iron                | mg/L |             | 0.010                  | 1.54                         | 0.013                        | 0.053                        | 0.030                        | 0.013                        |                           |
| Total Lead                | mg/L |             | 0.001                  | <0.001                       | <0.001                       | <0.001                       | <0.001                       | <0.001                       |                           |
| Total Manganese           | mg/L |             | 0.002                  | 0.063                        | 0.059                        | 0.043                        | 0.082                        | 0.054                        |                           |
| Total Mercury             | mg/L |             | 0.0001                 | 0.0001                       | <0.0001                      | <0.0001                      | <0.0001                      | <0.0001                      |                           |
| Total Molybdenum          | mg/L |             | 0.002                  | <0.002                       | 0.006                        | 0.002                        | 0.004                        | 0.002                        |                           |
| Total Nickel              | mg/L |             | 0.003                  | 0.004                        | < 0.003                      | < 0.003                      | < 0.003                      | < 0.003                      |                           |
| Total Phosphorus          | mg/L |             | 0.10                   | <0.10                        | <0.10                        | <0.10                        | <0.10                        | <0.10                        |                           |
| Total Selenium            | mg/L |             | 0.002                  | <0.002                       | < 0.002                      | <0.002                       | <0.002                       | <0.002                       |                           |
| Total Silicon             | mg/L |             | 0.08                   | 12.1                         | 7.89                         | 6.11                         | 8.40                         | 8.27                         |                           |
| Total Silver              | mg/L |             | 0.0001                 | <0.0001                      | <0.0001                      | < 0.0001                     | <0.0001                      | <0.0001                      |                           |
| Total Strontium           | mg/L |             | 0.005                  | 0.246                        | 0.520                        | 0.869                        | 1.52                         | 0.580                        |                           |
| Total Thallium            | mg/L |             | 0.0003                 | < 0.0003                     | < 0.0003                     | < 0.0003                     | < 0.0003                     | < 0.0003                     |                           |
| Total Tin                 | mg/L |             | 0.002                  | <0.002                       | <0.002                       | <0.002                       | <0.002                       | <0.002                       |                           |
| Total Titanium            | mg/L |             | 0.002                  | 0.085                        | <0.002                       | 0.003                        | 0.004                        | 0.003                        |                           |
| Total Uranium             | mg/L |             | 0.0005                 | 0.0010                       | 0.0035                       | 0.0026                       | 0.0016                       | 0.0033                       |                           |
| Total Vanadium            | mg/L |             | 0.002                  | 0.003                        | <0.002                       | <0.002                       | <0.002                       | < 0.002                      |                           |
| Total Zinc                | mg/L |             | 0.005                  | 0.012                        | <0.005                       | <0.005                       | <0.005                       | 0.005                        |                           |
| Total Zirconium           | mg/L |             | 0.004                  | < 0.004                      | < 0.004                      | < 0.004                      | < 0.004                      | < 0.004                      |                           |

**Certified By:** 

Inis Verastegui



AGAT WORK ORDER: 21T781957 PROJECT: Alliston(1101-4125)

**CLIENT NAME: CROZIER & ASSOCIATES** 

SAMPLING SITE:

ATTENTION TO: Caitlyn Macphee

**DATE REPORTED: 2021-08-06** 

SAMPLED BY:

Total Metals in water (mg/L)

DATE RECEIVED: 2021-07-30

**Comments:** RDL - Reported Detection Limit; G / S - Guideline / Standard Analysis performed at AGAT Toronto (unless marked by \*)

**Certified By:** 

Inis Verastegui

5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.agatlabs.com



### **Quality Assurance**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

#### PROJECT: Alliston(1101-4125)

SAMPLING SITE:

AGAT WORK ORDER: 21T781957 **ATTENTION TO: Caitlyn Macphee** 

SAMPLED BY:

### **Microbiology Analysis**

| RPT Date: Aug 06, 2021                    |           |    | DUPLICATE |        |     |                 | REFEREN             | RENCE MATERIAL       |       | METHOD BLANK SPIKE |                      |       | MATRIX SPIKE |                      |       |
|---|-----------|----|-----------|--------|-----|-----------------|---------------------|----------------------|-------|--------------------|----------------------|-------|--------------|----------------------|-------|
| PARAMETER                                 | Batch Sam |    | Dup #1    | Dup #2 | RPD | Method<br>Blank | nod<br>Ink Measured | Acceptable<br>Limits |       | Recoverv           | Acceptable<br>Limits |       | Recovery     | Acceptable<br>Limits |       |
|   |           | la | •         |        |     |                 | value               | Lower                | Upper |                    | Lower                | Upper |              | Lower                | Upper |
| Total Coliforms & E. Coli (Using MI Agar) |           |    |           |        |     |                 |                     |                      |       |                    |                      |       |              |                      |       |

| Escherichia coli | 2801012 2801012 | ND   | ND   | NA   | < 1 |
|------------------|-----------------|------|------|------|-----|
| Total Coliforms  | 2801012 2801012 | 3100 | 2900 | 6.7% | < 1 |

Comments: ND - Not Detected, NA - % RPD Not Applicable.



#### **AGAT** QUALITY ASSURANCE REPORT (V1)

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### **Quality Assurance**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

#### PROJECT: Alliston(1101-4125)

SAMPLING SITE:

AGAT WORK ORDER: 21T781957 ATTENTION TO: Caitlyn Macphee SAMPLED BY:

### Water Analysis

| PPT Date: Aug 06, 2021       |         |              | -       | REFERENCE MATERIAL |       | METHOD BLANK SPIKE |                   |       | MATRIX SPIKE |          |       |       |          |       |       |
|------------------------------|---------|--------------|---------|--------------------|-------|--------------------|-------------------|-------|--------------|----------|-------|-------|----------|-------|-------|
| KFT Date. Aug 00, 2021       |         |              | •       |                    | -     | Method             |                   |       |              | WILTIOD  |       |       |          |       |       |
| PARAMETER                    | Batch   | Sample<br>Id | Dup #1  | Dup #2             | RPD   | Blank              | Measured<br>Value | Lin   | nits         | Recovery | Lin   | nits  | Recovery | Lin   | nits  |
|                              |         |              |         |                    |       |                    |                   | Loner | opper        |          | Loner | opper |          | Lower | opper |
| Anion Scan                   | 0700440 |              |         | 0.05               |       |                    | 4000/             |       | 4000/        | 4050/    | 000/  | 4000/ | 070/     | 700/  | 4000/ |
| Fluoride                     | 2799410 |              | <0.05   | <0.05              | NA    | < 0.05             | 103%              | 70%   | 130%         | 105%     | 80%   | 120%  | 97%      | 70%   | 130%  |
| Chloride                     | 2799410 |              | 121     | 121                | 0.0%  | < 0.10             | 96%               | 70%   | 130%         | 102%     | 80%   | 120%  | 101%     | 70%   | 130%  |
| Nitrate as N                 | 2799410 |              | <0.05   | <0.05              | NA    | < 0.05             | 96%               | 70%   | 130%         | 100%     | 80%   | 120%  | 97%      | 70%   | 130%  |
| Nitrite as N                 | 2799410 |              | <0.05   | <0.05              | NA    | < 0.05             | 97%               | 70%   | 130%         | 93%      | 80%   | 120%  | 108%     | 70%   | 130%  |
| Bromide                      | 2799410 |              | <0.05   | <0.05              | NA    | < 0.05             | 103%              | 70%   | 130%         | 101%     | 80%   | 120%  | 98%      | 70%   | 130%  |
| Sulphate                     | 2799410 |              | 57.0    | 57.3               | 0.5%  | < 0.10             | 97%               | 70%   | 130%         | 99%      | 80%   | 120%  | 97%      | 70%   | 130%  |
| Phosphate as P               | 2799410 |              | <0.10   | <0.10              | NA    | < 0.10             | 104%              | 70%   | 130%         | 97%      | 80%   | 120%  | 96%      | 70%   | 130%  |
| Total Metals in water (mg/L) |         |              |         |                    |       |                    |                   |       |              |          |       |       |          |       |       |
| Total Aluminum               | 2796934 |              | 0.576   | 0.607              | 5.2%  | < 0.010            | 103%              | 70%   | 130%         | 104%     | 80%   | 120%  | 98%      | 70%   | 130%  |
| Total Antimony               | 2796934 |              | <0.003  | < 0.003            | NA    | < 0.003            | 98%               | 70%   | 130%         | 101%     | 80%   | 120%  | 101%     | 70%   | 130%  |
| Total Arsenic                | 2796934 |              | 0.007   | 0.008              | NA    | < 0.003            | 95%               | 70%   | 130%         | 103%     | 80%   | 120%  | 104%     | 70%   | 130%  |
| Total Barium                 | 2796934 |              | 0.020   | 0.021              | 4.9%  | < 0.002            | 101%              | 70%   | 130%         | 100%     | 80%   | 120%  | 101%     | 70%   | 130%  |
| Total Beryllium              | 2796934 |              | <0.0005 | <0.0005            | NA    | < 0.0005           | 109%              | 70%   | 130%         | 107%     | 80%   | 120%  | 110%     | 70%   | 130%  |
| Total Bismuth                | 2796934 |              | <0.002  | <0.002             | NA    | < 0.002            | 105%              | 70%   | 130%         | 104%     | 80%   | 120%  | 96%      | 70%   | 130%  |
| Total Boron                  | 2796934 |              | 0.126   | 0.131              | 3.9%  | < 0.010            | 101%              | 70%   | 130%         | 102%     | 80%   | 120%  | 106%     | 70%   | 130%  |
| Total Cadmium                | 2796934 |              | <0.0001 | <0.0001            | NA    | < 0.0001           | 101%              | 70%   | 130%         | 103%     | 80%   | 120%  | 102%     | 70%   | 130%  |
| Total Chromium               | 2796934 |              | 0.029   | 0.028              | 3.5%  | < 0.003            | 103%              | 70%   | 130%         | 99%      | 80%   | 120%  | 103%     | 70%   | 130%  |
| Total Cobalt                 | 2796934 |              | <0.0005 | <0.0005            | NA    | < 0.0005           | 103%              | 70%   | 130%         | 103%     | 80%   | 120%  | 103%     | 70%   | 130%  |
| Total Copper                 | 2796934 |              | 0.010   | 0.010              | 0.0%  | < 0.001            | 99%               | 70%   | 130%         | 100%     | 80%   | 120%  | 100%     | 70%   | 130%  |
| Total Iron                   | 2796934 |              | 0.082   | 0.096              | 15.7% | < 0.010            | 105%              | 70%   | 130%         | 103%     | 80%   | 120%  | 100%     | 70%   | 130%  |
| Total Lead                   | 2796934 |              | <0.001  | <0.001             | NA    | < 0.001            | 104%              | 70%   | 130%         | 103%     | 80%   | 120%  | 96%      | 70%   | 130%  |
| Total Manganese              | 2796934 |              | 0.130   | 0.131              | 0.8%  | < 0.002            | 103%              | 70%   | 130%         | 101%     | 80%   | 120%  | 100%     | 70%   | 130%  |
| Total Mercury                | 2798708 |              | <0.0001 | <0.0001            | NA    | < 0.0001           | 102%              | 70%   | 130%         | 100%     | 80%   | 120%  | 96%      | 70%   | 130%  |
| Total Molybdenum             | 2796934 |              | 0.005   | 0.004              | NA    | < 0.002            | 104%              | 70%   | 130%         | 102%     | 80%   | 120%  | 109%     | 70%   | 130%  |
| Total Nickel                 | 2796934 |              | 0.436   | 0.446              | 2.3%  | < 0.003            | 108%              | 70%   | 130%         | 101%     | 80%   | 120%  | 103%     | 70%   | 130%  |
| Total Phosphorus             | 2796934 |              | 2.45    | 2.46               | 0.4%  | < 0.10             | 98%               | 70%   | 130%         | 97%      | 80%   | 120%  | 104%     | 70%   | 130%  |
| Total Selenium               | 2796934 |              | 0.012   | 0.012              | 0.0%  | < 0.002            | 101%              | 70%   | 130%         | 101%     | 80%   | 120%  | 103%     | 70%   | 130%  |
| Total Silicon                | 2796934 |              | 3.05    | 2.86               | 6.4%  | < 0.08             | 106%              | 70%   | 130%         | 105%     | 80%   | 120%  | 95%      | 70%   | 130%  |
| Total Silver                 | 2796934 |              | <0.0001 | <0.0001            | NA    | < 0.0001           | 102%              | 70%   | 130%         | 102%     | 80%   | 120%  | 88%      | 70%   | 130%  |
| Total Strontium              | 2796934 |              | 3.23    | 3.20               | 0.9%  | < 0.005            | 103%              | 70%   | 130%         | 101%     | 80%   | 120%  | 97%      | 70%   | 130%  |
| Total Thallium               | 2796934 |              | <0.0003 | < 0.0003           | NA    | < 0.0003           | 104%              | 70%   | 130%         | 102%     | 80%   | 120%  | 96%      | 70%   | 130%  |
| Total Tin                    | 2796934 |              | 0.014   | 0.013              | 7.4%  | < 0.002            | 94%               | 70%   | 130%         | 94%      | 80%   | 120%  | 92%      | 70%   | 130%  |
| Total Titanium               | 2796934 |              | 0.009   | 0.009              | NA    | < 0.002            | 104%              | 70%   | 130%         | 100%     | 80%   | 120%  | 104%     | 70%   | 130%  |
| Total Uranium                | 2796934 |              | <0.0005 | <0.0005            | NA    | < 0.0005           | 105%              | 70%   | 130%         | 102%     | 80%   | 120%  | 102%     | 70%   | 130%  |
| Total Vanadium               | 2796934 |              | <0.002  | <0.002             | NA    | < 0.002            | 106%              | 70%   | 130%         | 104%     | 80%   | 120%  | 108%     | 70%   | 130%  |
| Total Zinc                   | 2796934 |              | 0.292   | 0.263              | 10.5% | < 0.005            | 103%              | 70%   | 130%         | 104%     | 80%   | 120%  | 98%      | 70%   | 130%  |
| Total Zirconium              | 2796934 |              | <0.004  | <0.004             | NA    | < 0.004            | 98%               | 70%   | 130%         | 102%     | 80%   | 120%  | 103%     | 70%   | 130%  |

#### **AGAT** QUALITY ASSURANCE REPORT (V1)

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### **Quality Assurance**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

#### PROJECT: Alliston(1101-4125)

SAMPLING SITE:

AGAT WORK ORDER: 21T781957

**ATTENTION TO: Caitlyn Macphee** 

SAMPLED BY:

### Water Analysis (Continued)

| RPT Date: Aug 06, 2021 |        |        | DUPLICATE     |     |                 |          | REFERENCE MATERIAL |                 |          | METHOD BLANK SPIKE   |       |                     | MATRIX SPIKE |                | KE    |
|------------------------|--------|--------|---------------|-----|-----------------|----------|--------------------|-----------------|----------|----------------------|-------|---------------------|--------------|----------------|-------|
| PARAMETER              | Sample | Dup #1 | Dun #1 Dun #2 | RPD | Method<br>Blank | Measured | Acce<br>Lir        | eptable<br>nits | Recoverv | Acceptable<br>Limits |       | Acce<br>Recovery Li |              | ptable<br>nits |       |
|                        |        | Ia     |               |     |                 |          | value              | Lower           | Upper    |                      | Lower | Upper               |              | Lower          | Upper |

Comments: NA signifies Not Applicable.

If the RPD value is NA, the results of the duplicates are under 5X the RDL and will not be calculated.

**Certified By:** 

Inis Verastegui

**AGAT** QUALITY ASSURANCE REPORT (V1)

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# **Method Summary**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

PROJECT: Alliston(1101-4125)

AGAT WORK ORDER: 21T781957

**ATTENTION TO: Caitlyn Macphee** 

| SAMPLING SITE:        |             | SAMPLED BY:          |                      |
|-----------------------|-------------|----------------------|----------------------|
| PARAMETER             | AGAT S.O.P  | LITERATURE REFERENCE | ANALYTICAL TECHNIQUE |
| Microbiology Analysis |             |                      |                      |
| Escherichia coli      | MIC-93-7010 | EPA 1604             | Membrane Filtration  |
| Total Coliforms       | MIC-93-7010 | EPA 1604             | Membrane Filtration  |



# **Method Summary**

#### **CLIENT NAME: CROZIER & ASSOCIATES**

#### PROJECT: Alliston(1101-4125)

SAMPLING SITE:

#### AGAT WORK ORDER: 21T781957 ATTENTION TO: Caitlyn Macphee

SAMPLED BY:

| PARAMETER        | AGAT S.O.P   | LITERATURE REFERENCE                             | ANALYTICAL TECHNIQUE |
|------------------|--------------|--|----------------------|
| Water Analysis   |              | 1  | 1                    |
| Fluoride         | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |
| Chloride         | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |
| Nitrate as N     | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |
| Nitrite as N     | INOR-93-6004 | SM 4110 B  | ION CHROMATOGRAPH    |
| Bromide          | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |
| Sulphate         | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |
| Phosphate as P   | INOR-93-6004 | modified from SM 4110 B                          | ION CHROMATOGRAPH    |
| Total Aluminum   | MET-93-6103  | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |
| Total Antimony   | MET-93-6103  | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |
| Total Arsenic    | MET-93-6103  | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |
| Total Barium     | MET-93-6103  | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |
| Total Beryllium  | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Bismuth    | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Boron      | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Cadmium    | MET -93-6103 | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Chromium   | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Cobalt     | MET-93-6103  | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |
| Total Copper     | MET-93-6103  | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |
| Total Iron       | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Lead       | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Manganese  | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Mercury    | MET-93-6100  | modified from EPA 245.2 and SM 3112<br>B         | <sup>2</sup> CVAAS   |
| Total Molybdenum | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Nickel     | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Phosphorus | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Selenium   | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Silicon    | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Silver     | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Strontium  | INOR-93-6003 | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |
| Total Thallium   | MET-93-6103  | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |



# **Method Summary**

### CLIENT NAME: CROZIER & ASSOCIATES

# PROJECT: Alliston(1101-4125)

AGAT WORK ORDER: 21T781957 ATTENTION TO: Caitlyn Macphee

| SAMPLING SITE:  |             | SAMPLED BY:                                      |                      |  |  |  |  |  |  |
|-----------------|-------------|--|----------------------|--|--|--|--|--|--|
| PARAMETER       | AGAT S.O.P  | LITERATURE REFERENCE                             | ANALYTICAL TECHNIQUE |  |  |  |  |  |  |
| Total Tin       | MET-93-6103 | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Titanium  | MET-93-6103 | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Uranium   | MET-93-6103 | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |  |  |  |  |  |  |
| Total Vanadium  | MET-93-6103 | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |  |  |  |  |  |  |
| Total Zinc      | MET-93-6103 | modified from EPA 200.8, 3005A, 3010A & 6020B    | ICP-MS               |  |  |  |  |  |  |
| Total Zirconium | MET-93-6103 | modified from EPA 200.8, 3005A,<br>3010A & 6020B | ICP-MS               |  |  |  |  |  |  |

|   |                                      | Lat  | oora                  | torie  | 2.S Ph:   | Mis<br>905.71:                          | 58<br>sissaug<br>2.5100<br>web                | 35 Coc<br>a, Onta<br>Fax: 90<br>earth.a | opers Ave<br>trio L42<br>05.712.9<br>ngatlabs | enue<br>1Y2<br>5122<br>.com   | La<br>Wo<br>Co                          | ork Order<br>oler Quan     | tity:  | se 0<br>2 1 - | nly                          | 361                                    | 19                | 5        | 14  | 2  |
|---|--------------------------------------|--|-----------------------|--|---|---|---|---|---|---|---|----------------------------|--|---------------|------------------------------|--|-------------------|----------|-----|--|
| Chain of Custody Record If this is a Drinking Water sample, please<br>Report Information:   |                                      |  |                       | use Drinking Water Chain of Custody Form (potable water consumed by humans)  Regulatory Requirements:  (Please check all annifeable bayes) |   |   |   |   |   |   | Custody Seal Intact:                    |                            |  |               |                              |  |                   |          |     |  |
| Company:       C.F.Cro3ltr + Associates         Contact:       Contact         Address:       Control MacPhee         Address:       2800 High Point dr suitcion         Milton ON L9T GP4       Milton ON L9T GP4         Phone:       Fax:         Reports to be sent to:       Fax:         1. Email:       Concepted Officion of Concepter Concenter Concepter Concen |                                      |  | Table                 | gulation 153/04 Excess Soils R4<br>Indicate One<br>nd/Com<br>Res/Park<br>kgriculture<br>xture (check One)<br>Coarse<br>Eine                | 06   [<br> <br>[<br>  | Sewee<br>Sar                            | r Use<br>itary<br>Region<br>Water<br>tives (I | Storm<br>Quality<br>PWQO)               |   | Notes:       Control Control         Turnaround Time (TAT) Required:         Regular TAT (Most Analysis)       5 to 7 Business         Rush TAT (Rush Surcharges Apply)         3 Business       2 Business         Days       Days         OR Date Required (Rush Surcharges May |   |                            |  |               | J:<br>usiness<br>D<br>May A  | s Days<br>Jext Busir<br>Day<br>(pply): | ness              |          |     |  |
| Project Information:<br>Project: <u>Alliston(1101-4125)</u><br>Site Location: <u>Alliston.on</u>  |                                      |  | Rec                   | Is this submission for a     Report Guideline       Record of Site Condition?     Certificate of Analy       □ Yes     □ No                |   |   |   | ine or<br>nalys                         | ls<br>D                                       | Please provide prior notification for rush TAT<br>*TAT is exclusive of weekends and statutory holidays<br>For 'Same Day' analysis, please contact your AGAT CPM   |   |                            |  |               |                              |  |                   |          |     |  |
| Sampled By:<br>AGAT ID #:<br>Please note: If quotation number is r<br>Invoice Information:<br>Company:<br>Contact:<br>Address:<br>Email:<br>Email:<br>Company:<br>Contact:<br>Email:  | PO:<br>ot provided, client will<br>B | be billed full price for a   | inalysis,<br>s 🗌 No 🗌 | B<br>GW<br>O<br>P<br>S<br>SD<br>SW   | ple Matrix Legend<br>Biota<br>Ground Water<br>Oil<br>Paint<br>Soil<br>Sediment<br>Surface Water | Field Filtered - Metals, Hg, CrVI, DOC  | s & Inorganics                                | s - CrVI, WHg, CHWSB as 123             | ze F4G if required □ Yes □ No                 | PCBs Droclor  | III Disposal Characterization TCLP: 608 | Soils SPLP Rainwater Leach | s Soils Characterization Package 00<br>PMS Metals, BTEX, F1-F4 | EC/SAR        | .Coli                        | otal Colifernis                        | arions (Nitrate & | Nitrite) |     | tially Hazardous or High Concentration (Y/N) |
| Sample Identification   | Date<br>Sampled                      | Time<br>Sampled  | # of<br>Containers    | Sample<br>Matrix   | Comments/<br>Special Instructions   | Y/N                                     | Metal   | Metal<br>BTEX,                          | Analy<br>PAHs                                 | Total   | Landfi                                  | Exces<br>SPLP              | Exces<br>pH, IC  | Salt -        | Ш                            | F 7                                    | . Q               |          |     | Poten  |
| MW2<br>MW3<br>MW4<br>MUS  | 07/30<br>07/30<br>07/30<br>07/30     | Q:00 PM<br>9:30 PM<br>10:00 PM<br>12:00 PM<br>12:00 PM<br>AM<br>AM<br>AM | 888                   | GW<br>GW<br>GW<br>GW   |   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | >>>>>   |   |   |   |   |                            |  |               | >>>>>                        |  |                   |          |     |  |
| Samples Relinquished By (Print Name and Sign):  | ne                                   | Date   | Time<br>2             | :15  | Samples Received By (Print, Name and Sign):   | _ <u> </u>                              |   |   |   | Date  |   | Time                       | 18   |               |                              | 121                                    | JU                | 30       | 2:1 | Spy  |
| Samples Relinquisheld By (Print Name and Sign): Date Samples Relinquished By (Print Name and Sign): Date  |                                      | Time   |                       | Samples Received By (Print Name and Sign):<br>Samples Received By (Print Name and Sign):   |   |   |   |   | Date  |   | Time                                    | Time                       |  |               | Pageof<br>№: <b>т1</b> 17274 |  |                   |          |     |  |

Potential (5) 101 20 1511 000

Pink Copy - Client 1 Yellow Copy - AGAT | White Copy- AGAT Drage 2007 2007 2007

# APPENDIX |

D-5-4 Impact Assessment

#### Table 1: D-5-4 Impact Assessment

|   | Project Name:               | Pilla Alliston 7723 HWY 89   |  |  |  |  |  |  |
|---|-----------------------------|--|--|--|--|--|--|--|
|   | Project Number              | : 1101-4125  |  |  |  |  |  |  |
|   | Date:                       | 7/6/2021   |  |  |  |  |  |  |
|   | Designed By:                | ΔΙ   |  |  |  |  |  |  |
| UNULIL  | Checked By:                 | KR   |  |  |  |  |  |  |
| CONSULTING ENGINE   | ERS Checked by:             |  |  |  |  |  |  |  |
|   |                             |  |  |  |  |  |  |  |
|   | D-5-4 IMPACT ASSI           | ESSMENT  |  |  |  |  |  |  |
| Calculate the Nitrate Concentration at a Boundary (Property or Surface Water) |                             |  |  |  |  |  |  |  |
| Parameter   | Value Unit                  | Notes:   |  |  |  |  |  |  |
| Infiltration Volume   |                             |  |  |  |  |  |  |  |
| Area of Dilution =  | 28.4 ha                     | Total area of site   |  |  |  |  |  |  |
| Background Nitrate Quality in Groundwater =                                   | 3.24 mg/L                   | Average of nitrate sample concentrations for all wells 8/6/2021              |  |  |  |  |  |  |
| Annual Infiltration Rate =  | 200 mm/m2/yr                | MECP infiltration rate for silt loam   |  |  |  |  |  |  |
|   | 5,479.45 L/ha/day           |  |  |  |  |  |  |  |
| Annual Infiltration Volume =  | 56,800 m³/year              |  |  |  |  |  |  |  |
| Total Average Background Nitrate =  | 503,886 mg/day              |  |  |  |  |  |  |  |
| Sewage Effluent Volume  |                             |  |  |  |  |  |  |  |
| Proposed Number of Lots   | 22                          |  |  |  |  |  |  |  |
| Average Daily Volume of Sewage Effluent =                                     | 1,500 L/day                 | Max total daily sewage flow (3,750L/d) with average day peaking factor (2.5) |  |  |  |  |  |  |
| Number of Days of Operation/Use =   | 365 days/year               |  |  |  |  |  |  |  |
| Annual Volume of Sewage Effluent =  | 12.045 m <sup>3</sup> /year |  |  |  |  |  |  |  |
| Nitrate Concentration in wastewater =   | 40.0 mg/L                   | MECP standard effluent for conventional systems = 40 mg/L                    |  |  |  |  |  |  |
| Total Average Nitrate Loading =   | 1,320,000 mg/day            | , ,  |  |  |  |  |  |  |
|   |                             |  |  |  |  |  |  |  |
| I OTAIS   |                             |  |  |  |  |  |  |  |
| I otal Dilutant = wastewater V + infiltration V =                             | 68,845 m <sup>~</sup> /year |  |  |  |  |  |  |  |
| Nitrate Concentration in Percolate =  | 9.67 mg/L                   | Less than 10 mg/L, sufficient for D-5-4 Impact Assessment                    |  |  |  |  |  |  |
|   |                             |  |  |  |  |  |  |  |

# FIGURES

Figure 1:Site Location PlanFigure 2:PhysiographyFigure 3:Bedrock GeologyFigure 4:Surficial GeologyFigure 5:MECP Well Location PlanFigure 6:Well Location Plan







Earl Rowe

**Provincial Park** 

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7723 HIGHWAY 89 TOWN OF ALLISTON

BEDROCK GEOLOGY

2800 High Point Drive Suite 100 Milton, ON L9T 6P4 905-875-0026 T 905-875-4915 F www.cfcrozier.ca

| Drawn | С.М.       | Design<br>C.G.           | Project | <sup>No.</sup> 1 | 101-4125                |
|-------|------------|--------------------------|---------|------------------|-------------------------|
| Date  | 2021-11-24 | Projection<br>EPSG:26917 | Scale   | 1:24,000         | <sup>Dwg.</sup> FIG. 03 |







Site Location



Adjala-Tosorontio

KEY PLAN SCALE: 1:100,000

Tecumse

## LEGEND

Property Limits

## Surficial Geology

| 19: clay, silt, sand, gravel        |
|-------------------------------------|
| 12: clay, silt, sand, gravel        |
| 9c: sand, silt                      |
| 7: sand                             |
| 6: sand, gravel                     |
| 5b: silty to sandy till, stone-poor |
|                                     |

5d: silty to clayey till

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ALL EXISTING UNDERGROUND UTILITIES TO BE VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO CONSTRUCTION.

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Drawing

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| 1 | .2 | km |
|---|----|----|
|   |    |    |

9c

| rawn | С.м.       | Design<br>C.G.           | Project | <sup>No.</sup> 1 | 101  | -41  | 25 |
|------|------------|--------------------------|---------|------------------|------|------|----|
| ate  | 2021-11-24 | Projection<br>EPSG:26917 | Scale   | 1:24,000         | Dwg. | FIG. | 04 |
|      |            |                          |         |                  |      |      |    |



